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PHYSICAL GEOGRAPHY OF PEARY LAND

I. METEOROLOGICAL OBSERVATIONS FOR
JØRGEN BRØNLUNDS FJORD

BY

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PREFACE

A regular meteorological service was established during the Danish Pearyland Expedition, partly for purely scientific reasons and partly for the sake of the flights to and from Peary Land. The observations were made at the winter station on the south coast of Jørgen Brønlunds Fjord, observations being made regularly every third hour and those of 00, 06, 12, and 18 o'clock being included in the radio reports to Denmark. The winter station "Brønlund Hus" thus entered in the net of Greenland weather stations, being given the number 311.

My most sincere thanks are due to Count EIGIL KNUTH, Chief of the Expedition, for his never failing interest in the meteorological service and for permitting that the whole material was submitted to me for working up. The observation service during the first wintering 1948—49 was attended to by the author and by Mr. AAGE JACOBSEN, wireless operator, who besides his exacting professional duties had with the greatest readiness undertaken this task, too, and who during my often prolonged absence from the station attended to the observations alone. During the second wintering the observations were made by Mr. BØRGE IB HAAGENSEN and Mr. KRISTEN SØRENSEN, wireless operators. It is a pleasant duty for me to thank all of them for the great interest, helpfulness, and never failing spirit with which they attended to the service, just as I also want to thank the other members of the Expedition for their helpfulness during the observations.

The working up of the whole material collected has taken place in the Geographical Laboratory of the University of Copenhagen, to the chief of which, Professor NIELS NIELSEN, Ph. D., I am much obliged for facilities and interest and support in the work.



Fig. 1.

INTRODUCTION

The winter house of the Danish Peary Land Expedition was situated on the south coast of Jørgen Brønlunds Fjord, a tributary fjord to the large Independence Fjord about 50 km in length, stretching in a due westerly direction, and continued by the 125 km long, very broad Wandels Dal, at the bottom of which Midsommersøen is situated. Jørgen Brønlunds Fjord is bounded in the north by the about 600 m high and very steep mountain called Buen ('the Arch'), which constitutes the edge of the large tableland forming the whole of the inner Peary Land, in the south by Heilprin Land, which is also a tableland, but the coast of which on Jørgen Brønlunds Fjord rises in terraces to heights of 1100—1300 m.

The winter station, "Brønlund Hus", was built on the edge of a small riverbed only about 8 m above sea level. In this locality the meteorological observations were made, as about 75 m west of the house there was a meteorological station with rain gauge and heliograph. An anemometer and a vane were placed on the roof of this station, the former being 5 m above the ground and $1\frac{1}{2}$ m above the roof of the house. By determinations made by Johs. Troelsen and Thorkild Nielsen the geographical coordinates of the station were made out to be $82^{\circ}10.4'$ lat. N. and $30^{\circ}29.8'$ long. W.

Column 1 and 2. Date and GMT.

Observations were made 8 times a day, viz. at 00, 03, 06, 09, 12, 15, 18, and 21 o'clock GMT, all time indications being stated at GMT. The observations at 03, 09, 15, and 21 o'clock were made at the full hour, thus 0300, etc., whereas those at 00, 06, 12, and 18 o'clock on account of the wireless service had to be made a quarter of an hour before, corresponding to what is normally the case of the other Greenland weather stations. The records of the observations were sent by radio via Danmarkshavn or Daneborg to Scoresbysund and from there to Denmark.

The ordinary synoptic observations were made, and besides these, measurements were made of the number of sunny hours, light intensity,

etc., but the following observation journal only contains a survey of the synoptic observations made. Radio-sonde observations were planned, but because of the difficult conditions of flying in East and North Greenland the equipment for measurements in the high altitudes had to be left at the south base at Zackenberg and so the observations of conditions in the high altitudes were not made.

Column 3. Pressure.

Atmospheric pressure was measured with a Fuess mercurial barometer with a nonius scale, which was read in mm, but the statements in the table are in mb. and reduced to 0° C., sea level, and 45° lat. N. The reduction has been made according to the "Directions for Observation Service Published by the Meteorological Institute and Aviation Service of the State" ("Vejledning i observationstjeneste udgivet af Meteorologisk Institut og Statens luftfartsvæsen").

Column 4. Wind.

Force of the wind was measured with an electric Meopta anemometer at m/sec., the direction of the wind being indicated according to a 32-partite scale.

Column 5, 6 and 7. Air Temperatures (Dry, Max., Min.).

Temperature was measured in the English hut, where there were a mercury thermometer and a spirit thermometer measuring at $\frac{1}{10}^{\circ}$ C. The maximum temperature was measured at 18 o'clock and states the maximum temperature of the preceding 24 hours, while the minimum temperature is correspondingly stated at 06 o'clock for the preceding 24 hours.

Column 8. Relative Humidity.

Humidity of the air was measured with a Hänni respiration psychrometer and with a hair hygrometer. In winter the latter was exclusively used.

Column 9. Visibility.

Visibility was indicated according to a 10-partite scale, the numbers 90—99 in the international code, i. e. the following intervals were distinguished:

0.00—	0.05 km
0.05—	0.2 —
0.2 —	0.5 —
0.5 —	1 —

1	—	2	km
2	—	4	-
4	—	10	-
10	—	20	-
20	—	50	-
and	>	50	-

As points of sight various prominent points on Buen were used, and the large visibilities were estimated according to the possibility of seeing the glaciers at Astrup Fjord on the other side of Independence Fjord.

Column 10. The Weather at the Time of Observation.

The weather at the time of observation was indicated according to the ordinary international code by means of the figures from 00 to 99, the following figures being used:

No precipitation at the station at the time of the observation.

- 00 cloud development not observed in the past hour.
- 01 clouds dissolving or becoming less developed during the past hour.
- 02 state of sky on the whole unchanged during the past hour.
- 03 clouds forming or developing during the past hour.
- 05 dry haze.
- 06 widespread dust in suspension in the air, not raised by wind at or near the station at the time of observation.
- 07 dust or sand raised by wind at or near station at the time of observation, but no well developed dust devil, and no duststorm or sandstorm seen.
- 08 well developed dust devil seen at or near the station within the last hour, but no duststorm or sandstorm.
- 09 duststorm or sandstorm within sight of station during the last hour.
- 10 mist, visibility 1—2 km.
- 11 shallow fog in patches.
- 12 shallow fog more or less continuous, fog not deeper than about 2 m.
- 14 precipitation within sight, not reaching the ground at the station.
- 15 precipitation within sight, reaching the ground but distant from the station.
- 16 precipitation within sight, reaching the ground near but not at the station.

Precipitation or fog at the station during the preceding hour
but not at the time of observation.

- 20 drizzle (not freezing).
- 21 rain (not freezing).

- 22 snow.
- 23 rain and snow.
- 24 freezing drizzle or freezing rain.
- 25 showers of rain.
- 26 showers of snow or of rain and snow.
- 28 fog.

Duststorm, sandstorm, or drifting snow.

- 30 slight or moderate duststorm or sandstorm has decreased during preceding hour.
- 31 slight or moderate duststorm or sandstorm; no appreciable change during preceding hour.
- 32 slight or moderate duststorm or sandstorm has increased during the preceding hour.
- 36 generally low, slight, or moderate drifting snow.
- 37 generally low, heavy drifting snow.
- 38 generally high, slight, or moderate drifting snow.
- 39 generally high, heavy drifting snow.

Fog at the time of observation, visibility below 1000 (with the exception of 40).

- 40 fog at a distance at the time of observation, but not in the last hour, the fog extending to a level above that of the observer.
- 41 fog in patches.
- 42 fog has become thinner during the preceding hour, sky discernible.
- 43 fog has become thinner during the preceding hour, sky not discernible.
- 44 fog, no appreciable change during the preceding hour, sky discernible.
- 45 fog, no appreciable change during the preceding hour, sky not discernible.
- 46 fog has begun or has become thicker during the preceding hour, sky discernible.
- 47 fog has begun or has become thicker during the preceding hour, sky not discernible.
- 48 fog, depositing rime, sky discernible.
- 49 fog, depositing rime, sky not discernible.

Precipitation at the station at the time of observation.

- 50 slight drizzle, not freezing, intermittent.
- 51 slight drizzle, not freezing, continuous.
- 52 moderate drizzle, not freezing, intermittent.
- 53 moderate drizzle, not freezing, continuous.
- 54 thick drizzle, not freezing, intermittent.
- 55 thick drizzle, not freezing, continuous.

- 56 drizzle, freezing, slight.
- 57 drizzle, freezing, moderate or thick.
- 58 drizzle and rain, slight.
- 59 drizzle and rain, moderate or heavy.
- 60 rain, not freezing, intermittent.
- 61 slight rain, not freezing, continuous.
- 62 moderate rain, not freezing, intermittent.
- 63 moderate rain, not freezing, continuous.
- 66 rain, freezing, slight.
- 67 rain, freezing, moderate or heavy.
- 68 rain or drizzle and snow, slight.
- 69 rain or drizzle and snow, moderate or heavy.
- 70 slight intermittent fall of snow flakes.
- 71 slight continuous fall of snow flakes.
- 72 moderate intermittent fall of snow flakes.
- 73 moderate continuous fall of snow flakes.
- 74 heavy intermittent fall of snow flakes.
- 75 heavy continuous fall of snow flakes.
- 76 ice needles (with or without fog).
- 77 granular snow (with or without fog).
- 78 isolated starlike snow crystals (with or without fog).
- 79 ice pellets.
- 80 rain showers, slight.
- 81 rain showers, moderate or heavy.
- 82 rain showers, violent.
- 83 showers of rain and snow, slight.
- 84 showers of rain and snow, moderate or heavy.
- 85 snow showers, slight.
- 86 snow showers, moderate or heavy.
- 87 slight showers of soft or small hail with or without rain or rain and snow mixed.
- 88 moderate or heavy showers of soft or small hail with or without rain or rain and snow mixed.

Column 11. Past Weather.

The course of the weather since the latest observation is indicated by the figures 0—9, the following code being used:

- 0 fair (clear or slightly clouded).
- 1 variable sky.
- 2 mainly overcast.
- 3 sandstorm or duststorm or storm of drifting snow, no precipitation.
- 4 fog or thick dust haze (visibility less than 1000 m).

- 5 drizzle.
- 6 rain.
- 7 snow or sleet.
- 8 showers.

Column 12. Total Amounts of Clouds.

The total amount of cloud is stated in eighths, 0—8, while 9 indicates that the amount of cloud cannot be stated.

Column 13. Amounts of Clouds Below 2500 m.

The amount of clouds, the altitude of which is stated in the following column, is measured in eighths as follows:

- 0 no clouds below 2500 m.
- 1 $\frac{1}{8}$ of the sky covered.
- 2 $\frac{2}{8}$ of the sky covered, etc.
- 9 amount of cloud cannot be stated.

Column 14. Form of Low Clouds.

The genera of lower clouds are indicated according to the international cloud atlas by the figures 0—9:

- 0 no stratocumulus, stratus, cumulus, or cumulonimbus clouds.
- 1 cumulus with little vertical development and seemingly flattened.
- 2 cumulus of considerable development, generally towering, with or without other cumulus or stratocumulus, bases all at the same level.
- 3 cumulonimbus with tops lacking clear-cut outlines but distinctly not cirriform or anvil-shaped or without cumulus, stratocumulus, or stratus.
- 4 stratocumulus formed by the spreading out of cumulus, cumulus also often present.
- 5 stratocumulus not formed by the spreading out of cumulus.
- 6 stratus or fractostratus or both, but no fractostratus of bad weather.
- 7 fractostratus and/or cractocumulus of bad weather ("scud") usually under nimbostratus. By bad weather is meant the conditions usually prevailing before, during, or after precipitation.
- 8 cumulus and stratocumulus other than those formed by the spreading out of cumulus, with bases at different levels.
- 9 cumulonimbus having a clearly fibrous (cirriform) top, often anvil-shaped, with or without cumulus, stratocumulus, stratus, or "scud".
- × the genera of clouds have not been observed.

Column 15. Height of Base of Clouds.

The altitude of cloud, i. e. the vertical distance from the ground to the base of the lowest clouds present, is indicated according to the following scale:

- 0 0— 50 m.
- 1 50— 100 -
- 2 100— 200 -
- 3 200— 300 -
- 4 300— 600 -
- 5 600—1000 -
- 6 1000—1500 -
- 7 1500—2000 -
- 8 2000—2500 -
- 9 more than 2500 m or cloudless.
- × altitude of cloud cannot be stated.

Column 16. Form of Middle Clouds.

The genera of clouds of medium altitude are indicated according to the following code:

- 0 no altocumulus, altostratus, or nimbostratus clouds.
- 1 thin altostratus (semi-transparent everywhere) through which the sun or moon would be seen dimly as through ground glass.
- 2 thick altostratus or nimbostratus. Through portions of the sheet the position of the sun or moon may be indicated by a light patch.
- 3 thin (semi-transparent) altocumulus, cloud elements not changing much, at a single level.
- 4 thin (semitransparent) altocumulus in patches (often almond- or fish-shaped), cloud elements continually changing and/or occurring at more than one level.
- 5 thin (semi-transparent) altocumulus in bands or in a layer gradually spreading over the sky and usually thickening as a whole; it may become partly opaque or double-layered.
- 6 altocumulus formed by the spreading out of cumulus.
- 7 double-layered altocumulus usually opaque in parts, not increasing; or a thick (opaque) layer of altocumulus, not increasing; or altostratus and altocumulus both present at the same or different levels.
- 8 altocumulus in the form of cumulus-shaped tufts or altocumulus with turrets.
- 9 altocumulus of a chaotic sky, generally at different levels, dense cirrus in patches usually also present.
- × the genera of clouds have not been observed.

Column 17. Form of High Clouds.

The genera of clouds of high altitude are indicated according to code:

- 0 no cirrus, cirrocumulus, or cirrostratus clouds.
- 1 filaments or strands of cirrus, scattered and not increasing, often "mares' tails".
- 2 dense cirrus in patches or twisted sheaves, usually not increasing, possibly but not certainly the remains of the upper part of cumulonimbus.
- 3 cirrus, often anvil-shaped, either the remains of the upper portions of cumulonimbus or part of a distant cumulonimbus the rest of which is not visible.
- 4 cirrus (often hook-shaped) gradually spreading over the sky and gradually thickening as a whole.
- 5 cirrus and cirrostratus, often in bands converging towards the horizon or cirrostratus alone, in either case gradually spreading over the sky and usually thickening as a whole, but the continuous layer not reaching 45° altitude.
- 6 cirrus and cirrostratus, often in bands converging towards the horizon, or cirrostratus alone, in either case gradually spreading over the sky and usually thickening as a whole, the continuous layer exceeding 45° altitude.
- 7 cirrostratus covering the whole sky.
- 8 cirrostratus not increasing and not covering the whole sky; cirrus and cirrocumulus may be present.
- 9 cirrocumulus alone or cirrocumulus with some cirrus or cirrostratus, but the cirrocumulus being the main cirriform cloud present; cirrocumulus may be present in C_H 1 to C_H 8.
- × the genera of clouds have not been observed.

Column 18. Characteristic of Barometric Tendency.

The characteristic of barometric tendency is indicated according to the following code:

Barometer now higher than or the same as 3 hours ago

- 0 rising then falling.
- 1 rising then steady, or rising then rising more slowly.
- 2 unsteady.
- 3 steady or rising.
- 4 falling or steady then rising, or rising then rising more quickly.

Barometer now lower than 3 hours ago.

- 5 falling then rising.
- 6 falling then steady, or falling then falling more slowly.

7 unsteady.

8 falling.

9 steady or rising then falling, or falling then falling more quickly.

Column 19. Precipitation.

Precipitation is indicated in mm of water, the snow being melted and converted into water. In summer a normal rain-gauge was used, which in winter was provided with a cross of tin in the funnel in order to prevent the snow from whirling up again. With the small totals of precipitation, however, all gaugings of snow are very uncertain. Measurements along poles also gave very poor results, so that the measurements of precipitation must be accepted with reserve. $\times \times$ indicates that measurement of precipitation was impossible; trace, that traces of precipitation have come down, but too small for measurement.

METEOROLOGICAL JOURNAL
OF JØRGEN BRØNLUNDS FJORD

Date	GMT	Pressure in mb. at sea level	Wind m. pr. sec.	Air temperatures			Relative humidity	Visibility	The weather at the time of observation	Past weather	Total amounts of clouds in eights	Amounts of clouds in eights below 2500 m.	Form of low clouds	Height of base of clouds	Form of middle clouds	Form of high clouds	Characteristic of barometric tendency	Precipitation in mm.
				Dry	Max.	Min.												

August 1948

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
2	12	1007.0	W 8	17.6	46	20—40	02	2	6
	15	1008.7	E 6	10.8	48	20—50	02	2	6	0	0	9	0	6	3	..
	18	1009.0	E 5	11.3	18.0	..	46	20—50	02	2	7	0	0	9	0	6	3	0.0
	21	1010.1	E 3	11.3	52	> 50	01	2	6	0	0	9	0	3	3	..
3	00	1010.2	E 2	11.2	50	> 50	02	2	6	0	0	9	0	3	3	..
	03	1011.0	E 4	6.7	43	20—50	02	2	6	0	0	9	4	3	3	..
	06	1011.3	W 9	10.9	..	6.5	43	20—50	02	2	6	0	0	9	4	3	3	0.0
	09	1011.5	E 4	10.8	42	20—50	03	2	7	7	0	8	4	3	3	..
	12	1011.6	E 5	11.0	45	20—50	02	2	7	7	0	8	7	0	3	..
	15	1011.8	E 4	9.4	55	20—50	02	2	7	7	0	8	7	0	3	..
	18	1012.5	E 7	9.0	11.5	..	45	> 50	02	2	7	7	0	8	7	0	1	0.0
	21	1012.5	W 2	9.7	68	> 50	03	2	7	7	0	8	7	0	3	..
4	00	1012.5	W 1	9.1	80	20—50	03	2	7	7	0	8	7	0	3	..
	03	1012.4	E 1	5.8	81	20—50	01	2	5	4	0	8	7	0	3	..
	06	1012.5	E 3	5.8	..	4.8	90	> 50	01	2	4	1	0	8	4	0	3	0.0
	09	1011.5	E 4	6.4	86	> 50	02	1	3	3	0	8	7	0	9	..
	12	1009.1	E 4	6.4	82	> 50	02	1	2	2	2	8	5	0	8	..
	15	1008.7	E 4	6.2	73	20—50	02	1	2	2	2	8	5	0	8	..
	18	1009.3	E 6	6.5	9.7	..	70	20—50	02	1	2	1	4	7	7	3	4	0.0
	21	1009.9	E 3	5.0	90	20—50	01	2	6	2	4	7	7	5	3	..
5	00	1010.5	E 3	5.0	85	20—50	01	2	4	2	4	7	7	5	3	..
	03	1012.9	0	5.0	99	10—20	21	5 ¹	8	8	5	4	×	×	4	..
	06	1013.6	E 1	5.0	..	4.8	98	0.5—1	62	6	8	8	6	3	×	×	1	0.7
	09	1014.3	E 1	4.3	98	4—10	66	6	8	8	5	4	×	×	3	..
	12	1015.0	E 2	3.4	98	4—10	62	6	8	8	5	4	×	×	3	..
	15	1015.0	E 3	4.3	95	4—10	62	6	8	8	5	4	×	×	3	..
	18	1015.0	E 4	4.8	6.5	..	98	4—10	62	6	7	7	5	4	×	×	3	1.9
	21	1015.6	E 2	4.8	99	4—10	62	6	8	8	5	3	×	×	3	..
6	00	1015.6	E 4	4.8	95	10—20	62 ²	6	7	4	5	5	7	×	3	..
	03	1015.7	E 1	4.2	85	10—20	22	2	6	3	5	6	3	0	3	..
	06	1014.3	E 3	4.6	..	3.0	70	20—50	02	2	6	3	2	7	5	9	9	0.6

¹ 0100 Fog coming from W, slight rain. ² Snow at "Buen".

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1013.2	E 3	4.5	74	20—50	02	2	6	4	2	7	5	9	8	
	12	1012.1	E 3	4.6	77	20—50	03	2	7	6	2	7	6	×	8	
	15	1010.6	E 3	4.5	77	20—50	01	2	6	6	0	8	7	0	8	
	18	1009.0	E 3	4.7	4.9	..	78	20—50	02	2	6	6	0	8	7	0	8	0.0
7	21	1007.5	E 5	5.1	72	> 50	01	1	0	0	0	9	0	0	8	
	00	1005.3	E 4	4.2	70	20—50	00	0	0	0	0	9	0	0	8	
	03	1004.9	E 4	3.6	72	20—50	00	0	0	0	0	9	0	0	9	
	06	1003.1	E 5	4.2	..	2.9	80	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1002.3	E 5	5.1	62	> 50	01	0	1	0	0	9	0	4	6	
	12	1002.3	E 4	5.2	66	> 50	02	0	1	0	0	9	0	4	3	
	15	1002.7	E 4	5.4	66	> 50	03	1	2	0	0	9	0	4	0	
	18	1002.3	E 5	5.6	5.9	..	65	> 50	02	1	2	0	0	9	0	4	0	0.0
8	21	1003.0	E 4	5.6	68	20—50	01	1	1	0	0	9	0	2	5	
	00	1004.4	E 4	5.6	79	20—50	03	2	6	4	0	8	7	4	3	
	03	1005.0	E 4	4.4	72	20—50	03	2	6	4	2	8	7	4	3	
	06	1005.4	E 4	4.6	..	3.2	73	20—50	02	2	6	4	5	7	7	0	3	0.0
	09	1005.4	E 4	4.1	74	10—20	03	2	7	5	5	7	7	0	3	
	12	1005.5	E 4	3.2	78	2—4	03	2	8	8	5	6	×	×	3	
	15	1005.5	E 5	2.8	85	2—4	03	2	8	8	5	3	×	×	3	
	18	1008.1	E 5	2.4	5.6	..	80	10—20	02	2	7	7	5	6	×	×	4	0.0
	21	1008.6	E 3	1.9	85	10—20	03	2	7	7	5	6	0	×	3	
9	00	1009.2	E 2	2.1	70	20—50	02	2	6	1	5	4	0	9	3	
	03	1005.8	W 7	3.2	68	20—50	02	2	6	7	5	7	6	9	9	
	06	1005.0	W 9	5.2	..	0.9	57	> 50	02	2	7	7	0	7	6	9	8	0.0
	09	1004.5	W 10	5.0	62	2—4	02	2	7	4	5	1	6	9	8	
	12	1003.8	W 12	4.7	73	2—4	02	2	7	4	5	1	6	×	8	
	15	1002.6	W 14	1.4	98	1—0.5	72	2	8	8	5	1	×	×	8	
	18	1000.4	W 10	2.1	5.3	..	98	2—4	72 ¹	2	8	8	5	5	×	×	8	0.2
	21	999.9	W 9	2.1	99	0.2—0.5	72	2	8	8	5	1	×	×	8	
10	00	1000.9	W 10	1.6	99	0.2—0.5	72	2	8	8	5	0	×	×	8	
	03	1001.3	W 9	1.3	100	0.2—0.5	72	2	8	8	5	1	×	×	3	
	06	1002.8	W 10	1.2	..	1.0	100	0.2—0.5	72	2	8	8	5	1	×	×	3	2.0
	09	1004.2	W 10	1.3	100	0.2—0.5	72	7	8	8	5	1	×	×	3	
	12	1005.8	W 14	1.5	100	0.05—0.2	72	7	8	8	5	1	×	×	3	
	15	1006.1	W 12	3.1	100	1—2	72	7	8	8	5	3	×	×	3	
	18	1006.7	W 9	3.4	3.4	..	100	1—2	72	7	8	8	5	3	×	×	3	1.6
	21	1008.2	W 3	4.1	100	2—4	68	7	8	8	5	4	×	×	4	
11	00	1009.5	W 12	2.8	98	0.5—1	68	2	8	8	5	5	×	×	3	
	03	1010.4	W 9	3.3	99	0.5—1	03	2	8	8	5	5	×	×	3	
	06	1011.3	W 6	3.5	..	1.1	88	4—10	03	2	8	8	5	6	×	×	3	0.6
	09	1010.8	W 6	4.0	82	4—10	03	2	8	8	5	6	×	×	9	
	12	1010.5	W 6	4.3	78	4—10	03	2	8	8	5	6	×	×	6	
	15	1009.8	W 5	5.0	5.0	..	78	10—20	03	2	8	8	5	6	×	×	8	
	18	1008.4	W 8	5.0	78	10—20	03	2	8	8	5	6	×	×	8	0.0
	21	1007.0	W 5	5.8	67	10—20	03	2	8	8	5	6	×	×	8	
12	00	1006.6	W 5	4.9	69	20—50	02	2	5	3	8	5	7	×	8	
	03	1006.0	W 4	4.7	73	20—50	02	2	5	3	8	5	7	×	8	
	06	1005.8	W 5	4.7	..	3.2	80	10—20	02	2	5	3	8	5	7	×	8	0.0

¹ Snow at "Buen".

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1005.4	W 6	6.1	70	10—20	02	2	5	3	8	6	7	×	8	
	12	1005.3	W 5	6.0	70	10—20	02	2	8	3	8	6	7	×	6	
	15	1005.3	W 5	6.2	67	10—20	02	2	8	3	8	6	7	×	3	
	18	1005.3	W 5	6.8	7.0	..	63	20—50	02	2	7	2	5	6	7	×	3	0.0
	21	1007.7	W 6	5.4	72	20—50	03	2	8	2	5	4	×	×	3	
13	00	1009.0	E 5	3.4	84	20—50	03	2	8	2	5	4	×	×	3	
	03	1009.7	E 3	2.8	90	20—50	03	2	8	4	5	3	×	×	3	
	06	1010.3	E 4	2.3	..	2.1	98	20—50	03	2	8	4	5	3	×	×	3	0.0
	09	1011.0	E 2	2.3	98	10—20	02	2	8	8	5	4	×	×	3	
	12	1011.0	E 2	3.1	98	20—50	02	2	8	7	5	4	×	×	3	
	15	1010.0	0	2.4	99	20—50	02	2	8	8	5	3	×	×	3	
	18	1009.5	0	1.5	6.8	..	99	0.5—1	09	6	8	8	5	2	×	×	3	0.0
	21	1009.5	0	1.1	99	0.5—1	09	6	8	8	5	2	×	×	3	
14	00	1009.6	E 1	1.1	100	4—10	72	6	8	8	5	2	×	×	3	
	03	1009.6	0	1.1	100	2—4	21	6	8	8	5	2	×	×	3	
	06	1009.6	0	1.3	..	1.0	100	2—4	60	6	8	8	5	2	×	×	3	5.0
	09	1009.8	0	2.0	87	2—4	60	6	8	8	5	2	×	×	3	
	12	1009.8	W 2	2.0	87	10—20	02	6	7	6	5	4	0	×	3	
	15	1009.4	W 2	6.5	68	20—50	02	2	6	3	3	5	5	0	9	
	18	1009.1	W 3	7.1	7.1	..	62	20—50	02	2	4	2	2	6	5	0	6	0.0
	21	1009.1	W 3	7.1	58	> 50	02	0	4	1	2	7	5	0	3	
15	00	1009.1	W 3	6.9	63	> 50	02	0	4	1	2	7	5	0	3	
	03	1009.2	E 1	4.2	78	> 05	01	0	2	2	4	7	0	0	3	
	06	1010.5	E 1	3.4	..	1.3	83	> 50	01	0	2	2	4	6	0	0	4	0.0
	09	1010.2	0	1.6	88	20—50	02	2	8	7	0	7	7	×	9	
	12	1008.0	E 5	3.6	78	20—50	03	2	8	8	5	6	×	×	8	
	15	1006.4	E 2	3.7	76	20—50	03	2	4	4	5	6	0	0	8	
	18	1004.7	E 1	3.4	7.2	..	78	20—50	01	0	4	3	4	6	0	0	8	0.0
	21	1004.1	E 5	2.7	78	20—50	02	2	4	4	5	6	0	0	5	
16	00	1000.0	E 1	2.1	84	20—50	01	2	4	4	5	6	0	0	8	
	03	1002.8	E 2	1.9	88	20—50	02	2	5	5	5	6	0	0	4	
	06	1002.6	0	1.4	..	0.9	92	20—50	02	2	6	5	5	6	0	0	9	0.0
	09	1002.4	0	2.2	100	20—50	02	2	8	8	5	5	0	0	8	
	12	1001.8	E 2	3.7	80	20—50	02	2	2	2	5	6	3	0	8	
	15	1001.4	E 1	3.8	78	20—50	00	2	4	3	5	6	3	0	8	
	18	1000.9	E 2	2.4	3.9	..	73	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	999.5	E 3	2.3	68	> 50	00	0	0	0	0	9	0	0	6	
17	00	999.0	E 3	3.5	73	> 50	00	0	0	0	0	9	0	0	7	
	03	996.7	0	1.0	78	> 50	00	0	0	0	0	9	0	0	8	
	06	993.2	E 3	0.4	..	÷ 0.6	91	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	993.7	0	1.3	83	> 50	00	0	0	0	0	9	0	0	4	
	12	995.8	0	3.3	69	> 50	01	0	1	1	0	9	0	8	4	
	15	998.9	W 12	5.8	45	> 50	01	0	2	2	0	9	0	5	3	
	18	998.9	W 10	6.1	7.0	..	41	> 50	01	0	3	3	0	9	0	5	3	0.0
	21	1000.1	W 14	5.4	44	> 50	01	0	3	1	1	7	0	5	3	
18	00	1001.0	W 12	4.6	48	> 50	01	0	0	0	1	9	0	0	3	
	03	1002.1	W 10	4.0	43	> 50	00	0	0	0	0	9	0	0	3	
	06	1003.0	W 8	3.5	..	0.5	49	> 50	00	0	0	0	0	9	0	0	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1004.0	W 6	4.9	56	> 50	00	0	0	0	0	9	0	0	3	
	12	1004.2	W 4	7.2	50	> 50	00	0	0	0	0	9	0	0	3	
	15	1004.2	0	6.7	49	> 50	00	0	0	0	0	9	0	0	3	
	18	1003.3	E 1	6.3	8.6	..	64	> 50	01	0	2	0	0	9	0	3	3	0.0
	21	1003.3	E 2	4.6	72	> 50	01	0	2	0	0	9	0	3	3	
19	00	1004.4	0	3.0	83	> 50	01	0	2	2	0	8	7	0	4	
	03	1005.5	0	2.3	86	> 50	01	0	2	2	0	7	7	0	3	
	06	1006.3	W 7	5.1	..	1.4	62	> 50	01	0	2	2	2	7	2	0	3	0.0
	09	1009.0	W 7	6.0	59	> 50	01	0	2	2	2	7	0	0	4	
	12	1009.0	W 7	6.8	47	> 50	00	0	1	0	0	9	0	1	3	
	15	1009.0	W 6	7.2	46	> 50	00	0	0	0	0	9	0	0	3	
	18	1008.6	W 3	8.8	9.3	..	39	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1007.7	0	6.2	66	> 50	01	0	0	4	2	7	0	6	8	
20	00	1005.7	0	6.0	70	> 50	01	0	0	3	0	9	0	6	9	
	03	1006.5	W 6	6.1	78	> 50	01	0	0	4	2	7	0	0	3	
	06	1007.1	W 10	4.7	..	4.7	55	> 50	02	1	0	3	2	7	0	0	3	0.0
	09	1009.5	W 7	3.5	58	> 50	01	1	2	2	0	7	5	0	4	
	12	1009.7	W 9	4.5	54	> 50	01	0	1	1	0	7	5	0	3	
	15	1012.2	W 4	4.9	48	> 50	01	0	1	1	0	7	5	0	4	
	18	1012.6	W 6	4.8	8.8	..	48	> 50	01	0	1	2	2	6	0	0	3	0.0
	21	1014.1	W 8	5.2	45	> 50	01	0	1	1	2	6	0	0	3	
21	00	1014.2	W 7	2.9	60	> 50	01	0	2	2	4	6	0	0	3	
	03	1014.8	W 4	3.0	59	20-50	02	1	6	6	0	6	5	0	3	
	06	1015.6	W 4	3.0	..	2.0	66	20-50	02	1	6	6	0	6	7	0	3	0.0
	09	1016.7	W 6	3.0	68	20-50	03	2	7	8	0	6	7	0	3	
	12	1018.3	W 6	3.7	61	20-50	03	2	8	8	0	6	7	0	3	
	15	1019.7	W 8	3.8	54	20-50	03	2	8	8	0	7	7	0	3	
	18	1020.3	W 8	3.2	6.1	..	49	> 50	02	2	7	7	0	7	7	0	3	0.0
	21	1021.7	W 8	3.0	52	> 50	02	2	6	6	0	7	6	0	3	
22	00	1022.8	W 7	2.0	57	> 50	02	2	5	4	0	7	6	0	3	
	03	1023.2	W 4	0.8	69	> 50	02	2	6	5	0	7	4	0	3	
	06	1023.2	W 4	1.2	..	0.6	72	20-50	02	2	6	6	0	7	4	0	3	0.0
	09	1023.1	W 4	1.6	71	20-50	02	2	4	1	1	6	4	0	8	
	12	1022.4	W 6	2.2	71	20-50	02	2	7	7	0	7	7	0	8	
	15	1020.9	W 7	3.5	59	20-50	02	2	7	7	0	7	7	0	8	
	18	1020.2	W 7	3.0	3.6	..	55	20-50	02	2	4	4	2	7	4	0	8	0.0
	21	1019.0	W 4	3.6	44	20-50	02	2	4	4	0	7	4	0	8	
23	00	1017.8	W 4	2.3	58	20-50	02	2	4	4	0	7	4	0	8	
	03	1016.6	W 3	1.2	72	> 50	02	2	6	4	0	7	4	0	8	
	06	1016.2	W 4	0.4	..	÷ 0.1	73	20-50	02	2	4	2	5	6	4	0	8	0.0
	09	1016.1	W 4	0.6	70	20-50	02	2	4	2	5	6	4	0	8	
	12	1013.4	W 6	1.0	60	20-50	02	2	4	2	2	7	7	0	9	
	15	1010.1	W 9	1.4	58	> 50	02	2	4	4	2	7	7	0	8	
	18	1009.7	W 5	2.0	3.8	..	53	> 50	02	2	5	4	2	7	7	0	8	0.0
	21	1009.1	W 5	1.5	61	> 50	02	2	7	2	2	7	7	0	8	
24	00	1008.1	W 6	1.5	69	> 50	02	2	7	7	0	8	7	0	8	
	03	1007.2	W 5	0.9	54	> 50	02	2	8	8	0	8	7	0	8	
	06	1006.3	W 3	0.4	..	÷ 0.1	57	> 50	02	2	8	8	0	8	7	0	8	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1005.8	W 3	1.0	57	> 50	03	2	8	8	0	9	2	0	8	
	12	1005.2	W 3	1.8	54	> 50	03	2	8	8	0	9	2	0	8	
	15	1003.9	W 3	2.8	44	> 50	03	2	8	8	0	9	2	0	8	
	18	1003.5	0	2.9	2.9	..	53	> 50	03	2	8	8	0	9	7	0	8	0.0
	21	1003.1	0	2.9	55	> 50	02	2	7	7	0	9	7	0	8	
25	00	1002.7	0	1.9	58	> 50	02	2	7	7	0	9	7	0	8	
	03	1002.8	0	1.2	63	> 50	02	2	7	7	0	8	7	0	4	
	06	1003.0	0	0.9	..	0.7	75	> 50	02	2	7	7	0	8	7	0	3	0.0
	09	1003.1	0	2.1	78	> 50	02	2	7	7	0	8	7	0	3	
	12	1003.7	0	2.9	82	> 50	02	2	7	7	0	8	7	0	3	
	15	1004.2	E 2	1.8	81	> 50	02	2	4	5	0	7	7	0	3	
	18	1004.8	E 3	1.8	3.2	..	77	> 50	02	2	7	7	0	8	7	0	3	0.0
	21	1005.4	E 3	1.9	73	> 50	02	2	7	7	0	8	7	0	3	
26	00	1006.0	E 3	1.4	76	> 50	02	2	7	7	0	8	7	0	3	
	03	1006.0	E 3	1.2	80	> 50	03	2	8	8	0	8	7	×	3	
	06	1006.3	E 2	1.2	..	0.7	85	> 50	03	2	8	8	0	8	7	×	3	0.0
	09	1007.2	E 2	1.3	85	> 50	03	2	8	8	0	8	7	×	3	
	12	1009.2	E 2	1.3	86	> 50	03	2	8	8	0	8	7	×	4	
	15	1010.5	E 3	1.4	81	> 50	03	2	8	8	0	8	7	×	3	
	18	1010.5	E 4	2.0	2.2	..	77	> 50	02	2	6	6	0	8	7	0	3	0.0
	21	1009.1	E 3	1.1	88	> 50	00	0	0	0	0	9	0	0	9	
27	00	1008.9	E 3	0.4	88	> 50	01	0	2	0	0	9	0	9	9	
	03	1006.8	E 3	÷ 1.0	97	> 50	01	0	2	0	0	9	0	9	8	
	06	1005.3	E 2	÷ 1.5	..	÷ 1.9	99	> 50	01	0	2	0	0	9	0	9	8	0.0
	09	1005.8	0	0.6	92	> 50	01	0	1	0	0	9	0	2	4	
	12	1005.0	E 2	1.3	82	> 50	01	0	4	0	0	9	0	6	9	
	15	1004.8	E 3	0.4	89	> 50	01	0	4	0	0	9	0	9	8	
	18	1003.6	E 3	0.6	1.6	..	88	> 50	02	2	7	7	0	8	7	0	8	0.0
	21	1001.8	E 3	0.0	92	> 50	02	2	6	6	0	8	7	4	8	
28	00	1001.8	E 3	0.3	94	> 50	02	2	6	6	0	8	7	0	3	
	03	1002.1	E 3	÷ 1.0	94	> 50	02	2	6	6	0	8	7	0	4	
	06	1002.5	E 2	÷ 1.8	..	÷ 1.8	96	> 50	02	2	4	4	5	4	7	0	3	0.0
	09	1003.6	E 3	÷ 1.4	98	> 50	02	2	7	7	0	8	7	×	3	
	12	1004.0	E 4	÷ 0.5	90	> 50	02	2	8	7	0	8	7	×	3	
	15	1003.9	E 4	0.3	82	> 50	02	2	8	8	0	8	7	×	3	
	18	1003.9	E 6	0.1	0.6	..	82	> 50	02	2	7	7	0	8	7	0	3	0.0
	21	1003.9	E 5	0.0	90	> 50	02	2	7	7	0	8	7	0	3	
29	00	1003.5	E 3	÷ 0.3	90	> 50	01	1	2	0	0	9	5	0	9	
	03	1003.1	E 1	÷ 1.8	93	> 50	01	0	2	0	0	9	5	8	8	
	06	1002.7	0	÷ 2.3	..	÷ 2.3	97	> 50	01	0	2	0	0	9	0	8	8	0.0
	09	1001.2	0	0.4	90	> 50	02	2	8	0	0	9	2	×	8	
	12	1002.0	W 7	4.5	82	> 50	61	2	8	2	5	4	2	×	4	
	15	1003.1	W 10	4.7	53	20—50	03	2	8	4	5	3	2	×	3	
	18	1004.1	W 10	4.5	4.9	..	49	20—50	02	2	6	5	5	6	0	×	3	0.2
	21	1004.4	W 7	3.8	42	20—50	01	0	2	2	0	8	1	0	3	
30	00	1005.0	W 5	÷ 1.2	56	20—50	01	0	4	4	0	8	1	0	3	
	03	1006.1	W 4	1.5	59	20—50	01	0	4	4	0	8	1	0	3	
	06	1007.3	W 6	1.0	..	÷ 2.1	55	20—50	01	0	3	3	0	8	4	0	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
	09	1007.5	0	2.3	53	> 50	00	0	0	0	0	9	0	0	3		
	12	1006.2	0	4.5	45	> 50	01	0	1	0	0	9	0	2	9		
	15	1005.9	0	3.5	55	> 50	01	0	1	0	0	9	0	2	8		
	18	1005.5	0	4.5	4.6	..	55	> 50	00	0	0	0	0	9	0	0	8	0.0	
	21	1005.5	0	3.0	65	> 50	00	0	0	0	0	9	0	0	3		
31	00	1005.9	0	0.0	80	> 50	01	0	3	0	0	9	0	2	4		
	03	1006.0	0	÷ 0.4	45	> 50	01	0	4	0	0	9	0	2	3		
	06	1006.2	0	0.6	..	÷ 1.0	80	> 50	02	2	6	0	0	9	0	7	3	0.0	
	09	1007.2	W 1	0.8	85	> 50	02	2	5	6	0	8	2	0	3		
	12	1008.0	W 1	4.0	61	> 50	01	1	4	0	0	9	0	2	3		
	15	1008.5	E 2	2.0	75	> 50	02	2	6	4	0	8	7	2	3		
	18	1009.5	W 11	6.2	6.4	..	55	> 50	02	1	7	7	2	8	7	×	4	0.0	
	21	1012.9	W 6	5.8	50	> 50	02	1	6	3	5	6	5	0	4		
	Mean	1007.7		4.1	3.6	6.0	1.6	73	12.0

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1016.2	W 4	5.4	45	> 50	02	1	6	1	5	2	0	2	3	
	03	1016.9	0	0.0	60	> 50	00	0	0	0	0	9	0	0	3	
	06	1017.5	0	÷ 0.3	..	÷ 1.0	60	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1017.6	0	0.7	70	> 50	00	0	0	0	0	9	0	0	0	
	12	1018.1	0	1.8	70	> 50	00	0	0	0	0	9	0	0	4	
	15	1017.7	S 2	1.4	70	> 50	00	0	0	0	0	9	0	0	8	
	18	1016.2	E 3	1.4	6.0	..	70	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1015.9	E 1	1.2	75	> 50	00	0	0	0	0	9	0	0	8	
2	00	1015.7	0	0.2	75	> 50	00	0	0	0	0	9	0	0	8	
	03	1015.6	0	÷ 1.8	75	> 50	00	0	0	0	0	9	0	0	6	
	06	1015.7	0	÷ 2.0	..	÷ 2.5	75	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1016.0	0	0.8	75	> 50	01	0	2	0	0	9	0	4	3	
	12	1015.5	W 1	1.9	65	20—50	01	0	4	0	0	9	0	4	9	
	15	1014.7	W 3	2.5	60	20—50	01	0	2	0	0	9	0	4	8	
	18	1014.3	W 2	2.7	3.0	..	58	> 50	01	0	2	0	0	9	0	9	8	0.0
	21	1014.0	0	1.8	60	> 50	02	1	4	0	0	9	6	0	5	
3	00	1014.0	0	0.0	60	> 50	00	1	0	0	0	9	0	0	3	
	03	1014.2	0	÷ 0.3	60	> 50	00	0	0	0	0	9	0	0	3	
	06	1014.5	0	÷ 0.1	..	÷ 2.4	65	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1015.2	0	1.7	65	> 50	00	0	0	0	0	9	0	0	3	
	12	1015.7	0	3.8	50	> 50	00	0	0	0	0	9	0	0	3	
	15	1015.5	E 3	2.9	50	> 50	01	0	2	0	0	9	0	2	9	
	18	1015.4	E 3	1.9	4.2	..	50	> 50	01	0	2	0	0	9	0	2	6	0.0
	21	1015.4	E 3	÷ 0.3	80	> 50	01	0	2	0	0	9	0	9	3	
4	00	1014.8	0	÷ 2.4	80	> 50	02	2	7	3	0	8	2	9	9	
	03	1013.7	0	÷ 1.7	80	> 50	02	2	7	7	0	8	7	0	8	
	06	1012.5	W 2	÷ 0.7	..	÷ 2.6	75	> 50	02	2	7	7	0	8	7	0	8	0.0
	09	1011.0	0	÷ 0.3	75	> 50	02	2	7	7	0	8	7	0	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1010.9	0	0.9	75	> 50	02	2	7	7	0	8	7	0	8	
	15	1010.1	W 5	2.7	65	> 50	02	2	6	7	0	8	7	0	8	
	18	1009.7	W 5	3.1	3.5	..	65	> 50	02	2	7	6	0	8	7	0	8	0.0
	21	1010.1	W 3	2.9	60	> 50	02	2	8	7	0	8	7	0	3	
5	00	1010.8	W 5	1.9	60	> 50	02	2	8	8	0	8	7	0	3	
	03	1011.4	W 5	0.6	65	> 50	02	2	8	8	0	8	7	0	3	
	06	1011.9	W 3	0.8	..	÷ 0.7	70	> 50	02	2	8	8	0	8	6	0	3	0.0
	09	1013.0	W 1	1.1	60	> 50	02	2	8	8	0	8	6	0	3	
	12	1013.2	W 1	1.4	60	> 50	02	2	8	8	0	8	6	0	1	
	15	1014.5	W 3	2.8	65	20-50	02	2	8	8	0	7	7	0	3	
	18	1014.9	W 3	3.0	3.1	..	65	20-50	02	2	8	8	0	7	7	0	3	0.0
	21	1016.4	W 3	2.1	65	20-50	02	2	7	7	0	7	7	0	4	
6	00	1017.3	W 3	1.8	70	20-50	02	2	6	6	0	7	7	0	3	
	03	1018.4	W 4	0.7	70	20-50	02	2	6	6	0	7	7	0	3	
	06	1019.0	W 4	0.0	..	0.0	70	> 50	02	2	6	6	0	8	8	0	3	0.0
	09	1020.3	W 3	1.0	65	> 50	02	2	7	7	0	7	7	0	3	
	12	1020.2	W 2	1.3	60	> 50	02	2	6	2	0	7	7	9	9	
	15	1020.0	W 1	1.8	2.9	..	58	> 50	01	0	2	1	0	8	7	9	8	
	18	1019.6	0	1.7	65	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1019.0	E 3	÷ 0.6	75	> 50	00	0	0	0	0	9	0	0	8	
7	00	1018.4	0	÷ 2.1	80	> 50	00	0	0	0	0	9	0	0	8	
	03	1017.1	0	÷ 2.8	83	> 50	00	0	0	0	0	9	0	0	8	
	06	1016.4	E 3	÷ 3.2	..	÷ 3.2	86	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1016.0	0	÷ 2.0	73	> 50	00	0	0	0	0	9	0	0	8	
	12	1015.0	0	÷ 1.2	71	> 50	00	0	0	0	0	9	0	0	8	
	15	1014.1	0	÷ 1.0	68	> 50	00	0	0	0	0	9	0	0	8	
	18	1013.7	W 1	÷ 0.2	1.7	..	60	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1013.8	W 3	÷ 0.4	56	> 50	00	0	0	0	0	9	0	0	6	
8	00	1014.3	W 5	÷ 1.5	51	> 50	01	0	3	0	0	9	0	6	3	
	03	1015.3	W 5	÷ 2.0	58	> 50	01	0	3	0	0	9	0	6	3	
	06	1016.1	W 9	÷ 2.7	..	÷ 3.2	58	20-50	02	2	8	4	5	6	0	6	3	0.0
	09	1017.1	W 9	÷ 2.5	60	20-50	02	2	8	5	0	7	6	0	3	
	12	1017.2	W 9	÷ 1.8	62	20-50	01	0	3	0	0	9	0	6	3	
	15	1017.0	W 8	÷ 0.6	59	20-50	01	0	3	0	0	9	0	6	9	
	18	1017.0	W 6	0.0	0.0	..	57	20-50	01	0	3	0	0	9	6	6	3	0.0
	21	1017.7	W 6	÷ 0.6	59	> 50	01	0	3	0	0	9	0	6	0	
9	00	1018.2	W 6	÷ 2.0	63	20-50	01	0	1	0	0	9	0	9	3	
	03	1018.2	W 4	÷ 3.6	68	20-50	01	0	1	0	0	9	0	9	3	
	06	1018.1	W 3	÷ 4.4	..	÷ 4.4	72	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1018.0	W 2	÷ 3.7	72	> 50	00	0	0	0	0	9	0	0	8	
	12	1018.0	W 4	÷ 3.0	69	> 50	00	0	0	0	0	9	0	0	3	
	15	1017.4	W 4	÷ 2.5	64	> 50	00	0	0	0	0	9	0	0	8	
	18	1017.0	W 5	÷ 2.2	÷ 0.1	..	60	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1017.2	W 5	÷ 3.3	57	> 50	00	0	0	0	0	9	0	0	3	
10	00	1017.8	W 5	÷ 4.6	56	> 50	00	0	0	0	0	9	0	0	3	
	03	1018.6	W 5	÷ 6.0	57	> 50	01	0	1	1	4	8	0	0	3	
	06	1019.1	W 4	÷ 6.6	..	÷ 6.6	58	> 50	01	0	2	2	5	7	0	0	3	0.0
	09	1019.7	W 3	÷ 5.0	62	20-50	01	0	2	2	5	7	0	0	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1020.0	E 3	÷ 5.0	70	20—50	02	2	6	6	5	7	0	0	3	
	15	1020.6	0	÷ 4.3	70	> 50	02	2	7	7	5	7	0	×	3	
	18	1020.9	0	÷ 3.7	÷ 2.2	..	68	> 50	03	2	7	7	5	7	0	×	3	0.0
	21	1021.2	E 3	÷ 4.4	83	> 50	03	2	8	8	5	7	0	×	3	
11	00	1022.2	E 6	÷ 5.5	92	1—2	72	7	8	8	5	4	×	×	3	
	03	1022.4	E 5	÷ 6.1	97	1—2	72	7	8	8	5	4	×	×	3	
	06	1022.6	E 3	÷ 6.6	..	÷ 6.9	98	2—4	72	7	8	8	5	4	×	×	3	0.3
	09	1022.8	E 5	÷ 5.8	93	2—4	72	7	8	8	5	4	×	×	3	
	12	1022.8	E 5	÷ 5.8	92	2—4	03	2	8	8	5	4	×	×	3	
	15	1022.8	E 5	÷ 5.6	89	2—4	03	2	8	8	5	4	×	×	3	
	18	1022.0	E 4	÷ 5.6	÷ 3.7	..	90	4—10	03	2	8	8	5	4	×	×	9	0.2
	21	1021.0	E 5	÷ 5.6	90	4—10	03	2	8	8	5	4	×	×	8	
12	00	1020.7	E 3	÷ 5.6	88	4—10	03	2	8	8	5	4	×	×	8	
	03	1019.8	E 3	÷ 5.6	79	10—20	03	2	8	8	5	5	×	×	8	
	06	1018.3	0	÷ 6.0	..	÷ 7.0	72	20—50	01	2	4	4	5	7	0	0	8	0.0
	09	1017.8	0	÷ 7.2	76	20—50	01	2	4	4	5	7	0	0	8	
	12	1017.2	0	÷ 6.6	76	20—50	01	0	4	4	0	9	5	0	8	
	15	1016.1	E 3	÷ 7.0	72	20—50	00	0	0	0	0	9	0	0	8	
	18	1014.7	E 2	÷ 7.0	÷ 5.4	..	74	20—50	00	0	0	0	0	9	0	0	8	0.0
	21	1012.9	0	÷ 7.5	70	20—50	00	0	0	0	0	9	0	0	8	
13	00	1011.3	0	÷ 8.7	73	20—50	00	0	0	0	0	9	0	0	8	
	03	1009.2	0	÷ 8.6	73	20—50	00	0	0	0	0	9	0	0	8	
	06	1007.7	W 1	÷ 8.1	..	÷ 8.7	73	20—50	03	0	8	8	0	8	2	×	8	0.0
	09	1006.2	W 3	÷ 7.6	72	20—50	01	1	4	0	0	9	0	5	8	
	12	1005.5	W 4	÷ 6.3	68	20—50	01	1	4	0	0	9	0	5	8	
	15	1002.8	W 5	÷ 4.6	60	20—50	01	1	3	0	0	9	0	5	8	
	18	1002.3	W 4	÷ 3.4	÷ 3.0	..	58	20—50	01	0	3	3	5	8	0	0	8	0.0
	21	1001.2	W 3	÷ 4.0	65	> 50	02	1	6	6	4	8	0	0	8	
14	00	1001.2	W 4	÷ 3.3	60	> 50	02	1	7	7	5	8	0	×	3	
	03	1001.2	W 5	÷ 3.4	56	> 50	02	1	7	7	5	8	0	×	3	
	06	1001.7	W 4	÷ 3.5	..	÷ 8.4	60	> 50	02	2	7	7	5	8	0	×	3	0.0
	09	1002.2	W 3	÷ 2.8	60	> 50	02	2	4	4	5	8	0	0	3	
	12	1003.2	W 4	÷ 1.0	56	> 50	02	2	4	4	5	8	0	0	3	
	15	1003.4	W 3	÷ 1.0	55	> 50	01	0	1	0	5	9	0	0	3	
	18	1005.1	E 8	÷ 4.6	÷ 0.8	..	70	> 50	01	0	2	2	0	8	4	0	3	0.0
	21	1006.0	E 4	÷ 6.2	82	> 50	01	0	1	1	0	8	4	0	3	
15	00	1006.0	E 4	÷ 7.0	86	> 50	01	0	1	1	5	7	0	0	3	
	03	1006.0	E 4	÷ 7.4	92	> 50	01	0	1	1	5	7	0	0	3	
	06	1006.0	E 5	÷ 8.2	..	÷ 8.2	90	> 50	01	0	1	1	5	7	0	0	3	0.0
	09	1005.8	E 4	÷ 8.4	92	> 50	01	0	1	1	5	7	0	0	8	
	12	1005.4	E 1	÷ 8.4	85	> 50	01	0	2	0	0	0	0	0	8	
	15	1005.0	0 ¹	÷ 7.2	82	> 50	01	0	3	0	0	0	0	8	8	
	18	1004.5	0	÷ 7.1	÷ 4.6	..	82	20—50	03	2	8	0	0	9	0	8	8	0.0
	21	1003.9	0	÷ 6.3	80	10—20	03 ²	2	8	0	0	9	0	7	8	
16	00	1003.6	0	÷ 7.0	98	0.05—0.2	77	7	9	9	×	0	×	7	8	
	03	1003.0	W 3	÷ 7.0	99	0.05—0.2	77	7	9	9	×	0	×	×	8	
	06	1002.7	W 1	÷ 6.5	..	÷ 8.7	100	0.05—0.2	77	7	9	9	×	0	×	×	8	7.5
	09	1002.2	W 3	÷ 5.8	100	0.05—0.2	77	7	9	9	×	0	×	×	8	

¹ From 1300 calm. ² 2200 Fog coming from W, snow began 2230.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1001.8	W 4	÷ 5.0	100	0.05—0.2	77	7	9	9	×	0	×	×	8	
	15	1001.5	W 4	÷ 4.0	100	0.05—0.2	77	7	9	9	×	0	×	×	8	
	18	1001.2	W 5	÷ 3.1	÷ 3.0	..	100	0.05—0.2	77	7	9	9	×	0	×	×	8	7.5
	21	1001.8	W 6	÷ 3.1	100	0.05—0.2	77	7	9	9	×	0	×	×	3	
17	00	1002.3	W 8	÷ 4.2	100	0.05—0.2	77	7	9	9	×	0	×	×	3	
	03	1004.0	W 8	÷ 5.1	100	0.05—0.2	77	7	9	9	×	0	×	×	3	
	06	1005.6	W 9	÷ 5.2	..	÷ 6.5	100	0.05—0.2	76	7	9	9	×	0	×	×	3	7.0
	09	1007.1	W 7	÷ 5.2	100	0.05—0.2	76	7	9	9	×	0	×	×	3	
	12	1008.2	W 7	÷ 5.3	100	0.05—0.2	76	7	9	9	×	0	×	×	3	
	15	1009.2	W 7	÷ 5.3	100	0.05—0.2	39	7	9	9	×	0	×	×	3	
	18	1009.7	W 5	÷ 5.5	÷ 2.8	..	100	0.05—0.2	39	3	9	9	×	0	×	×	3	5.3
	21	1010.1	W 5	÷ 6.6	100	0.05—0.2	39	3	8	8	5	4	×	×	3	
18	00	1011.5	W 5	÷ 7.2	95	1—2	03	3	8	8	5	5	×	×	3	
	03	1012.7	W 5	÷ 7.6	90	1—2	03	3	8	8	5	5	×	×	3	
	06	1013.7	W 5	÷ 7.8	..	÷ 7.8	82	4—10	03	3	8	8	5	6	×	×	3	0.0
	09	1015.3	W 6	÷ 7.8	78	4—10	03	7	8	8	5	6	×	×	3	
	12	1016.3	W 6	÷ 7.8	74	4—10	03	3	8	8	5	6	×	×	3	
	15	1016.4	W 6	÷ 7.5	68	4—10	03	3	8	8	5	6	×	×	3	
	18	1018.0	W 5	÷ 7.2	÷ 5.5	..	64	10—20	03	3	8	8	0	7	2	×	3	0.0
	21	1018.0	W 8	÷ 7.6	58	10—20	03	3	8	8	0	7	2	×	3	
19	00	1018.6	W 7	÷ 7.5	56	10—20	03	3	8	8	0	7	2	×	3	
	03	1018.6	W 6	÷ 7.9	54	10—20	03	3	8	8	0	7	2	×	3	
	06	1018.4	W 5	÷ 8.2	..	÷ 8.7	54	10—20	36	3	8	8	0	7	2	×	3	0.0
	09	1017.8	W 1	÷ 10.0	54	20—50	01	0	3	3	0	7	2	1	8	
	12	1017.8	0	÷ 10.2	58	20—50	01	0	1	1	0	9	0	1	3	
	15	1017.0	0	÷ 10.8	62	> 50	00	0	0	0	0	9	0	0	9	
	18	1017.0	0	÷ 10.4	÷ 7.0	..	68	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1016.9	0	÷ 13.4	68	> 50	00	0	0	0	0	9	0	0	9	
20	00	1016.6	0	÷ 15.2	72	> 50	00	0	0	0	0	9	0	0	3	
	03	1016.9	0	÷ 15.3	76	> 50	00	0	0	0	0	9	0	0	3	
	06	1016.6	0	÷ 16.0	..	÷ 16.3	78	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1015.3	0	÷ 16.0	80	> 50	00	0	0	0	0	9	0	0	9	
	12	1015.1	0	÷ 13.2	78	> 50	00	0	0	0	0	9	0	0	8	
	15	1014.0	0	÷ 13.0	78	> 50	00	0	0	0	0	9	0	0	9	
	18	1013.2	0	÷ 14.2	÷ 9.8	..	76	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1012.2	0	÷ 15.5	80	20—50	01	0	2	2	0	8	6	0	9	
21	00	1011.1	0	÷ 15.5	86	> 50	01	0	2	2	0	8	6	0	9	
	03	1009.1	0	÷ 13.8	88	> 50	00	0	0	0	0	9	0	0	9	
	06	1008.9	0	÷ 9.8	..	÷ 16.0	84	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1009.6	SW 4	÷ 2.3	80	> 50	02	2	7	2	0	8	7	2	3	
	12	1012.2	W 16 ¹	÷ 2.8	80	10—20	02	3	7	7	0	7	7	0	3	
	15	1016.1	W 14	÷ 3.5	76	0.5—1	39	3	7	7	5	5	0	0	4	
	18	1018.1	W 8	÷ 6.5	÷ 1.8	..	68	10—20	01	3	6	2	2	6	7	0	3	0.0
	21	1018.7	W 4	÷ 3.5	60	20—50	01	3	2	2	2	3	0	0	3	
22	00	1018.2	W 1	÷ 8.2	62	20—50	01	3	3	3	2	7	0	0	9	
	03	1017.2	0	÷ 9.9	66	20—50	02	2	5	4	0	8	1	0	8	
	06	1015.6	E 2	÷ 10.0	..	÷ 13.8	70	20—50	02	2	6	6	0	8	1	0	8	0.0
	09	1014.0	0	÷ 10.2	72	20—50	01	0	3	2	0	8	5	0	8	

¹ The Gale began 1005 with 10 m/sec.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1011.4	0	÷10.5	72	20—50	01	0	3	0	0	9	0	9	8	
	15	1009.7	SE 6	÷11.2	74	20—50	01	0	3	0	0	9	0	9	8	
	18	1009.0	0	÷11.5	÷ 3.5	..	79	20—50	01	0	3	0	0	9	0	9	8	0.0
	21	1008.2	0	÷11.8	78	20—50	02	2	7	7	0	9	7	0	8	
23	00	1007.6	W 3	÷10.2	78	20—50	02	2	8	7	0	9	7	0	8	
	03	1008.0	W 12 ¹	÷ 4.3	99	0.2—0.5	39	3	8	8	5	2	×	×	4	
	06	1009.4	W 14	÷ 5.0	..	÷12.2	99	0.2—0.5	39	3	8	8	5	2	×	×	3	0.0
	09	1010.9	W 10	÷ 5.8	96	0.2—0.5	39	3	8	8	5	3	×	×	3	
	12	1011.4	W 15	÷ 7.2	80	0.5—1	37	3	8	8	5	5	×	×	3	
	15	1011.0	W 15	÷ 7.5	78	0.5—1	37	3	8	8	5	5	×	×	9	
	18	1011.2	W 16	÷ 8.0	÷ 3.9	..	85	0.2—0.5	39	3	8	8	5	2	×	×	3	0.0
	21	1011.8	W 15	÷ 8.8	96	0.2—0.5	39	3	8	8	5	1	×	×	3	
24	00	1012.0	W 17	÷10.0	100	< 0.05	76	7	8	8	5	0	×	×	3	
	03	1011.7	W 18	÷10.0	100	< 0.05	76	7	8	8	5	0	×	×	9	
	06	1011.5	W 18	÷ 9.6	..	÷10.4	100	< 0.05	76	7	8	8	5	0	×	×	8	0.0
	09	1011.9	W 17	÷ 9.9	100	< 0.05	76	7	8	8	5	0	×	×	3	
	12	1012.6	W 19	÷ 9.2	100	< 0.05	76	7	8	8	5	0	×	×	2	
	15	1013.4	W 18	÷ 8.9	100	< 0.05	76	7	8	8	5	0	×	×	3	
	18	1016.2	W 16	÷11.8	÷ 8.0	..	100	< 0.05	76	7	8	8	5	0	×	×	4	0.0
	21	1019.8	W 18	÷11.5	100	< 0.05	76	7	8	8	5	0	×	×	4	
25	00	1021.0	W 21	÷ 8.5	100	0.2—0.5	39	3	8	8	5	5	×	×	4	
	03	1021.8	W 16	÷ 7.6	100	0.2—0.5	39	3	8	8	5	5	×	×	3	
	06	1021.9	W 16	÷ 8.1	..	÷12.3	100	0.2—0.5	39	3	8	8	5	5	×	×	3	xx
	09	1022.7	W 8	÷ 7.8	100	1—2	02	3	8	8	5	5	×	×	3	
	12	1022.0	W 10	÷ 4.3	80	4—10	02	3	8	8	5	6	×	×	9	
	15	1021.7	W 3	÷ 4.9	66	10—20	02	3	4	4	5	7	7	0	8	
	18	1019.4	0	÷ 5.5	÷ 4.1	..	66	10—20	02	2	3	6	5	7	7	0	8	xx
	21	1016.1	0	÷ 8.0	70	10—20	02	2	3	6	5	7	7	0	9	
26	00	1013.1	0	÷ 8.6	72	10—20	02	0	3	6	5	7	7	0	8	
	03	1009.0	W 1	÷10.6	76	10—20	02	0	3	3	5	7	7	9	8	
	06	1008.0	0	÷11.5	..	÷11.8	76	10—20	02	2	6	6	0	7	7	0	8	0.0
	09	1006.7	0	÷11.1	78	10—20	02	2	7	7	0	7	7	×	8	
	12	1005.5	0	÷ 9.7	76	10—20	01	1	4	4	0	8	7	0	8	
	15	1004.0	W 1	÷ 7.2	76	20—50	02	2	7	7	0	8	7	0	8	
	18	1003.6	W 1	÷ 7.0	÷ 5.5	..	76	20—50	02	2	6	6	0	8	7	0	8	0.0
	21	1003.4	0	÷ 7.4	76	10—20	02	2	6	6	0	8	7	0	8	
27	00	1003.1	0	÷ 7.6	76	10—20	02	2	7	7	0	8	7	0	8	
	03	1003.1	0	÷ 4.0	71	10—20	01	0	2	2	0	8	7	0	3	
	06	1003.5	SW 1	÷ 2.5	..	÷11.5	52	10—20	02	2	4	4	0	8	7	0	3	0.0
	09	1004.2	0	÷ 2.0	62	10—20	02	2	6	6	0	9	7	0	3	
	12	1004.2	W 5	÷ 1.6	56	20—50	01	1	4	4	0	9	7	0	3	
	15	1004.8	0 ²	÷ 3.9	62	20—50	01	1	3	4	0	9	7	0	3	
	18	1005.1	0	÷ 5.1	÷ 1.1	..	68	20—50	01	1	2	2	0	9	0	9	3	0.0
	21	1005.3	0	÷ 7.6	71	20—50	01	0	2	2	0	8	5	0	3	
28	00	1005.3	0	÷ 9.6	72	20—50	01	0	2	2	0	8	5	0	3	
	03	1004.8	0	÷10.1	72	20—50	02	2	6	6	0	7	5	0	3	
	06	1003.7	0	÷ 9.0	..	÷10.3	72	10—20	02	2	7	7	0	7	5	0	8	0.0
	09	1004.2	W 1	÷ 7.8	80	10—20	03	2	8	8	0	7	2	×	4	

¹ The Gale began 0045. ² 1730 Light breeze from E.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1003.4	W 1	÷ 6.2	74	10—20	02	2	6	6	0	8	8	0	9	
	15	1003.4	W 5	÷ 4.2	54	10—20	02	2	4	4	0	8	8	0	3	
	18	1006.2	W 6	÷ 3.5	÷ 3.5	..	56	10—20	02	2	6	6	0	7	8	0	4	0.0
	21	1007.9	W 7	÷ 3.5	56	10—20	03	2	8	8	0	7	8	×	3	
29	00	1009.2	W 5	÷ 4.0	60	10—20	03	2	8	8	0	7	8	×	3	
	03	1010.1	W 4	÷ 3.5	60	10—20	03	2	8	8	0	7	8	×	3	
	06	1010.7	W 3	÷ 2.2	..	÷ 9.0	62	10—20	03	2	8	8	0	7	8	×	3	0.0
	09	1011.8	0 ¹	÷ 6.0	86	10—20	02	2	8	8	0	7	8	×	3	
	12	1013.2	0	÷ 6.0	84	10—20	02	2	7	7	0	7	8	0	3	
	15	1013.4	0	÷ 6.0	84	10—20	02	2	7	7	0	8	8	0	3	
	18	1013.6	0	÷ 6.0	÷ 2.0	..	87	10—20	02	2	7	7	0	8	8	0	3	
	21	1013.9	0	÷ 5.6	76	10—20	02	2	7	7	0	8	8	0	3	0.0
30	00	1014.0	0	÷ 6.5	75	10—20	01	0	2	2	4	7	8	0	3	
	03	1014.2	0	÷ 7.2	71	10—20	01	0	2	2	4	7	8	0	3	
	06	1014.3	SW 1	÷ 8.2	..	÷ 8.2	72	10—20	01	0	2	2	4	7	8	0	3	0.0
	09	1014.5	0	÷ 10.0	76	10—20	01	0	2	2	4	7	8	0	3	
	12	1014.2	0	÷ 10.6	70	10—20	01	2	2	2	0	8	8	0	9	
	15	1013.4	0	÷ 9.8	70	10—20	02	2	6	6	0	8	8	0	8	
	18	1012.2	0	÷ 9.0	÷ 5.4	..	68	20—50	02	2	7	7	0	8	8	0	8	0.0
	21	1010.8	SE 1	÷ 9.5	68	20—50	02	2	7	7	0	8	8	0	8	
Mean		1012.8		3.7	÷ 5.1	÷ 2.3	÷ 7.6	74	27.8

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1010.3	0	÷ 12.7	82	20—50	02	2	7	1	4	7	8	0	8	
	03	1009.8	0	÷ 14.0	86	10—20	02	2	4	4	0	8	8	0	8	
	06	1009.8	0	÷ 15.0	..	÷ 15.0	84	20—50	01	0	1	1	0	8	4	0	3	0.0
	09	1009.7	0	÷ 15.1	84	> 50	01	0	1	1	0	9	4	0	3	
	12	1009.8	0	÷ 14.5	82	> 50	00	0	0	0	0	9	0	0	3	
	15	1009.1	0	÷ 15.0	82	> 50	01	0	1	1	0	8	8	0	9	
	18	1008.7	0	÷ 15.0	÷ 9.0	..	78	> 50	02	1	6	6	0	8	7	0	8	0.0
	21	1008.2	0	÷ 14.9	75	> 50	02	1	6	6	0	8	7	0	8	
2	00	1008.2	0	÷ 13.5	75	> 50	02	1	6	6	0	8	7	0	3	
	03	1009.1	0	÷ 13.5	70	> 50	01	1	6	6	0	8	7	0	3	
	06	1010.2	W 1	÷ 13.5	..	÷ 15.8	70	> 50	01	1	2	2	0	8	7	0	3	0.0
	09	1010.9	0	÷ 14.2	72	> 50	01	1	2	2	0	8	7	0	3	
	12	1011.2	0	÷ 15.0	72	> 50	01	1	1	1	0	8	1	0	3	
	15	1011.6	0	÷ 15.2	72	> 50	01	1	1	1	0	8	1	0	3	
	18	1011.0	0	÷ 14.6	÷ 13.0	..	72	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1009.4	0	÷ 15.7	70	> 50	00	0	0	0	0	9	0	0	8	
3	00	1008.2	0	÷ 16.1	71	> 50	00	0	0	0	0	9	0	0	8	
	03	1007.0	0	÷ 16.1	70	> 50	00	0	0	0	0	9	0	0	8	
	06	1006.7	0	÷ 16.1	..	÷ 16.9	72	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1006.7	0	÷ 16.6	72	> 50	00	0	0	0	0	9	0	0	3	
	12	1006.7	0	÷ 16.2	72	> 50	03	2	8	0	0	9	1	0	3	

¹ 0645 Light breeze from E.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1006.1	0	÷14.4	72	20—50	03	2	8	2	5	4	2	×	9	
	18	1005.6	0	÷14.0	÷14.0	..	72	20—50	09	2	8	2	5	4	2	×	8	0.0
	21	1004.6	W 4	÷13.1	83	2—4	74	7	8	8	5	4	2	×	8	
4	00	1004.1	W 1	÷12.3	85	10—20	03	2	8	8	5	5	×	×	8	
	03	1004.2	W 2	÷12.0	80	2—4	72	7	8	8	5	5	×	×	3	
	06	1005.0	W 2	÷11.5	..	÷17.0	80	1—2	74	7	8	8	5	4	×	×	3	0.5
	09	1007.4	W 1	÷10.5	80	1—2	72	7	8	8	5	5	×	×	3	
	12	1007.8	0	÷10.6	80	1—2	05	2	8	8	5	5	×	×	3	
	15	1010.1	0	÷10.0	÷9.9	..	78	1—2	05	2	6	8	5	5	×	×	3	
	18	1012.0	E 3	÷10.3	80	4—10	09	2	6	3	5	4	7	0	3	0.5
	21	1013.3	E 1	÷11.9	86	2—4	72	2	7	4	5	4	7	0	3	
5	00	1014.9	0	÷13.8	86	2—4	09	2	7	4	5	5	7	0	3	
	03	1015.7	0	÷14.4	83	2—4	09	2	7	4	5	5	0	0	3	
	06	1016.5	0	÷15.0	..	÷15.1	80	10—20	01	0	3	3	5	6	0	0	3	0.0
	09	1017.9	0	÷14.5	86	10—20	01	0	4	4	5	6	0	0	3	
	12	1018.9	0	÷14.8	85	> 50	01	0	4	3	5	6	7	0	3	
	15	1019.4	0	÷14.8	86	> 50	01	0	3	3	0	8	5	0	3	
	18	1020.0	0	÷15.0	÷10.0	..	86	> 50	01	0	3	1	5	8	5	0	3	0.0
	21	1020.8	0	÷16.0	86	> 50	01	0	4	2	4	7	5	0	3	
6	00	1021.2	0	÷16.9	84	20—50	02	0	4	4	0	9	7	0	3	
	03	1022.3	0	÷17.0	80	20—50	01	0	2	2	5	7	0	0	3	
	06	1022.7	W 1	÷18.0	..	÷19.3	78	20—50	01	0	3	2	5	7	7	0	3	0.0
	09	1024.3	W 2	÷17.7	82	20—50	02	2	5	1	5	7	7	0	3	
	12	1025.2	W 3	÷18.0	78	20—50	01	1	2	1	5	7	7	0	3	
	15	1026.5	W 2	÷17.5	72	20—50	01	1	2	1	5	7	7	0	3	
	18	1026.9	W 2	÷17.7	÷15.2	..	70	> 50	02	2	6	6	0	9	8	0	3	0.0
	21	1027.2	W 5	÷16.0	64	> 50	02	2	6	6	0	9	8	0	3	
7	00	1027.8	W 5	÷15.6	65	> 50	02	2	7	7	0	9	8	0	3	
	03	1028.5	W 8	÷15.2	61	20—50	03	2	8	8	0	8	7	0	3	
	06	1028.8	W 8	÷15.1	..	÷18.1	64	20—50	03	2	8	8	0	8	7	×	3	0.0
	09	1030.5	W 4	÷15.2	64	2—4	03	2	7	4	5	4	7	×	3	
	12	1030.7	W 4	÷15.5	65	4—10	03	2	7	2	5	5	7	0	3	
	15	1031.2	W 3	÷15.0	65	4—10	03	2	7	7	0	8	7	0	3	
	18	1031.3	W 3	÷15.1	÷14.8	..	66	10—20	03	2	8	8	0	8	2	0	3	0.0
	21	1031.7	W 4	÷15.5	70	10—20	03	2	8	8	0	8	2	×	3	
8	00	1032.4	W 1	÷15.5	72	10—20	72	7	8	8	0	8	2	×	3	
	03	1033.2	0	÷15.0	72	10—20	03	2	8	8	0	8	2	×	3	
	06	1033.6	0	÷15.0	..	÷15.6	70	10—20	03	2	8	8	0	8	2	×	3	0.0
	09	1034.0	0	÷15.5	70	10—20	03	2	8	8	0	8	2	×	3	
	12	1034.4	SW 1	÷16.1	70	20—50	02	1	4	4	0	8	4	0	3	
	15	1034.7	0	÷17.3	74	> 50	00	0	0	0	0	9	0	0	3	
	18	1034.6	0	÷18.0	÷14.9	..	70	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1033.2	0	÷18.9	70	> 50	00	0	0	0	0	9	0	0	9	
9	00	1031.2	0	÷19.9	68	> 50	00	0	0	0	0	9	0	0	8	
	03	1029.4	0	÷20.3	70	> 50	00	0	0	0	0	9	0	0	8	
	06	1026.9	0	÷21.0	..	÷21.0	71	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1025.5	W 2	÷21.0	71	> 50	02	2	6	6	8	8	0	0	8	
	12	1021.7	WSW 4	÷19.7	68	> 50	02	2	7	7	0	8	2	0	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1020.1	W 4	÷15.4	66	20—50	03	2	7	7	0	8	2	0	8	
	18	1018.4	W 10	÷14.0	÷13.8	..	62	10—20	03	2	7	7	0	8	2	0	8	0.0
	21	1018.2	W 7	÷13.1	55	4—10	03	2	8	8	5	5	×	×	7	
10	00	1017.6	W 10	÷13.0	58	4—10	03	2	8	8	5	5	×	×	8	
	03	1016.3	W 10	÷13.5	54	4—10	03	2	8	8	5	5	×	×	8	
	06	1016.9	W 8	÷13.5	..	÷21.9	65	2—4	74	2	8	8	5	4	×	×	4	9.7
	09	1015.0	W 7	÷13.5	70	2—4	03	2	8	8	5	5	×	×	9	
	12	1015.5	ESE 1	÷16.1	82	1—2	09	1	4	4	8	5	0	0	4	
	15	1015.0	NE 3	÷16.9	81	2—4	02	2	4	3	8	5	1	0	9	
	18	1014.1	0	÷17.7	÷12.7	..	84	1—2	74	7	6	5	8	5	1	0	8	9.1
	21	1013.6	SE 3	÷17.3	80	1—2	03	2	6	5	8	5	1	0	8	
11	00	1012.8	0	÷18.0	82	1—2	74	2	7	7	5	5	0	×	8	
	03	1011.9	0	÷20.6	88	4—10	00	0	0	0	0	9	0	0	8	
	06	1011.9	0	÷22.5	..	÷22.5	82	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1011.6	0	÷23.2	78	> 50	02	1	6	6	5	6	0	0	8	
	12	1011.7	0	÷20.1	77	> 50	02	1	4	4	8	6	0	0	3	
	15	1011.3	0	÷21.0	78	> 50	02	2	6	6	0	4	6	×	8	
	18	1011.1	W 7	÷20.0	÷17.1	..	77	2—4	71	7	8	8	5	×	5	×	8	0.1
	21	1011.1	W 2	÷18.7	78	2—4	77	7	8	8	5	×	5	×	3	
12	00	1010.9	0	÷18.2	78	2—4	77	7	8	8	5	×	5	×	8	
	03	1010.9	0	÷17.2	80	2—4	77	7	8	8	5	×	5	×	3	
	06	1011.1	0	÷17.0	..	÷24.0	82	1—2	77	7	8	8	5	5	×	×	3	—
	09	1010.9	0	÷17.1	84	0.5—1	77	7	8	8	5	5	×	×	8	
	12	1010.8	0	÷17.2	84	0.5—1	77	7	8	8	5	5	×	×	8	
	15	1010.7	SW 1	÷17.7	84	0.5—1	77	7	8	8	5	5	×	×	8	
	18	1010.6	SW 1	÷18.1	÷16.8	..	84	2—4	77	7	8	8	5	5	×	×	8	1.8 ¹
	21	1011.2	W 1	÷20.5	85	2—4	77	7	8	8	5	5	×	×	3	
13	00	1011.1	W 1	÷21.3	78	4—10	01	0	×	×	×	×	×	×	3	
	03	1010.3	0	÷22.0	78	4—10	01	0	×	×	×	×	×	×	8	
	06	1009.5	0	÷22.6	..	÷26.6	76	4—10	01	0	2	2	4	6	0	0	8	0.0
	09	1008.9	0	÷24.6	76	10—20	01	0	1	1	4	6	0	0	8	
	12	1006.8	0	÷25.0	76	20—50	00	0	0	0	0	9	0	0	8	
	15	1005.9	0	÷25.9	75	20—50	00	0	0	0	0	9	0	0	8	
	18	1004.8	0	÷26.6	÷18.0	..	75	> 50	01	0	1	1	4	6	0	0	8	0.0
	21	1004.4	0	÷26.6	78	> 50	01	0	1	1	4	6	0	0	8	
14	00	1004.1	0	÷26.5	78	> 50	01	0	1	1	4	6	0	0	8	
	03	1005.8	0	÷27.5	78	> 50	01	0	1	1	4	6	0	0	3	
	06	1006.2	0	÷27.0	..	÷28.1	78	10—20	02	2	7	7	5	7	0	0	3	0.0
	09	1007.7	0	÷27.0	78	10—20	02	2	7	7	5	7	0	0	3	
	12	1007.7	0	÷23.5	77	10—20	03	2	8	8	5	5	×	×	3	
	15	1009.0	0	÷22.5	76	4—10	03	2	8	8	5	4	×	×	3	
	18	1009.6	0	÷22.0	÷22.0	..	76	4—10	03	2	8	8	5	4	×	×	3	0.0
	21	1010.5	0	÷21.0	74	4—10	03	2	8	8	5	5	×	×	3	
15	00	1010.6	0	÷20.6	74	4—10	03	3	8	8	5	5	×	×	3	
	03	1010.7	0	÷20.5	74	4—10	03	3	8	8	5	5	×	×	3	
	06	1009.0	W 4	÷19.0	..	÷27.3	73	4—10	03	3	8	8	5	5	×	×	9	0.0
	09	1008.1	W 5	÷19.5	76	4—10	73	3	8	8	5	5	×	×	8	
	12	1005.9	W 4	÷19.4	76	0.5—1	38	3	8	8	5	5	×	×	8	

¹ Precipitation for 24 hours.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1004.1	W 5	÷18.3	76	10—20	03	3	8	6	5	6	7	×	8	
	18	1003.1	W 8	÷16.5	÷16.3	..	76	0.5—1	37	3	8	6	5	5	7	×	8	trace
	21	1001.2	W 9	÷17.0	74	4—10	02	2	8	2	5	5	7	×	8	
16	00	1000.6	W 9	÷17.3	72	10—20	01	0	2	2	0	7	5	0	8	
	03	1000.2	W 8	÷18.8	70	20—50	00	0	0	0	0	9	0	0	8	
	06	999.9	W 5	÷19.0	..	÷19.7	68	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	999.6	W 6	÷19.5	68	> 50	01	0	1	1	5	5	0	0	8	
	12	999.2	W 6	÷19.5	68	> 50	01	0	4	1	5	5	0	2	8	
	15	999.0	W 6	÷18.8	68	> 50	02	2	6	1	5	6	5	0	8	
	18	998.7	W 5	÷18.0	÷16.5	..	68	> 50	02	2	7	1	5	6	2	0	8	0.0
	21	1001.1	W 8	÷14.3	70	10—20	03	3	7	7	5	5	×	×	4	
17	00	1001.2	W 7	÷14.6	60	10—20	02	2	7	7	0	7	7	×	3	
	03	1001.4	W 8	÷14.0	62	10—20	02	3	7	7	0	7	7	×	3	
	06	1001.8	W 9	÷13.4	..	÷19.8	62	10—20	02	3	7	7	0	7	7	×	3	0.0
	09	1002.2	W 8	÷13.4	64	10—20	02	3	8	7	6	7	2	×	3	
	12	1003.1	W 7	÷13.0	64	10—20	02	2	7	4	6	7	2	0	3	
	15	1003.4	SW 4	÷12.3	62	10—20	02	2	7	7	0	7	7	0	3	
	18	1003.9	0	÷13.1	÷12.0	..	68	10—20	02	2	7	7	0	7	7	0	3	0.0
	21	1004.7	0	÷18.9	76	10—20	02	2	4	4	0	7	7	0	3	
18	00	1005.0	0	÷18.6	78	10—20	00	0	0	0	0	9	0	0	3	
	03	1004.9	0	÷17.3	73	20—50	00	0	0	0	0	9	0	0	9	
	06	1004.9	0	÷16.0	..	÷19.3	60	> 50	01	0	3	0	0	9	0	6	8	
	09	1004.9	0	÷16.3	66	> 50	01	1	2	2	0	7	1	0	3	
	12	1004.1	0	÷17.0	66	> 50	01	1	2	2	0	7	1	0	9	
	15	1003.3	W 1	÷17.5	68	> 50	02	2	8	8	0	7	2	×	8	
	18	1002.9	W 1	÷17.5	÷13.0	..	68	> 50	03	3	8	8	0	7	2	×	8	0.0
	21	1002.3	W 1	÷17.0	68	> 50	03	3	8	8	0	7	2	×	8	
19	00	1001.9	W 3	÷16.5	75	0.2—0.5	73	7	8	8	5	5	×	×	8	
	03	1001.9	W 4	÷16.0	80	0.2—0.5	73	7	8	8	5	5	×	×	3	
	06	1000.6	W 1	÷15.5	..	÷18.0	82	0.5—1	73	7	8	8	5	5	×	×	9	0.4
	09	1001.8	0	÷17.4	86	4—10	01	2	4	3	0	7	2	2	3	
	12	1002.8	0	÷17.6	88	4—10	02	2	8	8	0	7	7	×	3	
	15	1003.2	0	÷19.4	88	10—20	01	1	4	4	0	7	7	0	3	
	18	1003.9	0	÷20.0	÷15.2	..	87	20—50	01	1	1	1	0	7	7	0	3	0.0
	21	1005.4	0	÷20.9	88	20—50	01	1	1	1	0	7	7	0	3	
20	00	1006.7	0	÷21.9	85	20—50	00	0	0	0	0	9	0	0	3	
	03	1007.3	0	÷22.1	80	20—50	00	0	0	0	0	9	0	0	3	
	06	1007.9	0	÷22.5	..	÷22.5	76	20—50	00	0	0	0	0	9	0	0	3	0.0
	09	1007.9	0	÷22.0	75	20—50	00	0	0	0	0	9	0	0	3	
	12	1009.2	0	÷23.0	75	20—50	00	0	0	0	0	9	0	0	3	
	15	1009.2	0	÷23.0	74	20—50	00	0	0	0	0	9	0	0	3	
	18	1009.3	0	÷23.5	÷20.0	..	71	20—50	00	0	0	0	0	9	0	0	3	0.0
	21	1008.3	0	÷24.5	70	20—50	00	0	0	0	0	9	0	0	9	
21	00	1007.2	0	÷24.8	72	20—50	00	0	0	0	0	9	0	0	9	
	03	1006.2	W 3	÷24.1	73	20—50	00	0	0	0	0	9	0	0	8	
	06	1005.0	W 1	÷24.6	..	÷25.2	70	20—50	00	0	0	0	0	9	0	0	8	0.0
	09	1003.8	W 1	÷24.1	71	20—50	02	2	6	1	4	7	7	0	8	
	12	1003.1	W 1	÷22.5	70	20—50	03	2	8	8	0	7	7	×	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1002.2	0	÷20.1	70	20-50	02	2	7	7	0	7	7	×	8	
	18	1002.1	0	÷21.1	÷20.0	..	70	20-50	02	2	6	6	0	7	4	0	8	0.0
	21	1002.5	0	÷22.3	70	20-50	01	0	1	1	0	7	4	0	4	
22	00	1002.8	0	÷23.0	78	20-50	01	0	1	1	0	7	4	0	3	
	03	1002.7	0	÷22.5	78	20-50	01	0	1	1	0	7	4	0	9	
	06	1002.5	0	÷22.5	..	÷24.7	78	20-50	01	0	1	1	0	7	4	0	9	0.0
	09	1002.8	0	÷18.2	74	20-50	02	0	6	6	0	7	7	0	4	
	12	1003.7	W 6 ¹	÷18.5	62	20-50	02	0	6	6	0	7	7	0	3	
	15	1004.9	W 4	÷18.3	60	20-50	02	0	4	4	0	7	7	0	3	
	18	1005.0	W 6	÷19.5	÷19.8	..	68	20-50	02	0	4	4	0	7	7	0	3	0.0
	21	1006.3	W 10	÷14.7	68	20-50	02	2	6	6	0	7	7	0	3	
23	00	1009.0	W 10	÷15.5	70	20-50	02	2	6	4	0	7	7	0	3	
	03	1011.0	W 9	÷16.1	70	20-50	02	2	4	4	0	7	7	0	3	
	06	1013.2	W 8	÷17.0	..	÷22.5	71	20-50	02	2	4	4	0	7	7	0	3	0.0
	09	1014.5	W 8	÷17.4	62	20-50	01	1	2	2	0	7	7	0	3	
	12	1016.6	W 7	÷18.0	62	20-50	01	1	2	2	0	7	7	0	3	
	15	1016.5	SW 3 ²	÷18.5	60	20-50	01	1	2	2	0	7	7	0	3	
	18	1016.6	WSW 1	÷18.5	÷13.2	..	58	20-50	01	1	2	2	0	7	7	0	3	0.0
	21	1015.6	0	÷21.0	60	20-50	00	0	0	0	0	9	0	0	9	
24	00	1015.1	W 1	÷21.9	62	20-50	00	0	0	0	0	9	0	0	8	
	03	1015.1	0	÷23.5	64	20-50	00	0	0	0	0	9	0	0	3	
	06	1015.1	0	÷23.6	..	÷23.6	64	20-50	00	0	0	0	0	9	0	0	3	0.0
	09	1015.1	0	÷24.5	66	20-50	00	0	0	0	0	9	0	0	3	
	12	1015.1	0	÷25.0	67	20-50	00	0	0	0	0	9	0	0	3	
	15	1015.1	0	÷24.6	67	20-50	01	0	1	1	4	7	7	0	3	
	18	1015.3	0	÷24.8	÷18.5	..	70	> 50	01	0	1	1	0	7	4	0	3	0.0
	21	1015.4	0	÷25.8	70	> 50	01	0	1	1	0	7	4	0	3	
25	00	1015.1	0	÷26.8	75	> 50	00	0	0	0	0	9	0	0	9	
	03	1013.6	0	÷27.4	76	> 50	00	0	0	0	0	9	0	0	8	
	06	1012.2	0	÷28.0	..	÷28.0	77	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1011.2	0	÷28.0	76	> 50	01	0	1	1	0	6	5	0	8	
	12	1010.0	0	÷27.9	77	> 50	01	0	1	1	0	7	5	0	8	
	15	1009.1	0	÷25.8	76	> 50	01	0	3	3	0	7	5	0	8	
	18	1007.9	W 1	÷24.6	÷24.3	..	78	> 50	01	0	1	1	0	7	4	0	8	0.0
	21	1007.1	W 2	÷22.3	76	> 50	01	0	1	1	0	7	4	0	8	
26	00	1007.0	0	÷21.5	71	> 50	01	0	2	2	0	7	6	0	8	
	03	1006.7	0	÷21.2	70	> 50	00	0	0	0	0	9	0	0	8	
	06	1006.0	0	÷21.5	..	÷29.2	74	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1006.8	W 1	÷18.4	75	> 50	01	0	1	2	4	1	0	0	3	
	12	1008.5	W 1	÷17.9	76	> 50	02	2	7	7	0	7	2	0	3	
	15	1008.7	0	÷16.4	76	> 50	03	2	7	7	0	7	7	0	3	0.0
	18	1009.8	0	÷16.0	÷15.5	..	75	> 50	02	2	6	6	0	7	7	0	3	
	21	1010.8	0	÷18.1	76	> 50	02	2	4	4	0	7	7	0	3	
27	00	1011.1	0	÷19.0	75	> 50	01	2	3	3	0	7	7	0	3	
	03	1011.5	0	÷19.2	75	> 50	00	0	0	0	0	9	0	0	3	
	06	1010.8	0	÷19.5	..	÷21.7	74	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1010.5	0	÷20.2	74	> 50	00	0	0	0	0	9	0	0	8	
	12	1009.4	0	÷20.2	74	> 50	00	0	0	0	0	9	0	0	8	

¹ 0945 Wind gust 24 m/sec. ² Calm 1400.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
28	15	1008.6	0	÷20.3	74	> 50	01	0	3	3	0	7	6	0	8	0.0
	18	1008.2	0	÷21.1	÷15.8	..	74	> 50	01	0	3	3	0	7	6	0	8	
	21	1006.3	0	÷21.2	76	> 50	01	0	3	3	0	7	6	0	8	
	00	1005.6	W 1	÷20.9	75	> 50	01	0	3	2	0	7	6	0	8	
	03	1004.7	W 1	÷22.0	73	> 50	00	0	0	0	0	9	0	0	8	
	06	1003.1	0	÷22.1	74	> 50	00	0	0	0	0	9	0	0	8	
29	09	1003.3	0	÷23.1	75	> 50	00	0	0	0	0	9	0	0	4	0.0
	12	1003.9	W 1	÷23.3	74	> 50	00	0	0	0	0	9	0	0	3	
	15	1003.0	W 1	÷22.1	71	> 50	00	0	0	0	0	9	0	0	9	
	18	1003.6	0	÷23.0	÷21.0	..	72	> 50	00	0	0	0	0	9	0	0	3	
	21	1004.3	0	÷23.5	71	> 50	00	0	0	0	0	9	0	0	3	
	00	1005.9	0	÷23.5	71	> 50	00	0	0	0	0	9	0	0	3	
30	03	1006.0	0	÷24.1	70	> 50	00	0	0	0	0	9	0	0	3	0.0
	06	1006.9	0	÷23.5	..	÷24.3	70	> 50	01	0	2	2	0	8	5	0	3	
	09	1007.5	0	÷24.5	70	> 50	01	0	1	1	0	8	5	0	3	
	12	1007.7	0	÷25.1	72	> 50	01	0	1	1	0	8	5	0	3	
	15	1008.0	0	÷26.5	73	> 50	01	0	1	1	0	8	5	0	3	
	18	1008.1	0	÷26.6	÷22.7	..	74	> 50	01	0	1	1	0	8	5	0	3	
31	21	1008.7	0	÷26.0	72	> 50	01	0	2	2	0	8	5	0	3	0.0
	00	1009.2	0	÷24.8	69	> 50	01	0	3	3	0	8	6	0	3	
	03	1011.1	0	÷25.0	68	> 50	00	0	0	0	0	9	0	0	3	
	06	1011.9	0	÷25.0	..	÷26.5	68	> 50	00	0	0	0	0	9	0	0	3	
	09	1012.9	0	÷25.0	68	> 50	01	0	1	1	0	9	4	0	3	
	12	1016.4	W 1	÷26.4	71	> 50	00	0	0	0	0	9	0	0	3	
31	15	1017.3	0	÷25.8	70	> 50	00	0	0	0	0	9	0	0	3	0.0
	18	1018.0	0	÷27.6	÷24.5	..	71	> 50	00	0	0	0	0	9	0	0	3	
	21	1018.6	0	÷26.9	72	> 50	00	0	0	0	0	9	0	0	3	
	00	1018.0	0	÷26.5	72	> 50	00	0	0	0	0	9	0	0	9	
	03	1016.3	0	÷26.8	72	> 50	00	0	0	0	0	9	0	0	8	
	06	1014.7	W 2	÷27.0	..	÷29.3	72	> 50	00	0	0	0	0	9	0	0	8	
31	09	1012.0	0	÷27.5	72	> 50	01	0	1	1	0	7	3	0	8	0.0
	12	1009.3	W 1	÷27.9	73	> 50	01	0	1	1	0	7	5	0	8	
	15	1017.7	NW 1	÷27.1	72	> 50	01	0	2	2	0	7	5	0	8	
	18	1005.6	WNW 2	÷26.4	÷26.2	..	72	> 50	01	0	2	2	0	7	5	0	8	
	21	1004.5	0	÷25.9	69	> 50	01	0	3	3	0	7	5	0	8	
	Mean	1011.1		1.6	÷19.3	÷16.8	÷21.7	74	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1004.1	W 3	÷14.5	66	> 50	01	0	3	3	0	7	5	0	8	0.0
	03	1004.1	W 12	÷16.3	52	20-50	00	0	0	0	0	9	0	0	3	
	06	1004.1	W 6	÷15.0	..	÷28.3	58	> 50	00	0	0	0	0	9	0	0	3	
	09	1004.1	NE 2	÷18.8	62	> 50	00	0	0	0	0	9	0	0	3	
	12	1004.8	W 1	÷20.4	68	> 50	01	0	4	3	0	6	6	9	3	
	15	1005.3	0	÷20.3	69	> 50	02	2	7	7	0	7	7	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1005.4	W 2	÷18.1	÷13.8	..	70	> 50	02	2	7	7	0	7	7	×	3	0.0
	21	1004.8	0	÷18.9	76	4-10	71	7	8	8	5	6	2	×	9	
2	00	1004.8	0	÷17.0	78	4-10	03	2	7	7	5	6	×	×	3	
	03	1004.0	0	÷13.0	73	10-20	02	2	4	4	5	6	0	0	9	
	06	1003.7	W 8	÷ 9.5	..	÷20.9	72	10-20	02	2	4	4	5	6	0	0	8	0.0
	09	1004.4	W 6	÷ 9.1	70	10-20	02	2	7	7	5	6	0	0	3	
	12	1004.6	W 5	÷ 9.0	68	10-20	02	2	7	7	5	6	0	0	3	
	15	1005.3	W 6	÷ 8.7	65	10-20	02	2	7	7	5	6	0	0	3	
	18	1006.4	W 6	÷ 9.7	÷ 8.7	..	68	10-20	02	2	7	7	5	6	0	0	3	0.0
	21	1009.5	0 ¹	÷15.8	78	10-20	02	2	7	7	5	6	0	0	4	
3	00	1010.4	0	÷16.7	81	10-20	02	2	7	7	5	6	0	0	3	
	03	1012.0	0	÷17.2	77	10-20	01	0	2	2	5	6	0	0	3	
	06	1013.0	0	÷18.5	..	÷23.1	78	10-20	00	0	0	0	0	9	0	0	3	0.0
	09	1014.5	0	÷20.5	76	10-20	01	0	1	1	4	6	0	0	3	
	12	1014.8	SW 1	÷22.3	75	10-20	01	0	1	1	0	7	5	0	3	
	15	1015.0	E 3	÷19.9	73	10-20	03	2	8	8	0	7	7	0	3	
	18	1015.1	E 4	÷19.4	÷ 9.7	..	74	10-20	03	2	8	8	0	7	2	×	3	0.0
	21	1015.1	E 4	÷19.9	76	10-20	03	2	8	8	0	7	2	×	3	
4	00	1015.7	E 3	÷20.3	76	10-20	72	7	8	8	0	7	2	×	3	
	03	1018.5	0	÷20.2	76	10-20	72	7	8	8	0	7	2	×	3	
	06	1019.8	0	÷22.0	..	÷27.0	76	20-50	02	2	6	6	0	7	2	0	3	0.1
	09	1020.6	0	÷22.1	78	20-50	02	2	6	6	4	7	0	0	3	
	12	1021.5	0	÷23.5	79	20-50	01	0	1	1	4	7	0	6	3	
	15	1021.9	0	÷24.8	80	20-50	01	0	1	1	0	9	0	6	3	
	18	1022.8	0	÷25.5	÷19.5	..	80	20-50	01	0	1	1	0	9	0	6	3	0.0
	21	1023.8	0	÷25.5	76	20-50	00	0	0	0	0	9	0	0	3	
5	00	1024.6	0	÷25.8	76	20-50	00	0	0	0	0	9	0	0	3	
	03	1024.8	0	÷27.1	76	20-50	00	0	0	0	0	9	0	0	3	
	06	1025.0	W 1	÷26.1	..	÷27.3	74	20-50	00	0	0	0	0	9	0	0	3	0.0
	09	1024.7	W 1	÷26.0	72	20-50	01	0	1	1	4	5	0	0	9	
	12	1023.2	W 3	÷25.5	70	20-50	01	0	1	1	4	5	0	0	8	
	15	1021.7	W 3	÷24.9	68	20-50	00	0	0	0	0	9	0	0	8	
	18	1020.2	W 8	÷23.3	÷23.1	..	66	20-50	02	1	4	4	0	7	7	0	8	0.0
	21	1022.0	0	÷20.8	63	20-50	00	0	0	0	0	9	0	0	4	
6	00	1025.0	0	÷24.3	68	20-50	00	0	0	0	0	9	0	0	4	
	03	1026.8	S 2	÷26.0	70	20-50	00	0	0	0	0	9	0	0	3	
	06	1028.4	0	÷26.0	..	÷26.2	71	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1030.7	W 1	÷26.3	72	20-50	00	0	0	0	0	9	0	0	3	
	12	1031.2	0	÷27.3	72	20-50	01	0	1	1	4	6	0	0	3	
	15	1031.2	W 1	÷27.6	73	20-50	01	0	1	1	4	6	0	0	3	
	18	1031.7	W 4	÷25.7	÷19.8	..	70	20-50	00	0	0	0	0	9	0	0	3	0.0
	21	1031.0	W 3	÷24.0	68	20-50	00	0	0	0	0	9	0	0	9	
7	00	1031.1	W 9	÷21.4	64	> 50	02	×	×	×	0	×	×	×	3	
	03	1030.6	W 10	÷19.4	61	20-50	03	2	8	8	0	×	×	×	6	
	06	1030.0	W 8	÷16.5	..	÷27.8	57	20-50	03	2	8	8	0	7	2	×	8	0.0
	09	1030.8	W 8	÷14.5	56	20-50	03	2	8	8	0	7	2	×	3	
	12	1031.1	W 10	÷12.3	51	20-50	03	2	8	8	0	7	2	×	3	
	15	1031.5	W 9	÷13.4	53	20-50	03	2	8	8	0	7	7	×	3	

¹ Wind shifted to E. 1850 and 2000 calm.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1031.9	W 8	÷13.7	÷12.0	..	54	20-50	03	2	7	7	0	7	7	×	3	0.0
	21	1032.9	W 9	÷13.5	51	20-50	03	2	7	7	0	7	7	×	3	
8	00	1033.5	W 9	÷15.3	53	20-50	03	2	6	6	0	7	7	0	3	
	03	1033.7	W 4	÷17.2	58	20-50	01	0	4	4	0	7	7	0	3	
	06	1033.8	W 4	÷18.0	..	÷18.0	59	20-50	01	0	4	4	0	7	7	0	3	0.0
	09	1033.8	W 4	÷19.4	63	20-50	01	0	2	1	4	6	7	0	3	
	12	1033.2	W 3	÷18.9	61	20-50	01	0	1	1	0	6	7	0	9	
	15	1032.3	0	÷21.4	67	20-50	01	0	1	1	0	6	7	0	8	
	18	1030.7	0	÷22.3	÷13.1	..	69	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1028.9	W 1	÷21.9	67	> 50	00	0	0	0	0	9	0	0	8	
9	00	1027.3	W 1	÷24.6	71	> 50	00	0	0	0	0	9	0	0	8	
	03	1026.1	W 1	÷24.6	70	> 50	00	0	0	0	0	9	0	0	8	
	06	1026.1	W 1	÷25.2	..	÷25.2	70	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1026.1	W 1	÷25.2	70	> 50	00	0	0	0	0	9	0	0	3	
	12	1026.1	0	÷25.3	71	> 50	00	0	0	0	0	9	0	0	3	
	15	1025.9	W 1	÷25.9	72	> 50	00	0	0	0	0	9	0	0	9	
	18	1026.0	W 1	÷26.0	÷20.9	..	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1025.3	W 3	÷24.6	71	> 50	00	0	0	0	0	9	0	0	8	
10	00	1025.4	W 4	÷24.9	70	> 50	00	0	0	0	0	9	0	0	8	
	03	1025.0	W 3	÷24.3	68	> 50	00	0	0	0	0	9	0	0	8	
	06	1024.9	W 2	÷22.0	..	÷26.1	64	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1024.7	W 4	÷18.4	59	> 50	00	0	0	0	0	9	0	0	8	
	12	1024.1	W 4	÷19.3	60	> 50	02	1	3	3	0	8	7	0	8	
	15	1023.5	0	÷18.8	60	> 50	02	2	4	4	0	8	7	0	8	
	18	1022.7	W 3	÷16.0	÷15.8	..	66	> 50	02	2	4	4	0	8	7	0	8	0.0
	21	1021.1	W 1	÷17.2	70	> 50	03	2	8	8	0	8	7	×	8	
11	00	1020.0	0	÷15.8	70	> 50	03	2	8	8	0	8	7	×	8	
	03	1019.8	W 9	÷19.4	53	> 50	03	2	8	8	0	8	7	×	8	
	06	1019.4	W 5	÷12.0	..	÷22.0	58	> 50	03	2	8	8	0	8	7	×	8	0.0
	09	1019.2	W 4	÷12.6	60	> 50	02	1	4	4	0	8	7	×	8	
	12	1018.0	SW 4	÷12.9	57	> 50	03	2	8	8	0	8	7	×	8	
	15	1016.5	0	÷14.4	62	> 50	03	2	8	8	0	8	7	×	8	
	18	1015.7	0	÷16.1	÷ 9.3	..	69	> 50	03	2	8	8	0	8	7	×	8	0.0
	21	1015.1	NE 1	÷14.8	83	2-4	74	7	8	8	0	7	2	×	8	
12	00	1015.0	0	÷16.2	84	2-4	74	7	8	8	0	7	2	×	8	
	03	1015.3	W 1	÷16.1	86	2-4	74	7	8	8	0	6	2	×	3	
	06	1015.3	0	÷16.0	..	÷16.9	84	4-10	03	2	8	8	0	6	2	×	3	0.8
	09	1014.2	W 4	÷17.6	77	20-50	01	0	1	1	0	6	7	×	9	
	12	1011.8	0	÷19.4	78	20-50	01	0	3	3	0	6	7	×	8	
	15	1011.0	SE 3	÷20.7	70	10-20	02	2	4	4	0	6	7	×	8	
	18	1010.3	SE 3	÷20.1	÷14.4	..	70	4-10	03	2	8	8	0	6	7	×	8	0.0
	21	1010.1	SE 4	÷19.5	75	4-10	03	2	8	8	0	6	7	×	8	
13	00	1009.7	NE 2	÷20.4	79	4-10	02	2	4	4	0	6	7	0	8	
	03	1009.7	0	÷23.3	80	4-10	72	7	2	2	0	6	7	0	3	
	06	1009.7	0	÷25.1	..	÷25.1	80	20-50	01	7	1	1	0	8	7	0	3	0.5
	09	1009.7	0	÷28.0	80	> 50	01	0	1	1	0	8	7	0	3	
	12	1009.7	0	÷28.0	80	> 50	01	0	1	1	0	8	7	0	3	
	15	1009.7	0	÷29.1	80	> 50	01	0	2	2	0	8	7	0	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
14	18	1010.2	0	÷28.4	÷17.8	..	79	> 50	01	0	2	2	0	8	7	0	3	0.0
	21	1011.6	0	÷27.4	79	10—20	02	2	7	7	0	9	7	0	3	
	00	1011.6	W 1	÷27.0	78	10—20	02	2	7	7	0	9	7	0	3	
	03	1011.4	WSW 1	÷27.8	76	> 50	01	0	1	1	0	9	7	0	9	
	06	1010.5	0	÷29.1	..	÷30.5	75	> 50	01	0	1	0	0	9	7	0	9	0.0
	09	1011.1	0	÷29.3	75	> 50	00	0	0	0	0	9	0	0	4	
15	12	1011.2	0	÷29.9	75	> 50	01	0	1	0	0	9	7	0	3	
	15	1010.6	W 1	÷27.8	73	> 50	01	0	1	0	0	9	7	0	9	
	18	1009.5	W 1	÷27.9	÷27.3	..	75	> 50	03	2	8	8	0	7	2	×	8	0.0
	21	1008.7	W 1	÷25.4	73	> 50	03	2	8	8	0	7	2	×	8	
	00	1008.2	0	÷24.4	75	> 50	72	7	8	8	0	7	2	×	8	
	03	1007.8	0	÷24.3	75	20—50	03	2	8	8	0	7	2	×	8	
16	06	1007.4	0	÷24.2	..	÷31.8	75	20—50	03	2	8	8	0	7	2	×	8	0.2
	09	1007.4	S 1	÷24.0	78	20—50	03	2	8	8	0	8	5	×	3	
	12	1007.4	0	÷24.9	82	20—50	03	2	8	8	0	8	5	×	3	
	15	1006.7	0	÷24.7	82	20—50	03	2	8	8	5	6	5	×	9	
	18	1007.3	0	÷24.3	÷24.2	..	83	2—10	02	2	7	4	5	6	5	×	4	0.1
	21	1007.8	0	÷24.0	81	2—4	02	2	7	4	5	6	5	×	3	
17	00	1008.8	0	÷24.4	82	4—10	02	2	6	0	0	9	5	0	3	
	03	1008.9	SE 1	÷25.6	81	4—10	02	2	6	0	0	9	5	0	3	
	06	1009.0	0	÷25.6	..	÷27.3	80	10—20	03	2	8	0	0	9	7	×	3	0.4
	09	1009.1	0	÷27.3	81	10—20	02	2	7	0	0	9	7	×	3	
	12	1009.0	WSW 1	÷27.3	80	4—10	02	2	7	0	0	9	7	×	3	
	15	1008.6	0	÷31.0	80	10—20	01	0	3	0	0	9	5	0	7	
18	18	1008.1	0	÷32.1	÷24.0	..	80	10—20	01	0	1	0	0	9	5	0	8	0.1
	21	1008.0	0	÷31.5	79	> 50	01	0	2	0	0	9	0	8	8	
	00	1007.5	0	÷32.0	79	> 50	01	0	2	0	0	9	0	8	8	
	03	1007.1	0	÷32.3	78	> 50	01	0	2	0	0	9	0	8	8	
	06	1005.8	0	÷32.0	..	÷35.3	78	> 50	03	0	8	0	0	9	0	7	9	0.0
	09	1006.8	0	÷31.8	78	> 50	01	0	2	0	0	9	0	7	3	
19	12	1006.4	0	÷31.5	77	20—50	01	0	2	0	0	9	0	7	9	
	15	1006.1	0	÷32.5	77	20—50	01	0	2	0	0	9	5	0	8	
	18	1006.2	0	÷34.9	÷31.1	..	77	50	00	0	0	0	0	9	0	0	3	0.0
	21	1006.2	0	÷33.7	77	20—50	01	0	2	0	0	9	5	0	3	
	00	1006.3	0	÷33.1	77	20—50	01	0	2	0	0	9	5	0	3	
	03	1004.8	W 12	÷24.0	71	20—50	01	0	2	0	0	9	5	0	9	
19	06	1004.1	W 10	÷23.0	..	÷35.4	72	2—4	01	3	2	0	0	9	5	0	8	0.0
	09	1004.3	W 12	÷21.9	80	< 0.05	39	3	×	×	×	×	×	×	3	
	12	1005.9	W 14	÷21.4	82	< 0.05	39	3	×	×	×	×	×	×	4	
	15	1007.8	W 12	÷21.7	83	0.2—0.5	03	2	8	8	5	6	×	×	3	
	18	1008.9	W 12	÷20.3	÷19.8	..	85	< 0.05	39	2	8	8	5	6	×	×	3	0.0
	21	1010.2	W 12	÷20.1	78	10—20	02	2	7	0	0	9	7	0	3	
19	00	1012.0	W 12	÷20.7	75	10—20	01	1	4	0	0	9	7	0	3	
	03	1013.7	W 10	÷20.7	72	10—20	03	2	8	0	0	9	0	7	3	
	06	1014.8	W 10	÷20.5	..	÷23.2	72	20—50	03	2	8	0	0	9	0	7	3	0.0
	09	1017.0	W 4	÷21.3	76	20—50	03	2	8	0	0	9	0	7	3	
	12	1017.3	W 4	÷22.6	76	> 50	03	2	8	0	0	9	0	7	3	
15	1017.5	W 3	÷24.7	76	> 50	00	0	0	0	0	9	0	0	3		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
20	18	1017.6	W 1	÷25.0	÷20.0	..	74	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1017.9	0	÷26.4	76	> 50	00	0	0	0	0	9	0	0	3	
	00	1018.4	0	÷26.7	76	> 50	00	0	0	0	0	9	0	0	3	
	03	1017.0	0	÷27.1	77	> 50	02	2	1	0	0	9	0	9	9	
	06	1016.6	0	÷27.9	..	÷27.9	78	> 50	01	0	3	0	0	9	0	9	8	0.0
	09	1016.5	0	÷28.1	78	> 50	01	0	1	0	0	9	0	9	8	
	12	1016.4	0	÷27.8	76	> 50	00	0	0	0	0	9	0	0	8	
21	15	1017.2	W 4	÷26.1	74	> 50	01	0	2	0	0	9	0	9	4	
	18	1017.6	W 7	÷24.3	÷22.1	..	70	> 50	02	2	7	0	0	9	7	×	3	0.8
	21	1020.4	W 7	÷22.7	68	> 50	01	1	1	0	0	8	7	0	3	
	00	1021.1	W 9	÷22.1	66	> 50	02	1	6	1	0	8	7	0	3	
	03	1021.7	W 10	÷21.1	64	> 50	02	1	6	0	0	9	0	6	3	
	06	1021.8	W 10	÷20.5	..	÷28.3	62	> 50	03	2	8	0	0	9	0	6	3	0.0
	09	1021.8	W 12	÷20.7	61	> 50	02	2	6	0	0	9	0	6	3	
22	12	1022.1	W 10	÷21.1	68	> 50	02	2	6	0	0	9	0	6	3	
	15	1022.0	W 9	÷20.4	68	> 50	02	2	6	1	5	5	0	6	9	
	18	1021.5	W 9	÷19.8	÷19.3	..	66	> 50	03	2	8	0	0	9	0	7	8	0.0
	21	1020.6	W 10	÷20.1	78	> 50	01	0	2	0	0	9	0	9	8	
	00	1020.6	W 14	÷20.3	76	> 50	01	0	1	0	0	9	0	9	3	
	03	1021.6	W 14	÷20.0	78	10—20	03	3	8	0	0	9	0	7	4	
	06	1021.8	W 12	÷19.6	..	÷22.0	78	10—20	03	3	8	0	0	9	0	7	3	0.0
23	09	1022.1	W 10	÷19.6	82	10—20	03	3	8	0	0	9	0	7	3	
	12	1023.0	W 10	÷20.3	62	10—20	02	2	7	0	0	9	0	7	3	
	15	1023.8	W 10	÷20.4	61	10—20	02	2	5	0	0	9	0	7	3	
	18	1024.4	W 9	÷22.3	÷19.1	..	60	10—20	02	2	5	0	0	9	0	7	3	0.0
	21	1024.2	W 6	÷22.9	52	10—20	00	0	0	0	0	9	0	0	3	
	00	1024.3	W 5	÷24.1	52	10—20	00	0	0	0	0	9	0	0	0	
	03	1023.5	SW 3	÷25.7	56	10—20	00	0	0	0	0	9	0	0	9	
24	06	1023.0	0	÷27.8	..	÷27.8	59	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1021.9	0	÷28.3	61	> 50	00	0	0	0	0	9	0	0	8	
	12	1021.9	0	÷28.7	62	> 50	00	0	0	0	0	9	0	0	3	
	15	1021.0	0	÷30.0	63	> 50	00	0	0	0	0	9	0	0	9	
	18	1020.9	0	÷30.7	÷22.3	..	64	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1021.0	W 1	÷31.4	64	20—50	00	0	0	0	0	9	0	0	3	
	00	1021.1	0	÷31.2	64	> 50	00	0	0	0	0	9	0	0	3	
25	03	1020.9	0	÷30.7	64	> 50	00	0	0	0	0	9	0	0	9	
	06	1020.0	0	÷31.8	..	÷32.0	66	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1018.6	0	÷31.9	64	> 50	00	0	0	0	0	9	0	0	8	
	12	1016.4	0	÷31.7	64	> 50	00	0	0	0	0	9	0	0	8	
	15	1014.5	0	÷32.5	64	> 50	00	0	0	0	0	9	0	0	8	
	18	1014.2	0	÷33.3	÷30.7	..	64	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1012.5	0	÷34.1	66	> 50	00	0	0	0	0	9	0	0	8	
25	00	1011.3	0	÷34.1	67	> 50	00	0	0	0	0	9	0	0	8	
	03	1010.8	0	÷34.2	68	> 50	01	0	1	0	0	9	5	0	8	
	06	1010.4	0	÷33.5	..	÷35.7	66	> 50	01	0	2	0	0	9	5	0	8	0.0
	09	1010.2	W 4	÷31.1	63	> 50	02	2	7	0	0	9	5	0	8	
	12	1010.2	WSW 3	÷30.9	62	> 50	01	0	4	0	0	9	5	0	3	
15	1010.7	W 3	÷29.1	60	> 50	03	2	8	0	0	9	5	0	3		

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1022.8	W 10	÷25.7	65	10—20	02	2	4	4	0	7	7	0	3	
	03	1023.8	W 10	÷25.9	62	10—20	01	0	2	2	0	7	7	0	3	
	06	1024.6	W 12	÷25.7	..	÷28.4	61	10—20	01	0	2	2	0	7	7	0	3	
	09	1025.1	W 10	÷25.8	58	10—20	01	0	1	1	0	7	7	0	3	
	12	1025.3	W 12	÷26.0	60	10—20	01	0	1	1	0	7	7	0	3	
	15	1026.7	W 10	÷26.7	58	10—20	01	0	1	1	0	7	7	0	4	
	18	1027.6	W 10	÷26.5	÷24.1	..	56	10—20	01	0	1	1	0	7	7	0	3	0.0
	21	1028.0	W 8	÷27.1	56	10—20	01	0	1	1	0	7	7	0	3	
2	00	1028.7	W 8	÷27.3	53	10—20	01	0	1	1	0	7	7	0	3	
	03	1029.2	W 8	÷27.6	51	10—20	01	0	1	1	0	7	7	0	3	
	06	1029.3	W 5	÷29.2	51	20—50	01	0	1	1	0	7	7	0	3	0.0
	09	1029.3	W 5	÷28.3	49	20—50	00	0	0	0	0	9	0	0	3	
	12	1029.3	W 4	÷29.4	49	20—50	00	0	0	0	0	9	0	0	3	
	15	1029.4	W 3	÷30.5	50	> 50	00	0	0	0	0	9	0	0	3	
	18	1029.3	WSW 2	÷31.0	÷26.5	..	52	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1029.0	W 3	÷23.5	53	> 50	00	0	0	0	0	9	0	0	9	
3	00	1028.5	W 3	÷33.0	54	> 50	00	0	0	0	0	9	0	0	8	
	03	1028.5	W 2	÷34.2	57	> 50	00	0	0	0	0	9	0	0	3	
	06	1027.7	0	÷34.7	..	÷34.9	57	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1026.7	W 1	÷35.5	58	> 50	00	0	0	0	0	9	0	0	8	
	12	1026.3	0	÷36.5	58	> 50	00	0	0	0	0	9	0	0	8	
	15	1025.5	0	÷36.6	59	> 50	00	0	0	0	0	9	0	0	8	
	18	1024.6	0	÷37.0	÷31.0	..	61	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1023.9	0	÷37.5	63	20—50	00	0	0	0	0	9	0	0	8	
4	00	1023.5	W 1	÷37.4	63	20—50	00	0	0	0	0	9	0	0	8	
	03	1023.4	W 1	÷36.2	..	÷37.5	62	20—50	00 ¹	0	0	0	0	9	0	0	8	0.0
	06	1023.3	W 1	÷35.9	64	20—50	00	0	0	0	0	9	0	0	8	
	09	1022.7	W 1	÷36.2	65	20—50	00	0	0	0	0	9	0	0	8	
	12	1022.5	0	÷37.7	65	> 50	00	0	0	0	0	9	0	0	8	
	15	1022.3	0	÷38.2	67	> 50	01	0	1	1	0	9	7	0	8	
	18	1021.0	0	÷38.0	÷35.7	..	68	10—20	01	0	2	2	0	9	7	0	8	trace
	21	1020.4	0	÷38.5	68	10—20	01	0	1	1	0	8	7	0	8	
5	00	1019.9	0	÷39.4	69	10—20	01	0	1	1	0	8	7	0	8	
	03	1018.9	0	÷38.9	68	10—20	79	7	4	4	0	7	7	0	8	
	06	1019.2	0	÷38.3	..	÷39.8	66	10—20	79	7	4	4	0	7	7	0	4	0.2
	09	1018.4	W 1	÷37.1	65	10—20	02	2	6	6	0	7	7	0	9	
	12	1017.7	SW 1	÷37.1	65	10—20	79	7	6	6	0	7	7	0	8	
	15	1016.5	W 8	÷35.1	64	2—4	02	2	6	6	0	6	7	0	8	
	18	1017.4	W 9	÷35.3	÷35.0	..	66	2—4	01	0	4	4	0	6	7	0	4	0.2
	21	1018.0	W 9	÷35.7	57	2—4	01	0	4	4	0	6	7	0	3	
6	00	1018.3	W 8	÷36.1	58	2—4	01	0	1	1	0	6	7	0	3	
	03	1019.3	W 10	÷35.2	54	2—4	01	0	1	1	0	6	7	0	3	
	06	1019.3	WSW 6	÷35.1	..	÷39.0	52	20—50	00	0	0	0	0	9	7	0	3	0.0
	09	1017.1	0	÷34.5	52	20—50	00	0	0	0	0	9	0	0	9	
	12	1016.9	SE 4	÷37.0	54	20—50	00	0	0	0	0	9	0	0	8	
	15	1016.3	SE 2	÷37.1	56	20—50	01	0	1	1	0	8	7	0	8	

¹ 0300—1800 Ice-needles in the air.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1014.7	SE 1	÷37.1	÷34.1	..	62	10—20	01	0	1	1	0	8	7	0	8	0.0
	21	1014.8	0	÷35.4	58	10—20	02	2	7	7	0	7	7	0	3	
7	00	1013.4	WSW 5	÷32.3	58	10—20	02	2	4	4	0	7	7	0	8	
	03	1011.9	W 4	÷31.8	56	10—20	01	0	4	4	0	7	7	0	8	
	06	1010.4	W 4	÷31.5	..	÷37.4	56	10—20	01	0	4	4	0	7	7	0	8	0.0
	09	1007.9	W 10	÷30.5	54	10—20	01	0	4	4	0	7	7	0	9	
	12	1005.3	W 14	÷28.5	54	< 0.05	39 ¹	3	×	×	0	×	×	0	8	
	15	1003.4	W 22	÷28.4	×	< 0.05	39 ²	3	×	×	0	×	×	0	8	
	18	1001.5	W 24	÷28.9	÷28.1	..	×	< 0.05	39	3	×	×	0	×	×	0	8	×
	21	1001.4	W 26	÷29.2	×	< 0.05	39	3	×	×	0	×	×	0	3	
8	00	1000.6	W 28	÷28.6	×	< 0.05	39	3	×	×	0	×	×	0	8	
	03	1001.1	W 28 ³	÷26.4	×	< 0.05	39	3	×	×	0	×	×	0	3	
	06	1002.8	W 26	÷25.7	..	÷31.5	×	< 0.05	39	3	×	×	0	×	×	0	4	×
	09	1008.7	W 20	÷25.3	×	< 0.05	39	3	×	×	0	×	×	0	4	
	12	1010.6	W 24	÷25.3	×	< 0.05	39	3	×	×	0	×	×	0	4	
	15	1013.8	W 20	÷25.9	×	< 0.05	39	3	×	×	0	×	×	0	4	
	18	1016.8	W 20	÷26.1	÷25.0	..	×	< 0.05	39	3	×	×	0	×	×	0	5	×
	21	1019.7	W 25	÷26.9	×	< 0.05	39	3	×	×	0	×	×	0	3	
9	00	1022.1	W 27	÷26.8	×	< 0.05	39	3	×	×	×	×	×	×	3	
	03	1024.7	W 27	÷26.2	×	< 0.05	39	3	×	×	×	×	×	×	3	
	06	1027.7	W 25	÷26.0	..	÷27.2	×	< 0.05	39	3	×	×	×	×	×	×	3	×
	09	1031.2	W 20	÷26.1	×	2—4	02	3	4	4	0	6	7	0	3	
	12	1031.7	W 15	÷25.7	×	2—4	02	2	6	6	0	6	7	0	1	
	15	1032.6	W 15	÷25.9	×	2—4	02	2	6	6	0	6	7	0	3	
	18	1032.9	W 12	÷26.0	÷25.2	..	×	4—10	02	2	6	6	0	6	7	0	3	0.0
	21	1033.5	W 9	÷26.3	58	4—10	02	2	7	7	0	6	7	0	3	
10	00	1033.5	W 6	÷27.6	58	10—20	01	0	2	2	0	6	7	0	3	
	03	1033.4	0	÷30.1	60	20—50	00	0	0	0	0	9	0	0	3	
	06	1032.1	0	÷31.1	..	÷31.2	66	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1030.6	0	÷31.7	67	20—50	00	0	0	0	0	9	0	0	8	
	12	1030.1	0	÷32.4	70	20—50	00	0	0	0	0	9	0	0	8	
	15	1028.9	0	÷33.2	73	20—50	00	0	0	0	0	9	0	0	8	
	18	1029.0	0	÷34.9	÷26.0	..	74	20—50	00	0	0	0	0	9	0	0	3	0.0
	21	1030.0	0	÷34.0	74	20—50	00	0	0	0	0	9	0	0	3	
11	00	1030.9	W 3	÷34.0	72	> 50	00	0	0	0	0	9	0	0	3	
	03	1032.6	W 3	÷34.1	69	> 50	00	0	0	0	0	9	0	0	3	
	06	1036.7	W 2	÷33.4	..	÷35.0	68	> 50	01	0	2	2	0	8	6	0	4	0.0
	09	1039.8	W 4	÷31.0	61	> 50	01	0	4	4	0	8	6	0	3	
	12	1040.5	W 3	÷31.1	60	> 50	01	0	4	4	0	8	6	0	3	
	15	1042.5	W 4	÷31.9	61	> 50	01	0	4	2	0	8	6	9	4	
	18	1046.1	W 1	÷32.5	÷30.7	..	60	> 50	01	0	1	1	0	8	4	9	4	0.0
	21	1045.8	W 4	÷32.2	60	> 50	00	0	0	0	0	9	0	0	9	
12	00	1046.0	W 4	÷32.7	58	> 50	00	0	0	0	0	9	0	0	3	
	03	1047.1	W 5	÷33.3	60	> 50	00	0	0	0	0	9	0	0	4	
	06	1047.3	W 3	÷34.5	..	÷34.8	60	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1046.8	W 4	÷33.7	60	> 50	00	0	0	0	0	9	0	0	9	
	12	1046.6	W 3	÷34.0	62	> 50	01	0	1	1	0	8	7	0	8	
	15	1046.6	W 2	÷34.5	62	> 50	00	0	0	0	0	9	0	0	3	

¹ Snow drift. ² Strong sand drift too. ³ Wind 32–33 m/sec. in the gusts.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
13	18	1045.5	W 4	÷34.2	÷31.9	..	62	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1045.3	W 3	÷34.4	63	> 50	00	0	0	0	0	9	0	0	8	
	00	1045.0	W 4	÷34.4	63	> 50	00	0	0	0	0	9	0	0	8	
	03	1044.0	W 2	÷35.0	65	> 50	00	0	0	0	0	9	0	0	8	
	06	1042.9	W 4	÷34.6	..	÷34.8	64	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1042.2	W 3	÷34.4	62	> 50	00	0	0	0	0	9	0	0	8	
14	12	1040.9	W 1	÷35.0	63	> 50	00	0	0	0	0	9	0	0	8	
	15	1039.8	W 1	÷35.7	64	> 50	00	0	0	0	0	9	0	0	8	
	18	1038.8	0	÷36.3	÷34.1	..	70	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1037.3	0	÷37.9	71	> 50	00	0	0	0	0	9	0	0	8	
	00	1036.6	0	÷37.4	71	> 50	01	0	1	0	0	9	0	9	8	
	03	1035.3	0	÷37.3	71	> 50	01	0	4	0	0	9	0	9	8	
15	06	1033.8	0	÷36.9	..	÷38.3	70	> 50	03	2	8	0	0	9	0	7	9	0.0
	09	1032.0	0	÷35.9	70	> 50	03	2	8	0	0	9	0	7	8	
	12	1030.7	0	÷35.3	70	> 50	03	2	8	0	0	9	0	7	8	
	15	1026.7	W 3	÷34.1	70	> 50	03	2	8	0	0	9	0	7	9	
	18	1024.8	W 3	÷32.5	÷32.5	..	69	> 50	03	2	8	0	0	9	0	7	8	0.0
	21	1021.2	W 6	÷31.1	69	2-4	79	7	8	0	0	9	0	7	9	
16	00	1017.0	W 6	÷29.3	72	2-4	79	7	8	0	0	9	0	7	9	
	03	1015.6	W 3	÷29.3	72	10-20	79	7	8	0	0	9	0	7	8	
	06	1013.8	W 10	÷27.5	..	÷37.2	71	10-20	03	3	8	0	0	9	0	7	8	×
	09	1011.9	W 13	÷24.8	69	10-20	03	2	8	0	0	9	0	7	8	
	12	1011.6	W 13	÷24.1	60	10-20	03	2	8	0	0	9	0	7	8	
	15	1010.2	W 15	÷23.9	63	10-20	03	2	8	0	0	9	0	7	8	
17	18	1009.2	W 16	÷23.8	÷22.8	..	52	10-20	02 ¹	2	7	0	0	9	0	7	8	0.0
	21	1010.4	W 16	÷24.3	48	10-20	01	0	1	0	0	9	0	9	4	
	00	1011.3	W 12	÷24.3	49	10-20	00	0	0	0	0	9	0	0	3	
	03	1011.6	W 11	÷24.8	52	10-20	00	0	0	0	0	9	0	0	3	
	06	1012.7	W 7	÷25.0	..	÷27.8	55	10-20	00	0	0	0	0	9	0	0	3	0.0
	09	1013.3	0	÷24.5	56	10-20	00	0	0	0	0	9	0	0	3	
18	12	1013.4	0	÷28.5	58	10-20	00	0	0	0	0	9	0	0	3	
	15	1013.6	0	÷28.1	63	10-20	00	0	0	0	0	9	0	0	3	
	18	1012.6	W 1	÷29.2	÷22.5	..	65	10-20	00	0	0	0	0	9	0	0	9	0.0
	21	1011.3	0	÷30.9	67	10-20	00	0	0	0	0	9	0	0	8	
	00	1010.6	W 1	÷31.2	68	10-20	00	0	0	0	0	9	0	0	8	
	03	1009.7	W 4	÷30.7	69	10-20	00	0	0	0	0	9	0	0	8	
18	06	1008.6	W 1	÷31.3	..	÷32.6	69	10-20	00	0	0	0	0	9	0	0	8	0.0
	09	1008.5	0	÷31.8	68	10-20	01	0	1	0	0	9	0	5	8	
	12	1007.8	0	÷32.1	70	10-20	00	0	0	0	0	9	0	0	8	
	15	1006.1	W 4	÷34.1	70	10-20	00	0	0	0	0	9	0	0	9	
	18	1004.9	W 1	÷33.7	÷29.0	..	72	10-20	00	0	0	0	0	9	0	0	8	0.0
	21	1003.8	W 1	÷33.6	72	10-20	00	0	0	0	0	9	0	0	8	
18	00	1002.8	W 1	÷33.8	69	10-20	01	0	1	0	0	9	0	5	8	
	03	1002.0	W 5	÷32.8	69	10-20	01	0	1	0	0	9	0	5	8	
	06	1001.2	W 4	÷32.8	..	÷34.1	68	10-20	02	2	8	0	0	9	0	5	8	0.0
	09	1002.3	W 2	÷31.9	66	10-20	03	2	8	0	0	9	0	7	4	
	12	1003.7	W 6	÷31.9	64	10-20	03	2	8	0	0	9	0	7	3	
	15	1003.7	W 8	÷29.5	62	10-20	03	2	8	0	0	9	0	7	3	

¹ Snow drift on Brønlunds Fjord, not at the station.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
19	18	1003.8	W 9	÷28.1	÷28.0	..	60	10—20	03	2	8	0	0	9	0	7	3	0.0
	21	1004.9	W 12	÷26.9	60	10—20	03	2	8	0	0	9	0	7	4	
	00	1007.1	W 13	÷26.3	56	10—20	03	2	8	0	0	9	0	7	4	
	03	1010.2	W 14	÷25.4	58	10—20	03	2	8	0	0	9	0	7	3	
	06	1011.9	W 12	÷25.0	..	÷32.8	57	10—20	03	2	8	0	0	9	0	7	3	0.0
	09	1015.1	W 11	÷23.7	56	10—20	03	2	8	0	0	9	0	7	4	
	12	1017.0	W 11	÷23.7	64	4—10	03	2	8	8	5	6	×	×	3	
20	15	1018.5	W 13	÷23.2	67	4—10	03	2	8	8	5	6	×	×	3	
	18	1020.4	W 10	÷23.4	÷22.3	..	65	4—10	03	2	8	8	5	7	×	×	3	0.0
	21	1022.9	W 12	÷24.2	67	4—10	02 ¹	2	4	4	5	7	×	0	3	
	00	1024.3	W 10	÷24.5	63	20—50	02	2	6	6	0	9	5	0	3	
	03	1025.3	W 8	÷24.9	61	20—50	02	2	8	0	0	9	5	0	3	
	06	1026.4	W 12	÷24.8	..	÷25.2	59	20—50	03	2	8	0	0	9	0	7	3	0.0
	09	1028.1	W 13	÷24.5	64	20—50	03	2	8	0	0	9	0	7	3	
21	12	1029.1	W 13	÷24.9	64	20—50	03 ²	2	8	0	0	9	0	7	3	
	15	1029.5	W 14	÷25.3	62	20—50	03	2	8	0	0	9	0	7	3	
	18	1030.4	W 10	÷26.1	÷23.1	..	58	20—50	02	2	7	0	0	9	0	7	3	0.0
	21	1030.4	W 7	÷26.3	56	20—50	00	0	0	0	0	9	0	0	3	
	00	1029.2	W 6	÷27.1	54	20—50	00	0	0	0	0	9	0	0	9	
	03	1027.0	W 4	÷28.9	56	20—50	00	0	0	0	0	9	0	0	9	
	06	1024.8	W 4	÷30.9	..	÷31.5	60	20—50	00	0	0	0	0	9	0	0	8	0.0
22	09	1021.3	WSW 5	÷32.1	64	20—50	00	0	0	0	0	9	0	0	8	
	12	1020.1	0	÷32.4	62	20—50	00	0	0	0	0	9	0	0	8	
	15	1016.9	W 2	÷33.3	63	20—50	00	0	0	0	0	9	0	0	9	
	18	1014.7	W 4	÷33.7	÷25.8	..	63	20—50	00	0	0	0	0	9	0	0	8	0.0
	21	1014.2	W 4	÷33.7	63	20—50	00	0	0	0	0	9	0	0	6	
	00	1013.9	W 4	÷33.0	60	20—50	00	0	0	0	0	9	0	0	6	
	03	1014.3	0	÷33.3	59	20—50	00	0	0	0	0	9	0	0	3	
23	06	1015.0	0	÷32.7	..	÷34.4	60	20—50	00	0	0	0	0	9	0	0	3	0.0
	09	1015.3	0	÷33.7	60	20—50	00	0	0	0	0	9	0	0	3	
	12	1014.5	0	÷35.1	62	20—50	00	0	0	0	0	9	0	0	9	
	15	1011.9	0	÷34.4	62	20—50	00	0	0	0	0	9	0	0	9	
	18	1010.0	0	÷33.7	÷32.5	..	61	20—50	00	0	0	0	0	9	0	0	8	0.0
	21	1009.9	0	÷33.4	62	20—50	03	2	8	0	0	9	0	7	8	
	00	1009.1	0	÷33.4	65	20—50	01	0	2	0	0	9	0	7	8	
24	03	1009.0	0	÷34.6	66	20—50	01	0	1	0	0	9	0	7	3	
	06	1007.4	0	÷35.8	..	÷36.8	66	20—50	00	0	0	0	0	9	0	0	9	0.0
	09	1007.2	0	÷36.1	66	20—50	00	0	0	0	0	9	0	0	8	
	12	1007.1	E 2	÷33.1	68	20—50	03	2	7	7	0	8	7	×	8	
	15	1007.5	0	÷32.3	72	10—20	72	7	8	8	0	7	2	×	3	
	18	1007.6	0	÷32.3	÷32.2	..	72	10—20	72	7	8	8	0	7	2	×	3	×
	21	1007.5	0	÷31.9	70	10—20	74	7	8	8	0	7	2	×	3	
24	00	1008.6	0	÷31.9	71	20—50	74	7	8	8	0	7	2	×	3	
	03	1010.0	E 5	÷33.0	72	20—50	74	7	8	8	0	7	2	×	3	
	06	1011.2	E 4	÷33.5	..	÷36.3	72	20—50	78	7	0	0	0	9	0	0	3	×
	09	1013.5	0	÷33.7	70	20—50	78	7	0	0	0	9	0	0	4	
	12	1014.9	0	÷36.9	78	20—50	78	7	0	0	0	9	0	0	3	
15	1017.6	0	÷37.5	×	20—50	00	0	0	0	0	9	0	0	4		

¹ Snow drift on Brønlunds Fjord. ² Snow drift on Brønlunds Fjord.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
25	18	1018.2	0	÷38.5	÷31.7	..	74	20-50	00	0	0	0	0	9	0	0	3	×	
	21	1019.3	0	÷38.6	72	20-50	00	0	0	0	0	9	0	0	3		
	00	1020.3	0	÷39.6	70	20-50	00	0	0	0	0	9	0	0	3		
	03	1021.8	0	÷39.8	71	20-50	00	0	0	0	0	9	0	0	3		
	06	1022.8	0	÷40.4	..	÷40.4	×	×	20-50	00	0	0	0	0	9	0	0	3	0.0
	09	1023.9	0	÷40.1	×	×	20-50	00	0	0	0	0	9	0	0	3	
26	12	1025.4	E 2	÷38.1	60	> 50	00	0	0	0	0	9	0	0	3		
	15	1026.6	E 2	÷40.1	62	> 50	00	0	0	0	0	9	0	0	3		
	18	1026.6	E 3	÷40.4	÷38.5	..	×	> 50	01	0	1	0	0	9	7	0	9	0.0	
	21	1024.4	E 1	÷40.6	×	> 50	01	0	2	0	0	9	7	0	9		
	00	1022.0	E 1	÷40.3	×	10-20	02	2	4	0	0	9	7	0	8		
	03	1018.3	E 4	÷40.1	×	10-20	02	2	4	0	0	9	7	0	9		
27	06	1015.1	E 3	÷40.2	..	÷41.3	×	2-4	03	2	7	7	0	7	2	0	8	0.0	
	09	1012.4	0	÷39.9	×	2-4	02	2	4	4	0	7	2	0	8		
	12	1007.4	0	÷40.0	×	2-4	02	0	4	4	0	7	2	0	8		
	15	1005.1	0	÷39.9	×	2-4	02	0	4	4	0	7	2	0	8		
	18	1001.9	0	÷39.6	÷39.4	..	×	2-4	02	0	4	4	0	7	7	0	9	0.0	
	21	997.2	W 1	÷38.9	×	2-4	03	0	8	8	0	7	2	0	9		
28	00	995.4	0	÷36.7	×	2-4	03	0	8	8	0	7	2	0	8		
	03	993.7	0	÷34.6	×	1-2	74	7	8	8	0	5	2	×	8		
	06	993.7	W 3	÷34.1	..	÷40.4	×	1-2	74	7	8	8	0	5	2	×	3	0.8	
	09	994.5	W 4	÷31.3	×	1-2	74	7	8	8	0	5	2	×	3		
	12	995.9	W 5	÷29.7	×	1-2	74	7	8	8	0	5	2	×	3		
	15	995.8	W 1	÷27.9	×	1-2	74	7	8	8	0	5	2	×	3		
29	18	995.0	E 6	÷28.1	÷27.5	..	×	1-2	03	7	8	8	0	5	2	×	9	1.8	
	21	994.4	0	÷30.4	×	20-50	00	0	0	0	0	9	0	0	8		
	00	993.6	W 2	÷32.1	×	20-50	01	0	1	0	0	9	2	0	8		
	03	991.0	0	÷33.2	94	20-50	01	0	1	0	0	9	2	0	9		
	06	988.8	W 12	÷25.9	..	÷35.2	95	1-2	36	2	8	0	0	9	2	0	8	0.0	
	09	989.2	W 14	÷25.1	90	1-2	36	2	8	0	0	9	2	0	4		
30	12	989.9	W 15	÷24.4	92	1-2	36	2	8	0	0	9	2	0	3		
	15	991.9	W 18	÷24.3	95	1-2	36	2	8	0	0	9	2	0	3		
	18	994.3	W 15	÷24.4	÷23.8	..	98	0.5-1	37	2	8	0	0	9	2	0	3	0.0	
	21	997.8	W 15	÷24.8	97	0.05-0.2	39	3	×	×	×	×	×	×	3		
	00	1000.1	W 14	÷24.9	98	0.5-1	37	3	8	0	0	9	2	×	3		
	03	1003.0	W 10	÷25.3	98	1-2	37	3	4	0	0	9	0	0	3		
30	06	1004.4	W 9	÷25.6	..	÷27.0	96	1-2	02	2	4	4	0	7	2	×	3	×	
	09	1005.9	W 8	÷25.2	90	1-2	02	2	4	4	0	7	2	0	3		
	12	1006.8	W 8	÷25.7	84	2-4	02	0	3	3	0	7	2	0	3		
	15	1006.9	W 9	÷26.1	84	2-4	02	2	4	4	0	7	2	0	3		
	18	1007.6	W 10	÷26.3	÷24.1	..	82	2-4	02	2	4	4	0	7	2	0	3	0.0	
	21	1007.7	W 9	÷26.4	83	2-4	02	2	4	4	0	7	2	0	3		
30	00	1007.8	W 9	÷26.3	81	10-20	02	2	7	7	0	7	2	×	3		
	03	1007.9	W 9	÷26.3	80	10-20	02	2	7	7	0	7	2	×	3		
	06	1008.3	W 10	÷26.3	..	÷26.7	77	10-20	02	2	7	7	0	7	2	×	3	0.0	
	09	1009.6	W 10	÷26.6	76	10-20	02	2	7	7	0	7	2	×	3		
	12	1009.7	W 11	÷26.4	77	10-20	02	2	7	7	0	7	2	×	3		
	15	1010.1	W 10	÷26.9	72	20-50	01	0	1	1	0	8	7	0	3		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
31	18	1010.6	W 9	÷27.9	÷26.0	..	74	20—50	01	0	1	1	0	8	7	0	3	0.0
	21	1010.9	W 10	÷27.7	75	20—50	01	0	2	2	0	8	7	0	3	
	00	1011.5	W 9	÷27.8	75	20—50	01	0	1	1	0	8	7	0	3	
	03	1012.3	W 8	÷27.4	75	20—50	01	0	1	1	0	8	7	0	3	
	06	1013.7	W 9	÷27.6	..	÷28.9	75	20—50	01	0	1	1	0	8	7	0	4	0.0
	09	1015.6	W 8	÷27.8	76	20—50	00	0	0	0	0	9	0	0	3	
	12	1015.7	W 6	÷27.1	78	20—50	00	0	0	0	0	9	0	0	3	
	15	1016.2	W 5	÷27.0	78	20—50	00	0	0	0	0	9	0	0	3	
	18	1016.4	0	÷26.9	÷26.7	..	78	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1016.6	0	÷30.0	80	> 50	00	0	0	0	0	9	0	0	3	
Mean	1018.0		5.9	÷31.3	÷29.9	÷33.9	66	3.0

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1017.6	WSW 7	÷24.8	77	20—50	03	0	2	2	0	7	8	0	3	
	03	1017.7	W 9	÷23.3	75	20—50	03	2	4	4	0	7	8	0	3	
2	06	1017.8	W 9	÷23.3	..	÷30.1	74	20—50	01	0	3	3	0	7	7	0	3	0.0
	09	1019.5	W 8	÷25.3	74	20—50	02	0	3	3	0	7	7	0	4	
	12	1020.5	W 8	÷23.5	74	20—50	01	0	2	2	0	7	7	0	3	
	15	1020.5	W 8	÷24.7	72	20—50	03	2	6	6	0	7	7	×	3	
	18	1020.5	W 6	÷23.5	÷23.1	..	72	10—20	03	2	7	7	0	7	7	×	3	0.0
	21	1021.0	W 7	÷24.3	74	20—50	02	2	7	7	0	7	7	×	3	
	00	1020.1	W 7	÷24.9	76	20—50	01	2	6	6	0	7	7	0	9	
	03	1020.8	W 8	÷24.3	76	20—50	01	0	3	3	0	7	7	0	3	
	06	1020.6	W 7	÷24.9	..	÷25.2	76	20—50	02	0	3	3	0	7	7	0	9	0.0
	09	1021.0	W 7	÷25.2	76	20—50	00	0	0	0	0	9	0	0	4	
3	12	1021.3	W'S 5	÷24.7	74	20—50	00	0	0	0	0	9	0	0	3	
	15	1020.4	W 7	÷26.2	75	20—50	00	0	0	0	0	9	0	0	9	
	18	1020.0	SW 4	÷26.1	÷23.1	..	72	20—50	00	0	0	0	0	9	0	0	8	0.0
	21	1019.6	W 3	÷27.1	75	20—50	00	0	0	0	0	9	0	0	8	
	00	1019.2	W 2	÷27.8	74	20—50	00	0	0	0	0	9	0	0	8	
	03	1019.0	SSW 2	÷27.5	75	20—50	00	0	0	0	0	9	0	0	8	
	06	1018.8	W 3	÷28.3	..	÷28.5	74	20—50	00	0	0	0	0	9	0	0	8	0.0
	09	1018.6	0	÷29.9	75	20—50	00	0	0	0	0	9	0	0	8	
	12	1018.3	0	÷29.3	78	> 50	00	0	0	0	0	9	0	0	8	
	15	1018.2	NE 1	÷29.9	77	> 50	00	0	0	0	0	9	0	0	8	
4	18	1018.0	0	÷33.2	÷26.0	..	82	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1019.6	S'W 1	÷34.0	86	> 50	00	0	0	0	0	9	0	0	4	
	00	1019.5	0	÷34.3	87	> 50	00	0	0	0	0	9	0	0	4	
	03	1020.1	0	÷34.3	89	> 50	03	0	2	2	0	9	1	0	4	
	06	1020.6	0	÷35.2	..	÷35.3	90	> 50	02	0	2	2	0	9	1	0	9	0.0
	09	1020.9	0	÷35.3	90	> 50	00	0	0	0	0	9	0	0	4	
	12	1022.0	0	÷35.8	90	> 50	00	0	0	0	0	9	0	0	4	
	15	1022.7	0	÷36.1	91	> 50	00	0	0	0	0	9	0	0	3	
	18	1022.9	0	÷36.5	÷33.3	..	91	> 50	00	0	0	0	0	9	0	0	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
5	21	1023.5	0	÷37.9	91	> 50	00	0	0	0	0	9	0	0	4	
	00	1024.4	0	÷37.4	91	> 50	00	0	0	0	0	9	0	0	3	
	03	1025.1	0	÷37.7	91	> 50	00	0	0	0	0	9	0	0	3	
	06	1025.7	0	÷38.2	..	÷38.2	91	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1025.7	0	÷38.4	91	> 50	00	0	0	0	0	9	0	0	3	
6	12	1026.0	0	÷38.1	90	> 50	00	0	0	0	0	9	0	0	3	
	15	1025.6	0	÷38.5	90	> 50	00	0	0	0	0	9	0	0	3	
	18	1025.1	0	÷38.5	÷36.5	..	90	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1025.1	0	÷38.5	90	> 50	00	0	0	0	0	9	0	0	3	
	00	1024.1	0	÷38.5	90	> 50	00	0	0	0	0	9	0	0	9	
7	03	1023.7	W 1	÷38.5	89	> 50	00	0	0	0	0	9	0	0	8	
	06	1023.2	W 2	÷38.3	..	÷39.1	88	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1023.6	W 3	÷38.1	86	> 50	00	0	0	0	0	9	0	0	9	
	12	1023.8	W 3	÷37.5	86	> 50	00	0	0	0	0	9	0	0	3	
	15	1023.3	W 4	÷37.3	85	> 50	00	0	0	0	0	9	0	0	8	
8	18	1022.6	W 4	÷36.2	÷36.0	..	84	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1022.5	W 2	÷36.1	82	> 50	00	0	0	0	0	9	0	0	8	
	00	1022.8	W 2	÷36.7	84	> 50	00	0	0	0	0	9	0	0	4	
	03	1023.7	0	÷35.2	84	> 50	00	0	0	0	0	9	0	0	4	
	06	1024.9	0	÷37.3	..	÷38.5	82	> 50	00	0	0	0	0	9	0	0	4	0.0
9	09	1026.9	0	÷36.9	86	> 50	00	0	0	0	0	9	0	0	4	
	12	1028.5	0	÷37.6	86	> 50	00	0	0	0	0	9	0	0	3	
	15	1027.6	0	÷38.3	86	> 50	00	0	0	0	0	9	0	0	9	
	18	1026.7	0	÷37.9	÷35.2	..	85	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1026.3	W 7	÷28.1	76	> 50	00	0	0	0	0	9	0	0	8	
10	00	1024.1	W 6	÷26.2	74	> 50	00	0	0	0	0	9	0	0	8	
	03	1022.4	W 6	÷27.3	75	> 50	00	0	0	0	0	9	0	0	8	
	06	1019.9	SSW 1	÷30.2	..	÷38.5	76	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1017.9	SW 3	÷32.3	78	> 50	00	0	0	0	0	9	0	0	8	
	12	1014.5	0	÷32.6	80	> 50	00	0	0	0	0	9	0	0	9	
10	15	1012.4	W 4	÷28.7	80	> 50	03	2	8	0	0	9	2	×	8	
	18	1011.6	W 4	÷28.7	÷28.1	..	79	> 50	01	2	7	0	0	9	2	0	8	0.0
	21	1012.0	W 6	÷26.4	79	> 50	03	2	8	0	0	9	2	×	4	
	00	1011.6	W 8	÷25.9	78	> 50	03	2	8	0	0	9	2	×	0	
	03	1010.5	W 8	÷26.3	76	> 50	03	2	8	0	0	9	2	×	8	
10	06	1010.2	W 9	÷26.4	..	÷32.8	76	> 50	02	2	8	0	0	9	2	×	8	0.0
	09	1010.7	W 9	÷27.3	74	> 50	02	2	8	0	0	9	2	×	4	
	12	1009.6	W 9	÷29.1	72	> 50	02	2	8	0	0	9	2	×	9	
	15	1009.2	W 9	÷29.9	70	> 50	02	2	8	0	0	9	2	×	8	
	18	1009.0	W 8	÷31.3	÷25.7	..	71	> 50	01	2	4	0	0	9	2	0	3	0.0
10	21	1008.5	W 14	÷30.5	82	1—2	03 ¹	2	8	0	0	9	2	×	8	
	00	1008.0	W 20	÷30.5	86	0.05—0.1	39	3	8	0	0	9	2	×	8	
	03	1007.5	W 8	÷31.0	81	10—20	01	2	8	0	0	9	2	×	4	
	06	1005.3	W 3	÷31.6	..	÷31.6	76	20—50	02	2	8	0	0	9	2	×	9	0.0
	09	1002.6	W 2	÷30.9	74	20—50	02	2	8	0	0	9	2	×	9	
10	12	998.0	SE 7	÷35.4	84	20—50	02	2	8	0	0	9	2	×	9	
	15	995.9	E 4	÷36.1	86	> 50	02	2	8	0	0	9	2	×	8	
	18	994.7	0	÷36.3	÷30.3	..	86	> 50	02	2	8	0	0	9	2	×	8	0.0

¹ Strong snow drift on Bronlund's Fjord, not by the station.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
11	21	996.1	W 12	÷28.8	78	> 50	01	2	6	0	0	9	0	9	4	
	00	999.1	W 11	÷31.3	75	> 50	03	2	6	0	0	9	0	9	3	
	03	1002.5	NW 8	÷35.1	75	> 50	03	2	6	0	0	9	0	9	3	
	06	1004.7	0	÷39.2	..	÷39.4	80	> 50	03	2	7	0	0	9	0	9	3	0.0
	09	1005.9	W 9	÷33.9	74	20—50	03	2	8	8	0	8	2	×	3	
	12	1006.9	W 14	÷34.6	76	20—50	03	2	8	8	0	8	2	×	3	
	15	1007.9	W 17	÷36.3	88	0.05—0.2	39	3	8	8	0	8	2	×	3	
	18	1007.8	W 19	÷35.4	÷28.8	90	< 0.05	39	3	8	8	0	8	2	×	3
12	21	1004.8	W 24	÷34.4	90	0—0.02	39	3	8	9	×	×	×	×	9	
	00	1003.4	W 26 ¹	÷34.7	95	0—0.02	39	3	9	9	×	×	×	×	8	
	03	1003.4	W 24	÷34.3	94	0—0.02	39	3	9	9	×	×	×	×	3	
	06	1003.3	W 27	÷33.3	..	÷39.3	96	0—0.02	39	3	9	9	×	×	×	×	3	×
	09	1003.6	W 26	÷33.1	96	0—0.02	39	3	9	9	×	×	×	×	3	
	12	1003.2	W 16	÷28.3	90	0—0.02	39	3	9	9	×	×	×	×	4	
	15	1003.4	W 19	÷28.7	98	0.08—0.1	39	3	8	0	0	9	0	9	9	
	18	1002.5	W 16	÷27.9	÷27.9	..	×	0.1—0.2	39	3	8	0	0	9	2	0	8	0.0
13	21	1001.9	W 16	÷26.5	×	0.1—0.2	39	3	8	0	0	9	2	0	8	
	00	999.3	WSW 16	÷26.6	×	0.1—0.2	39	3	8	0	0	9	1	0	9	
	03	996.6	WSW 15	÷25.7	95	0.08—0.1	37	3	8	0	0	9	2	0	8	
	06	998.0	W 15	÷24.8	..	÷33.6	95	0.08—0.1	37	3	8	0	0	9	2	0	4	0.0
	09	999.9	W 15	÷24.9	×	4—10	36	3	8	0	0	9	2	0	4	
	12	1001.7	W 10	÷26.1	×	4—10	36	3	8	0	0	9	2	×	3	
	15	1002.6	W 7	÷27.3	69	20—50	01	1	4	0	0	9	0	5	3	
	18	1003.1	W 7	÷28.2	÷25.6	..	69	> 50	03	2	5	0	0	9	0	6	3	0.0
14	21	1003.4	W'S 3	÷28.6	69	> 50	01	0	2	0	0	9	0	5	3	
	00	1005.5	0	÷31.7	75	> 50	01	0	0	0	0	9	0	0	4	
	03	1006.7	0	÷32.2	78	> 50	00	0	0	0	0	9	0	0	3	
	06	1008.5	0	÷33.3	..	÷33.3	78	> 50	03	2	8	0	0	9	0	7	4	0.0
	09	1011.2	E 2	÷33.1	78	> 50	03	2	8	0	0	9	0	7	4	
	12	1013.3	0	÷33.7	78	> 50	02	2	8	0	0	9	0	7	4	
	15	1014.7	ENE 3	÷34.2	79	> 50	02	2	8	0	0	9	0	7	3	
	18	1016.2	ENE 3	÷34.3	÷28.2	..	79	> 50	02	2	8	0	0	9	0	7	3	0.0
15	21	1017.4	E 3	÷34.2	79	> 50	01	2	6	0	0	9	0	8	3	
	00	1017.8	0	÷35.2	79	> 50	01	0	1	0	0	9	0	9	1	
	03	1018.0	0	÷36.1	79	> 50	02	0	1	0	0	9	0	9	3	
	06	1017.6	SE 2	÷37.2	..	÷37.3	78	> 50	00	0	0	0	0	9	0	0	0	0.0
	09	1017.0	SSW 1	÷37.5	78	> 50	00	0	0	0	0	9	0	0	8	
	12	1015.6	0	÷37.1	78	> 50	00	0	0	0	0	9	0	0	9	
	15	1013.6	0	÷37.9	78	> 50	00	0	0	0	0	9	0	0	9	
	18	1012.7	0	÷38.3	÷34.0	..	79	> 50	00	0	0	0	0	9	0	0	8	0.0
16	21	1011.2	0	÷39.0	79	> 50	00	0	0	0	0	9	0	0	8	
	00	1011.0	0	÷38.6	78	> 50	00	0	0	0	0	9	0	0	8	
	03	1009.8	0	÷39.0	79	> 50	00	0	0	0	0	9	0	0	8	
	06	1009.4	0	÷38.9	..	÷39.3	79	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1011.4	W'N 2	÷37.1	78	> 50	03	0	1	1	0	8	4	0	4	
	12	1012.0	W'S 4	÷35.3	76	> 50	03	0	2	0	0	9	0	5	1	
	15	1013.0	W'S 5	÷34.5	71	> 50	02	0	2	0	0	9	0	5	3	
	18	1014.1	W 2	÷34.9	÷34.2	..	72	> 50	02	0	2	0	0	9	0	9	3	0.0

¹ Wind 32—33 m/sec. in the gusts.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
17	21	1014.3	W 2	÷35.8	73	> 50	03	0	6	0	0	9	0	9	3	
	00	1015.0	0	÷36.6	74	> 50	01	0	2	0	0	9	0	9	3	
	03	1016.1	0	÷38.3	76	> 50	01	0	0	0	0	9	0	0	3	
	06	1017.8	0	÷38.9	..	÷39.2	78	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1017.9	0	÷38.3	78	> 50	00	0	0	0	0	9	0	0	1	
	12	1019.5	0	÷38.7	76	> 50	00	0	0	0	0	9	0	0	4	
18	15	1019.6	SW 3	÷38.4	74	> 50	00	0	0	0	0	9	0	0	3	
	18	1019.9	SW 1	÷38.2	÷34.7	..	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1020.9	SW 4	÷37.9	71	> 50	00	0	0	0	0	9	0	0	3	
	00	1021.7	SW 1	÷38.3	72	> 50	00	0	0	0	0	9	0	0	3	
	03	1022.0	W 1	÷37.7	72	> 50	00	0	0	0	0	9	0	0	3	
	06	1021.7	0	÷38.5	..	÷39.1	71	> 50	03	0	1	0	0	9	0	9	9	0.0
19	09	1021.7	0	÷38.5	73	> 50	03	2	5	0	0	9	0	6	3	
	12	1021.5	0	÷38.7	74	> 50	03	2	6	0	0	9	0	6	9	
	15	1020.2	0	÷38.5	72	> 50	02	2	6	0	0	9	0	6	8	
	18	1019.4	W 2	÷38.3	÷37.3	..	72	> 50	02	2	6	0	0	9	0	6	8	0.0
	21	1018.4	W 5	÷36.3	71	> 50	03	2	8	0	0	9	0	7	8	
	00	1018.2	0	÷35.9	71	> 50	01	2	6	0	0	9	0	7	8	
20	03	1018.0	0	÷36.0	72	> 50	03	2	8	0	0	9	0	7	8	
	06	1017.9	0	÷36.2	..	÷38.9	72	> 50	01	2	8	0	0	9	0	7	8	0.0
	09	1018.1	W 1	÷36.1	72	> 50	02	2	8	0	0	9	0	7	4	
	12	1018.7	0	÷35.7	72	> 50	02	2	8	0	0	9	0	7	3	
	15	1018.3	0	÷35.3	73	> 50	02	2	8	0	0	9	0	7	3	
	18	1018.3	0	÷35.1	÷35.0	..	74	> 50	02	2	8	0	0	9	0	7	3	0.0
21	21	1018.8	0	÷34.3	74	> 50	02	2	8	0	0	9	0	7	3	
	00	1019.1	0	÷34.1	75	> 50	02	2	8	0	0	9	0	7	3	
	03	1020.5	0	÷33.9	76	> 50	02	2	8	0	0	9	0	7	4	
	06	1020.8	W 3	÷33.3	..	÷36.3	75	> 50	02	2	8	0	0	9	0	7	3	0.0
	09	1021.2	W'N 4	÷32.1	74	> 50	01	0	1	0	0	9	0	7	3	
	12	1020.9	W'N 2	÷32.1	74	> 50	00	0	0	0	0	9	0	0	9	
22	15	1020.1	0	÷29.1	72	> 50	03	0	1	0	0	9	0	5	8	
	18	1018.7	W 4	÷30.4	÷28.9	..	71	> 50	03	0	2	0	0	9	6	5	9	0.0
	21	1018.3	0	÷31.3	73	20-50	03	0	3	0	0	9	6	5	8	
	00	1015.5	0	÷31.6	74	20-50	02	0	3	0	0	9	6	5	9	
	03	1011.5	NE 5	÷33.2	76	20-50	03	2	4	0	0	9	0	6	8	
	06	1009.7	0	÷33.4	..	÷33.9	77	20-50	02	0	4	0	0	9	0	6	8	0.0
23	09	1006.1	W'N 1	÷33.5	74	> 50	01	0	1	0	0	9	0	6	9	
	12	1004.4	W 6	÷31.7	76	> 50	03	1	2	0	0	9	0	6	9	
	15	1002.1	0	÷30.1	76	> 50	00	0	0	0	0	9	0	0	6	
	18	1000.7	0	÷30.0	÷28.1	..	76	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1000.0	W 2	÷29.8	74	> 50	00	0	0	0	0	9	0	0	6	
	00	1000.2	0	÷28.5	72	> 50	00	0	0	0	0	9	0	0	4	
24	03	1002.1	NE 6	÷33.5	76	> 50	00	0	0	0	0	9	0	0	3	
	06	1003.3	0	÷24.7	..	÷34.7	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1003.7	W 17	÷25.7	70	10-20	00	3	0	0	0	9	0	0	9	
	12	1004.4	W 14	÷26.1	71	20-50	00	3	0	0	0	9	0	0	4	
	15	1006.4	W 12	÷27.8	69	20-50	00	0	0	0	0	9	0	0	3	
	18	1007.9	W 11	÷25.8	÷24.2	..	67	> 50	00	0	0	0	0	9	0	0	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
23	21	1009.5	W 11	÷24.3	63	> 50	00	0	0	0	0	9	0	0	3	
	00	1011.9	W 10	÷23.7	68	> 50	00	0	0	0	0	9	0	0	4	
	03	1013.8	W 14	÷22.8	63	> 50	00	0	0	0	0	9	0	0	3	
	06	1015.0	W 14	÷23.9	..	÷33.9	65	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1015.0	W 11	÷23.7	62	> 50	00	0	0	0	0	9	0	0	3	
	12	1014.6	W 9	÷24.3	62	> 50	00	0	0	0	0	9	0	0	3	
24	15	1013.1	W 6	÷24.5	62	> 50	03	0	1	0	0	9	5	0	8	
	18	1012.6	ENE 3	÷27.5	÷21.8	..	68	> 50	02	0	1	0	0	9	5	0	8	0.0
	21	1010.6	0	÷31.6	75	> 50	02	0	1	0	0	9	5	0	8	
	00	1008.4	0	÷30.3	75	> 50	03	2	8	0	0	9	0	7	8	
	03	1005.7	0	÷30.0	76	> 50	02	2	8	0	0	9	0	7	8	
	06	1003.8	0	÷25.7	..	÷32.7	73	> 50	02	2	8	0	0	9	0	7	8	0.0
25	09	1000.5	0	÷25.3	66	> 50	01	1	3	0	0	9	0	7	9	
	12	998.4	0	÷26.1	64	> 50	02	0	3	0	0	9	0	7	8	
	15	997.0	0	÷28.7	70	> 50	03	2	6	0	0	9	0	7	8	
	18	996.1	0	÷27.5	÷25.1	..	76	> 50	03	2	8	0	0	9	0	7	8	0.0
	21	996.5	W 10	÷19.5	76	> 50	02	2	8	0	0	9	0	7	4	
	00	997.1	W 10	÷19.2	70	> 50	02	2	8	0	0	9	6	7	3	
26	03	997.1	W 6	÷18.9	68	> 50	02	2	8	0	0	9	6	7	3	
	06	996.9	0	÷20.5	..	÷29.0	72	20-50	76	7	0	0	0	9	0	7	8	trace
	09	997.4	0	÷24.5	79	20-50	01	2	7	0	0	9	0	7	4	
	12	997.7	0	÷25.5	82	> 50	01	0	2	0	0	9	0	5	3	
	15	997.7	0	÷26.2	82	> 50	03	0	2	0	0	9	5	0	3	
	18	996.1	0	÷27.7	÷17.3	..	82	> 50	01	0	1	0	0	9	0	1	9	0.0
27	21	995.4	0	÷28.1	80	> 50	03	0	3	0	0	9	0	6	8	
	00	993.7	0	÷28.3	82	20-50	02	0	3	0	0	9	0	6	9	
	03	991.3	0	÷29.5	84	10-20	71	7	8	8	0	8	2	×	8	
	06	989.6	W 4	÷28.3	..	÷29.7	84	10-20	71	7	8	8	0	8	2	×	8	0.8
	09	987.9	0	÷28.7	82	10-20	01	2	3	3	0	8	2	0	6	
	12	988.2	W 3	÷28.9	82	10-20	02	0	3	3	0	8	2	0	5	
28	15	988.3	W 2	÷29.9	80	20-50	02	0	3	3	0	8	5	0	3	
	18	988.5	W 1	÷30.0	÷26.1	..	80	20-50	03	2	4	4	0	8	7	0	3	0.0
	21	990.0	W 2	÷30.2	80	20-50	02	2	4	4	0	8	7	0	4	
	00	990.3	W 4	÷30.6	79	20-50	01	1	2	2	0	8	7	0	3	
	03	990.8	W 5	÷28.9	78	10-20	70	7	8	8	0	8	2	×	3	
	06	991.0	W 7	÷27.6	..	÷30.6	80	4-10	70	7	8	8	0	8	2	×	9	0.2
29	09	991.1	W 7	÷26.3	80	4-10	70	7	8	8	0	8	2	×	4	
	12	991.4	W 18	÷25.9	81	4-10	70	7	8	8	0	8	2	×	3	
	15	992.0	W 11	÷24.5	81	4-10	37	3	8	8	0	8	2	×	3	
	18	993.2	W 12	÷24.5	÷23.4	..	81	2-4	37	3	8	8	0	8	2	×	3	trace
	21	994.0	W 13	÷24.1	83	1-2	37	3	8	8	0	8	2	×	3	
	00	996.2	W 15	÷23.9	86	0.5-1	39	3	8	8	0	8	2	×	4	
30	03	999.0	W 16	÷22.9	87	0.5-1	39	3	8	8	0	8	2	×	4	
	06	1001.5	W 16	÷23.3	..	÷27.8	87	0.5-1	39	3	8	8	0	8	2	×	3	0.0
	09	1005.1	W 15	÷23.1	84	0.5-1	39	3	8	8	0	8	2	×	4	
	12	1007.7	W 15	÷23.0	84	0.5-1	39	3	8	8	0	8	2	×	2	
	15	1010.6	W 10	÷23.5	84	0.5-1	37	3	7	7	0	8	6	×	3	
	18	1012.4	W 14	÷24.2	÷22.4	..	83	1-2	36	3	7	7	0	8	6	×	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
29	21	1014.4	W 6	÷25.5	83	10—20	01	0	2	2	0	8	6	0	3	0.0
	00	1016.2	W 5	÷25.8	82	20—50	01	0	1	1	0	8	6	0	3	
	03	1017.8	W 2	÷27.9	82	20—50	02	0	1	1	0	8	6	0	3	
	06	1018.2	0	÷29.3	..	÷29.5	82	30—50	00	0	0	0	0	9	0	0	3	
	09	1019.9	W 2	÷30.6	82	20—50	00	0	0	0	0	9	0	0	4	
	12	1020.1	W 2	÷31.3	82	> 50	00	0	0	0	0	9	0	0	1	
	15	1019.9	W 2	÷31.7	82	> 50	00	0	0	0	0	9	0	0	9	
30	18	1018.3	W 1	÷31.3	÷24.0	..	82	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1017.8	W 1	÷33.2	82	> 50	00	0	0	0	0	9	0	0	8	
	00	1017.7	W 3	÷32.5	81	> 50	00	0	0	0	0	9	0	0	8	
	03	1018.1	0	÷32.3	82	> 50	00	0	0	0	0	9	0	0	4	
	06	1019.2	0	÷33.2	..	÷33.3	80	> 50	00	0	0	0	0	9	0	0	3	
	09	1020.1	W 2	÷32.1	79	> 50	00	0	0	0	0	9	0	0	3	
	12	1021.3	0	÷32.1	79	> 50	00	0	0	0	0	9	0	0	4	
31	15	1023.5	SW 1	÷33.1	78	> 50	03	0	1	0	0	9	4	0	3	0.0
	18	1024.6	0	÷34.2	÷31.2	..	79	> 50	03	0	1	0	0	9	4	0	3	
	21	1026.0	0	÷34.9	81	> 50	02	0	1	0	0	9	4	0	3	
	00	1026.6	0	÷35.5	82	> 50	02	0	1	0	0	9	4	0	3	
	03	1026.9	0	÷35.5	82	> 50	03	2	4	0	0	9	4	0	3	
	06	1027.9	0	÷36.5	..	÷36.8	83	> 50	01	1	1	0	0	9	4	0	3	
	09	1027.8	0	÷37.1	80	> 50	00	0	0	0	0	9	0	0	9	
Mean	12	1026.8	0	÷37.6	80	> 50	00	0	0	0	0	9	0	0	9	0.0
	15	1024.5	0	÷38.0	80	> 50	00	0	0	0	0	9	0	0	8	
	18	1022.9	0	÷37.0	÷34.0	..	82	1—2	49	4	1	0	0	9	4	0	8	
	21	1021.3	0	÷36.0	83	0.2—0.5	76	7	8	0	0	9	2	×	8	
	Mean	1012.3	4.5	÷31.4	÷28.8	÷34.3	78	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19		
1	00	1018.0	ESE 2	÷35.8	80	10—20	01	1	1	0	0	9	2	0	8	0.1		
	03	1012.6	E 9	÷35.2	80	0.5—1	76	7	6	0	0	9	2	0	9			
	06	1007.2	E 6	÷34.9	..	÷38.4	80	0.2—0.5	48	4	3	0	0	9	2	0	8			
	09	1001.8	E 5	÷34.1	76	0.2—0.5	49	4	9	9	×	×	×	×	8			
	12	998.1	0	÷31.6	77	0.2—0.5	71	7	9	9	×	×	×	×	6			
	15	995.2	W 7	÷31.5	80	0.2—0.5	71	7	9	9	×	×	×	×	8			
	18	993.2	W 8	÷30.7	÷30.5	..	80	0.2—0.5	71	7	9	9	×	×	×	×	8			
	21	991.9	W 5	÷28.9	80	0.5—1	71	7	9	9	×	×	×	×	6			
	2	00	992.2	W 14	÷26.8	78	0.2—0.5	37	3	9	9	×	×	×	×		4	0.0
		03	993.0	W 16	÷24.5	×	0.2—0.5	37	3	9	9	×	×	×	×		3	
06		994.3	W 16	÷23.4	..	÷35.0	83	0.2—0.5	37	3	9	9	×	×	×	×	3			
09		994.7	W 18	÷23.2	80	0.2—0.5	37	3	9	9	×	×	×	×	2			
12		996.6	W 20	÷23.3	80	0.2—0.5	37	3	9	9	×	×	×	×	4			
15		999.0	W 18	÷23.9	81	0.5—1	37	3	9	9	×	×	×	×	3			
18		1000.7	W 21	÷23.5	÷22.9	..	82	0.5—1	37	3	9	9	×	×	×	×	3			
21		1001.7	W 20	÷24.1	82	0.5—1	37	3	9	9	×	×	×	×	3			

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
3	00	1004.0	W 23	÷23.1	82	0.5—1	37	3	9	9	×	×	×	×	3	
	03	1006.1	W 20	÷24.3	82	0.5—1	02	2	9	9	0	6	2	×	3	
	06	1008.8	W 20	÷23.8	..	÷25.1	82	0.5—1	37	3	9	9	0	6	2	×	3	0.0
	09	1011.7	W 20	÷22.3	81	0.05—0.2	37	3	9	9	×	×	×	×	2	
	12	1014.5	W 21	÷22.3	81	0.5—1	37	3	9	9	×	×	×	×	2	
	15	1018.9	W 16	÷22.5	83	1—2	02	2	8	0	0	9	2	×	4	
	18	1019.9	W 15	÷22.3	÷22.3	..	83	10—20	02	2	8	0	0	9	2	×	1	0.0
	21	1023.3	W 11	÷22.0	81	20—50	02	2	8	0	0	9	2	×	4	
4	00	1024.2	W 8	÷22.8	80	20—50	02	2	8	0	0	9	2	×	3	
	03	1024.2	W 5	÷24.5	×	20—50	02	2	8	0	0	9	1	×	3	
	06	1022.5	W 4	÷26.2	..	÷26.4	×	20—50	01	1	3	0	0	9	1	0	9	0.0
	09	1021.5	E 5	÷24.8	×	20—50	03	2	5	0	0	9	7	0	9	
	12	1019.5	E 5	÷26.7	79	> 50	01	0	3	0	0	9	7	2	9	
	15	1018.9	W 5	÷29.3	77	20—50	02	0	3	0	0	9	7	2	4	
	18	1019.8	W 1	÷29.8	÷21.9	..	77	0.05—0.2	71	7	9	0	0	9	2	×	3	×
	21	1018.5	0	÷32.3	77	20—50	01	0	0	0	0	9	0	0	9	
5	00	1017.0	0	÷32.8	78	> 50	00	0	0	0	0	9	0	0	8	
	03	1015.1	WNW 2	÷33.3	78	0.2—0.5	48	4	6	0	0	9	1	8	8	
	06	1014.2	SW 4	÷33.4	..	÷33.7	77	20—50	01	0	0	0	0	9	0	0	8	0.1
	09	1016.1	W 5	÷32.1	73	> 50	01	0	1	0	0	9	7	0	4	
	12	1016.3	W 4	÷31.7	70	> 50	00	0	0	0	0	9	0	0	1	
	15	1017.3	W 1	÷33.3	71	> 50	00	0	0	0	0	9	0	0	3	
	18	1015.8	W 1	÷33.6	÷29.8	..	71	> 50	03	0	1	0	0	9	1	0	9	0.0
	21	1015.8	0	÷34.2	71	> 50	01	0	1	0	0	9	1	0	3	
6	00	1013.1	E 1	÷33.9	73	20—50	03	2	7	0	0	9	1	0	9	
	03	1008.1	E 6	÷31.3	75	20—50	03	2	8	0	0	9	1	0	8	
	06	1002.0	NE 8	÷31.3	..	÷34.4	75	1—2	76	7	8	0	0	9	1	1	7	0.2
	09	996.0	E 4	÷31.1	76	0.5—1	49	4	9	9	×	×	×	×	9	
	12	992.3	E 4	÷31.7	76	20—50	01	1	4	4	0	9	1	0	7	
	15	994.8	W 14	÷28.3	78	0.05—0.2	37	3	7	0	0	9	9	0	4	
	18	996.3	W 12	÷26.1	÷26.0	..	76	10—20	03	2	8	0	0	9	2	0	3	0.0
	21	999.8	W 12	÷26.2	66	10—20	02	2	8	0	0	9	9	0	2	
7	00	1000.1	W 10	÷26.1	62	10—20	02	2	8	0	0	9	9	0	1	
	03	1000.6	W 5	÷27.0	62	10—20	02	2	8	0	0	9	2	×	3	
	06	994.4	W 2	÷27.9	..	÷32.4	65	20—50	02	2	8	0	0	9	2	×	9	0.0
	09	999.6	0	÷27.6	65	20—50	02	2	8	0	0	9	2	×	4	
	12	998.6	W 1	÷27.7	68	20—50	02	2	8	8	0	8	2	×	9	
	15	997.8	0	÷27.3	76	1—2	76	7	8	8	0	7	2	×	8	
	18	996.4	0	÷27.1	÷26.1	..	76	1—2	76	7	8	8	0	7	2	×	8	trace
	21	995.8	0	÷26.5	78	1—2	76	7	8	8	0	7	2	×	8	
8	00	995.5	0	÷26.1	81	1—2	76	7	8	8	0	7	2	×	8	
	03	997.4	0	÷26.4	80	2—4	76	7	8	8	0	7	2	×	4	
	06	998.3	W 5	÷26.5	..	÷28.4	80	2—4	76	7	8	8	0	7	2	×	3	1.2
	09	999.6	W 5	÷26.5	78	2—4	76	7	8	8	0	7	2	×	3	
	12	1000.7	W 5	÷26.5	77	2—4	76	7	8	8	0	7	2	×	3	
	15	1001.6	W 5	÷26.5	78	20—50	03	0	3	0	0	9	4	9	3	
	18	1001.8	W 3	÷28.3	÷26.0	..	77	20—50	00	0	0	0	0	9	0	0	3	0.2
	21	1002.3	W 6	÷30.5	76	20—50	00	0	0	0	0	9	0	0	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
9	00	1003.2	W 7	÷29.8	76	20—50	00	0	0	0	0	9	0	0	3	
	03	1004.1	W 10	÷27.2	72	20—50	00	0	0	0	0	9	0	0	3	
	06	1005.6	W 5	÷26.5	..	÷31.0	70	> 50	03	2	5	0	0	9	0	6	3	0.0
	09	1003.8	W 5	÷26.1	68	> 50	02	2	5	0	0	9	0	6	9	
	12	1002.0	W 5	÷26.1	65	> 50	03	2	6	0	0	9	2	8	9	
	15	1000.9	W 10	÷24.6	66	20—50	03	2	8	0	0	9	2	×	8	
	18	999.7	W 11	÷22.6	÷22.6	..	68	20—50	02	2	8	0	0	9	2	×	8	0.0
	21	998.4	W 14	÷21.3	76	0.5—1	36	3	8	0	0	9	2	×	8	
10	00	998.5	W 13	÷21.2	78	0.5—1	36	3	8	0	0	9	2	×	3	
	03	999.5	W 12	÷21.0	78	0.5—1	36	3	8	0	0	9	2	×	3	
	06	1000.1	W 13	÷21.1	..	÷26.6	78	0.5—1	36	3	7	0	0	9	3	×	3	0.1
	09	1000.7	W 8	÷22.3	74	20—50	02	2	7	0	0	9	3	×	3	
	12	1000.8	W 8	÷22.4	70	> 50	03	2	8	0	0	9	7	×	4	
	15	1001.0	W 1	÷23.2	68	20—50	76	7	8	0	0	9	0	7	3	
	18	1001.4	0	÷23.9	÷20.8	..	72	2—4	76	7	8	0	0	9	0	7	3	trace
	21	1001.4	0	÷26.2	78	4—10	76	7	8	0	0	9	0	7	3	
11	00	1001.6	0	÷28.2	78	20—50	01	1	3	0	0	9	8	0	3	
	03	1001.7	0	÷28.0	80	20—50	03	2	4	0	0	9	8	0	3	
	06	1000.2	W 6	÷24.3	..	÷28.4	68	10—20	03	2	8	0	0	9	2	×	9	trace
	09	999.0	W 11	÷23.7	65	10—20	02	2	8	0	0	9	2	×	6	
	12	998.1	W 11	÷23.7	60	10—20	02	2	8	0	0	9	2	×	8	
	15	996.4	W 10	÷24.5	60	10—20	02	2	8	0	0	9	7	×	8	
	18	995.5	W 11	÷24.3	÷23.5	..	59	10—20	02	2	8	0	0	9	8	×	8	0.0
	21	993.6	W 7	÷24.3	56	20—50	02	2	8	0	0	9	8	×	8	
12	00	993.4	W 6	÷26.1	55	> 50	00	0	0	0	0	9	0	0	8	
	03	993.2	W 5	÷28.3	57	> 50	00	0	0	0	0	9	0	0	8	
	06	993.6	W 6	÷29.8	..	÷29.8	58	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	994.6	W 4	÷29.3	56	> 50	03	0	1	0	0	9	0	5	3	
	12	995.7	W 4	÷30.7	58	> 50	00	0	0	0	0	9	0	0	3	
	15	996.6	0	÷32.1	59	> 50	00	0	0	0	0	9	0	0	3	
	18	997.8	0	÷32.2	÷24.1	..	60	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	998.8	0	÷33.2	65	> 50	03	0	2	0	0	9	0	9	3	
13	00	998.9	0	÷33.9	70	> 50	03	2	4	0	0	9	0	9	3	
	03	998.0	0	÷33.5	72	> 50	03	2	6	0	0	9	0	9	9	
	06	997.2	0	÷32.9	..	÷34.5	75	1—2	03	2	8	0	0	9	0	7	8	0.0
	09	997.9	0	÷33.3	76	1—2	02	2	8	0	0	9	0	7	4	
	12	997.9	0	÷33.7	74	0.5—1	02	2	8	0	0	9	0	7	3	
	15	998.2	W 4	÷33.7	76	< 0.02	01	0	2	0	0	9	4	0	3	
	18	998.4	W 3	÷34.1	÷32.0	..	72	< 0.02	03	0	2	0	0	9	4	0	3	0.0
	21	997.8	W 4	÷33.1	70	< 0.02	01	0	1	0	0	9	4	0	9	
14	00	998.4	W 1	÷33.8	70	< 0.02	02	0	1	0	0	9	0	2	4	
	03	998.3	W 10	÷31.8	65	< 0.02	03	2	8	0	0	9	2	7	3	
	06	997.7	W 9	÷30.3	..	÷34.5	68	< 0.02	71	7	8	0	0	9	2	×	9	×
	09	996.1	W 10	÷29.1	75	< 0.02	71	7	8	0	0	9	2	×	9	
	12	994.1	W 17	÷24.9	80	< 0.02	39	3	9	9	×	×	×	×	8	
	15	990.0	W 22	÷24.2	86	< 0.02	39	3	9	9	×	×	×	×	8	
	18	988.4	W 19	÷23.5	÷23.5	..	87	< 0.02	39	3	9	9	×	×	×	×	8	×
	21	986.8	W 26	÷23.9	×	< 0.02	39	3	9	9	×	×	×	×	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
15	00	989.0	W 20	÷ 24.3	×	< 0.02	39	3	9	9	×	×	×	×	4		
	03	990.8	W 18	÷ 24.5	×	< 0.02	39	3	9	9	×	×	×	×	3		
	06	991.6	W 16	÷ 25.3	..	÷ 30.5	×	< 0.02	39	3	9	9	×	×	×	×	3	×	
	09	991.0	W 18	÷ 24.7	×	< 0.02	39	3	9	9	×	×	×	×	9		
	12	990.7	W 20	÷ 24.3	×	< 0.02	39	3	9	9	×	×	×	×	8		
	15	988.6	W 22	÷ 23.5	×	< 0.02	39	3	9	9	×	×	×	×	8		
	18	988.4	W 20	÷ 24.2	÷ 23.4	..	×	< 0.02	39	3	9	9	×	×	×	×	8	×	
	21	989.3	W 23	÷ 23.4	×	< 0.02	39	3	9	9	×	×	×	×	4		
	16	00	990.1	W 22	÷ 23.1	×	< 0.02	39	3	9	9	×	×	×	×	3	
03		991.0	W 22	÷ 23.5	×	< 0.02	39	3	9	9	×	×	×	×	3		
06		991.9	W 26	÷ 24.2	..	÷ 25.3	×	< 0.02	39	3	9	9	×	×	×	×	3	×	
09		989.5	W 27	÷ 24.1	×	< 0.02	39	3	9	9	×	×	×	×	3		
12		989.7	W 27	÷ 24.2	×	< 0.02	75	7	9	9	×	×	×	×	4		
15		990.8	W 28	÷ 24.6	×	< 0.02	75	7	9	9	×	×	×	×	3		
18		990.9	W 26	÷ 23.8	÷ 23.0	..	×	< 0.02	75	7	9	9	×	×	×	×	3	×	
21		992.5	W 26	÷ 23.2	×	< 0.02	75	7	9	9	×	×	×	×	4		
17		00	993.4	W 26	÷ 23.0	×	< 0.02	75	7	9	9	×	×	×	×	3	
	03	994.8	W 26	÷ 22.4	×	< 0.02	75	7	9	9	×	×	×	×	3		
	06	996.6	W 23	÷ 22.3	..	÷ 24.8	×	< 0.02	75	7	9	9	×	×	×	×	3	×	
	09	997.3	W 23	÷ 22.3	×	< 0.02	75	7	9	9	×	×	×	×	3		
	12	998.9	W 22	÷ 22.2	×	< 0.02	75	7	9	9	×	×	×	×	3		
	15	1000.0	W 20	÷ 22.0	×	20-50	39	3	9	9	×	×	×	×	3		
	18	1001.6	W 18	÷ 22.1	÷ 21.8	..	×	20-50	39	3	9	9	×	×	×	×	3	×	
	21	1003.9	W 17	÷ 23.0	×	10-20	00	0	0	0	0	0	9	0	0	3	
	18	00	1005.9	W 15	÷ 22.7	×	10-20	00	0	0	0	0	9	0	0	3	
03		1007.8	W 10	÷ 23.2	×	10-20	00	0	0	0	0	9	0	0	3		
06		1009.2	W 13	÷ 22.4	..	÷ 23.0	×	10-20	03	3	8	0	0	9	2	×	3	×	
09		1010.8	W 12	÷ 22.2	×	10-20	02	3	8	0	0	9	2	×	3		
12		1012.8	W 8	÷ 23.3	×	20-50	01	0	2	0	0	9	2	0	3		
15		1013.1	W 8	÷ 25.3	×	> 50	00	0	0	0	0	9	0	0	3		
18		1013.8	W 6	÷ 26.8	÷ 22.1	..	76	> 50	00	0	0	0	0	9	0	0	3	0.0	
21		1013.3	W 4	÷ 26.0	74	> 50	71	7	8	0	0	9	2	0	9		
19		00	1013.0	W 2	÷ 24.7	78	10-20	71	7	8	0	0	9	2	0	8	
	03	1012.8	0	÷ 24.0	81	10-20	71	7	8	0	0	9	2	0	8		
	06	1012.3	E 4	÷ 22.9	..	÷ 27.1	87	10-20	71	7	8	0	0	9	2	0	8	0.1	
	09	1013.5	E 2	÷ 24.3	86	20-50	03	2	8	3	0	8	2	×	4		
	12	1013.4	E 2	÷ 22.5	86	10-20	02	2	8	8	0	8	2	×	9		
	15	1011.2	0	÷ 22.2	86	2-4	71	7	8	8	0	8	2	×	9		
	18	1012.1	E 4	÷ 21.7	÷ 21.7	..	87	2-4	71	7	8	8	0	8	2	×	4	0.2	
	21	1012.1	E 1	÷ 20.3	88	2-4	71	7	8	8	0	8	2	×	3		
	20	00	1011.4	0	÷ 18.9	89	2-4	71	7	8	8	0	8	2	×	9	
03		1010.5	0	÷ 20.3	89	2-4	71	7	8	8	0	8	2	×	8		
06		1009.6	0	÷ 20.2	..	÷ 24.5	89	2-4	71	7	8	8	0	8	2	×	8	0.5	
09		1010.1	0	÷ 17.5	90	2-4	71	7	8	8	0	8	2	×	4		
12		1010.5	0	÷ 18.0	88	2-4	71	7	8	8	0	8	2	×	3		
15		1011.2	0	÷ 18.9	91	2-4	71	7	8	8	0	8	2	×	3		
18		1011.2	0	÷ 19.1	÷ 17.2	..	91	2-4	71	7	8	8	0	8	2	×	3	2.0	
21		1012.9	0	÷ 19.5	91	2-4	71	7	8	8	0	8	2	×	3		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
21	00	1013.8	0	÷18.9	91	2-4	71	7	8	8	0	8	2	×	3	0.3	
	03	1014.6	E 5	÷17.9	84	2-4	71	7	8	8	0	8	2	×	3		
	06	1015.1	E 5	÷18.3	..	÷20.3	80	2-4	71	7	8	8	0	8	2	×	3		
	09	1015.6	W 2	÷19.9	76	10-20	02	2	8	8	0	8	2	×	3		
	12	1015.6	W 2	÷19.9	76	20-50	02	2	8	8	0	8	2	×	3		
	15	1015.8	W 4	÷19.9	75	20-50	02	2	8	8	0	8	2	×	3		
	18	1015.8	0	÷20.1	÷17.5	..	80	20-50	02	2	8	8	0	8	2	×	3		trace
22	21	1015.8	0	÷23.1	84	20-50	01	2	5	0	0	9	4	0	3	0.0	
	00	1015.6	SW 2	÷25.5	85	20-50	01	2	3	0	0	9	4	0	9		
	03	1014.5	0	÷28.1	89	20-50	00	0	0	0	0	9	0	0	8		
	06	1014.2	0	÷28.5	..	÷30.1	88	20-50	00	0	0	0	0	9	0	0	8		
	09	1013.9	0	÷29.7	87	20-50	00	0	0	0	0	9	0	0	8		
	12	1013.4	0	÷30.1	87	> 50	00	0	0	0	0	9	0	0	8		
	15	1013.3	E 4	÷29.3	87	> 50	03	0	3	0	0	9	3	0	8		
23	18	1013.2	W 4	÷29.5	÷19.3	..	87	> 50	03	2	5	0	0	9	3	0	8	0.0	
	21	1012.7	W 8	÷25.1	82	> 50	03	2	8	0	0	9	2	×	9		
	00	1012.0	W 9	÷24.8	81	20-50	03	2	8	0	0	9	2	×	8		
	03	1011.9	W 10	÷23.7	83	4-10	01	2	6	0	0	9	2	0	8		
	06	1012.3	W 10	÷22.8	..	÷31.0	85	4-10	02	2	6	0	0	9	2	0	4	0.0	
	09	1013.0	W 10	÷22.5	83	20-50	02	2	7	0	0	9	2	0	3		
	12	1013.1	W 6	÷22.7	82	20-50	02	2	8	0	0	9	2	×	1		
24	15	1015.3	W 4	÷22.6	80	> 50	02	2	8	0	0	9	2	×	3	0.0	
	18	1014.9	W 7	÷23.6	÷22.3	..	80	> 50	02	2	8	0	0	9	2	×	9		
	21	1017.2	W 7	÷25.3	79	> 50	02	2	8	0	0	9	2	0	3		
	00	1018.0	W 7	÷25.7	81	> 50	01	0	2	0	0	9	0	0	3		
	03	1020.0	NW 3	÷27.9	83	> 50	00	0	0	0	0	9	0	0	3		
	06	1021.0	W 2	÷28.4	..	÷28.4	82	> 50	00	0	0	0	0	9	0	0	3		0.0
	09	1022.8	W 1	÷28.1	82	> 50	01	0	1	0	0	9	2	0	3		
25	12	1023.8	W 1	÷30.0	82	> 50	01	0	1	0	0	9	2	0	3	0.0	
	15	1024.0	W 1	÷30.7	82	> 50	00	0	0	0	0	9	0	0	3		
	18	1024.7	W 3	÷28.9	÷23.5	..	82	> 50	00	0	0	0	0	9	0	0	3		
	21	1025.5	W 2	÷31.2	82	> 50	00	0	0	0	0	9	0	0	3		
	00	1026.4	W 3	÷31.3	83	> 50	00	0	0	0	0	9	0	0	3		
	03	1028.0	0	÷32.3	83	> 50	00	0	0	0	0	9	0	0	3		
	06	1028.7	0	÷32.5	..	÷32.9	83	> 50	00	0	0	0	0	9	0	0	3		0.0
26	09	1029.3	0	÷33.1	82	> 50	03	0	1	0	0	9	5	0	3	0.0	
	12	1029.0	W 6	÷33.3	84	> 50	03	2	8	0	0	9	5	×	9		
	15	1028.3	W 3	÷32.5	83	20-50	03	2	8	0	0	9	5	×	8		
	18	1028.3	W 4	÷31.2	÷28.1	..	83	20-50	03	2	8	0	0	9	5	×	3		
	21	1028.4	W 3	÷32.4	82	20-50	01	0	4	0	0	9	5	0	3		
	00	1029.1	W 2	÷32.3	81	20-50	01	0	2	0	0	9	5	0	4		
	03	1029.8	W 3	÷32.3	82	20-50	00	0	0	0	0	9	0	0	3		
26	06	1030.8	W 3	÷34.4	..	÷34.8	82	20-50	00	0	0	0	0	9	0	0	3	0.0	
	09	1033.5	W 1	÷34.0	82	> 50	03	0	1	0	0	9	1	0	4		
	12	1035.0	W 2	÷32.7	80	> 50	03	2	5	0	0	9	1	6	3		
	15	1036.2	W 9	÷30.1	78	> 50	02	2	5	0	0	9	1	6	3		
	18	1037.4	W 6	÷28.9	÷28.9	..	77	20-50	03	2	8	0	0	9	5	×	3	0.0	
	21	1038.4	W 8	÷26.8	76	20-50	02	2	8	0	0	9	5	×	3		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
27	01	1039.8	W 6	÷26.3	73	20—50	01	2	6	0	0	9	5	0	3	0.0	
	03	1040.3	W 8	÷26.5	71	20—50	01	0	2	0	0	9	5	0	3		
	06	1040.3	W 6	÷27.5	..	÷34.5	71	20—50	02	0	2	0	0	9	5	0	3		
	09	1039.0	W 6	÷28.3	72	> 50	02	0	2	0	0	9	5	0	9		
	12	1038.3	W 6	÷29.3	73	> 50	03	0	3	0	0	9	5	0	8		
	15	1037.1	W 8	÷28.3	72	> 50	02	0	3	0	0	9	5	0	8		
	18	1037.0	W 6	÷28.3	÷26.0	72	> 50	03	2	4	0	0	9	5	0		6
	21	1037.6	0	÷29.9	80	> 50	03	2	8	0	0	9	5	×	4		
28	00	1037.6	0	÷29.0	87	> 50	02	2	8	0	0	9	2	×	3	×	
	03	1037.0	0	÷27.8	82	20—50	76	2	8	0	0	9	2	×	9		
	06	1036.9	W 7	÷26.1	..	÷29.9	78	20—50	76	2	8	0	0	9	2	×	8		
	09	1037.3	W 7	÷24.5	76	20—50	76	2	8	0	0	9	2	×	4		
	12	1037.7	W 6	÷23.9	78	> 50	02	2	8	0	0	9	2	×	3		
	15	1038.1	W 6	÷23.4	80	20—50	03	2	8	0	0	9	7	×	3		
	18	1038.2	W 9	÷23.3	÷23.1	80	20—50	02	2	8	0	0	9	7	×		3
	21	1038.5	W 9	÷23.5	80	20—50	02	2	8	0	0	9	7	×	3		
Mean	1009.0		7.6	÷26.5	÷23.9	÷29.8	72	×	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
1	00	1038.8	W 8	÷24.5	80	20—50	02	2	8	0	0	9	7	0	3	0.0	
	03	1039.1	W 10	÷24.7	79	20—50	02	2	8	0	0	9	7	0	3		
	06	1039.8	W 2	÷23.9	..	÷26.0	78	20—50	02	2	8	0	0	9	7	0	3		
	09	1042.6	E 8	÷24.1	82	20—50	02	2	8	0	0	9	7	0	4		
	12	1043.8	E 6	÷26.9	82	20—50	02	2	8	0	0	9	7	0	3		
	15	1044.8	E 5	÷26.9	82	20—50	02	2	8	0	0	9	7	0	3		
	18	1045.0	E 3	÷30.3	÷23.0	84	20—50	01	0	1	0	0	9	4	0		3
	21	1044.2	E 1	÷28.5	86	20—50	03	2	8	0	0	9	7	0	9		
2	00	1042.9	0	÷29.0	85	20—50	01	2	6	0	0	9	7	0	8	0.0	
	03	1041.3	0	÷31.3	85	20—50	01	0	2	0	0	9	7	0	8		
	06	1037.5	0	÷32.5	..	÷32.5	86	> 50	01	0	1	0	0	9	4	0	9		
	09	1034.4	NE 3	÷34.1	86	> 50	02	0	1	0	0	9	4	0	8		
	12	1029.9	NE 6	÷34.7	84	4—10	40	0	3	0	0	9	4	2	8		
	15	1024.1	NE 6	÷30.3	86	2—4	40	2	6	0	0	9	5	2	8		
	18	1018.3	NE 9	÷29.4	÷27.4	86	0.5—1	48	4	8	0	0	9	7	×		8
	21	1011.3	SE 16	÷27.4	87	0.5—1	48	4	8	0	0	9	7	×	8		
3	00	1008.0	SE 20	÷26.1	90	0.2—0.5	48	4	8	0	0	9	2	×	8	0.0	
	03	1004.1	E 20	÷23.4	90	0.5—1	36	3	8	0	0	9	2	×	8		
	06	1005.3	E 8	÷24.6	..	÷35.4	92	10—20	01	0	2	0	0	9	7	0	4		
	09	1006.8	0	÷24.9	×	> 50	02	0	2	0	9	9	7	0	3		
	12	1007.5	SE 2	÷30.1	×	> 50	03	0	3	0	0	9	7	2	3		
	15	1007.6	SW 6	÷29.4	×	> 50	02	0	3	0	0	9	5	2	3		
	18	1006.2	SW 4	÷28.3	÷22.8	×	> 50	03	2	6	0	0	9	5	2		9
	21	1002.6	W 4	÷27.4	×	0.5—1	71	7	8	0	0	9	2	×	8		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
4	00	1000.6	W 14	÷24.8	×	0.5—1	73	7	8	0	0	9	2	×	8	
	03	998.0	W 12	÷23.6	×	0.5—1	73	7	8	0	0	9	2	×	8	
	06	995.7	W 17	÷22.5	..	÷31.0	×	< 0.05	73	7	8	0	0	9	2	×	8	trace
	09	995.2	W 24	÷23.5	×	< 0.05	73	7	8	0	0	9	2	×	8	
	12	995.6	W 24	÷24.5	×	< 0.02	39	7	9	9	×	×	×	×	4	
	15	996.4	W 26	÷24.9	×	< 0.02	39	3	9	9	×	×	×	×	3	
	18	998.4	W 25	÷25.3	÷22.0	..	×	< 0.05	39	3	9	9	×	×	×	×	4	trace
5	21	1000.3	W 26	÷25.5	×	0.05—0.2	39	3	9	9	×	×	×	×	3	
	00	1001.7	W 28	÷25.1	×	< 0.05	39	3	9	9	×	×	×	×	3	
	03	1003.0	W 26	÷24.5	×	< 0.05	39	3	8	0	0	9	2	×	3	
	06	1004.5	W 23	÷24.5	..	÷26.1	×	0.05—0.2	39	3	8	0	0	9	2	×	3	0.0
	09	1006.3	W 14	÷24.3	×	0.2—0.5	02	3	8	0	0	9	2	×	3	
	12	1007.8	W 12	÷23.3	×	2—4	02	3	8	0	0	9	2	×	3	
	15	1009.5	W 10	÷23.3	×	2—4	40	1	4	0	0	9	4	3	3	
6	18	1012.0	W 13	÷22.8	÷22.8	..	×	0.2—0.5	36	3	4	0	0	9	4	3	4	0.0
	21	1014.4	W 16	÷21.5	×	0.2—0.5	36	3	4	0	0	9	0	3	3	
	00	1017.0	W 13	÷22.0	×	0.5—1	36	3	2	0	0	9	0	0	3	
	03	1019.2	W 11	÷22.4	68	> 50	00	0	0	0	0	9	0	0	3	
	06	1020.5	W 7	÷22.3	..	÷24.5	62	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1022.4	W 6	÷24.5	64	> 50	00	0	0	0	0	9	0	0	3	
	12	1024.6	0	÷25.1	64	> 50	00	0	0	0	0	9	0	0	4	
7	15	1025.9	0	÷26.8	72	> 50	00	0	0	0	0	9	0	0	3	
	18	1026.8	E 6	÷30.3	÷21.2	..	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1028.9	E 2	÷31.2	78	> 50	00	0	0	0	0	9	0	0	3	
	00	1030.5	0	÷32.7	80	> 50	03	0	1	0	0	9	4	0	3	
	03	1030.0	0	÷33.8	81	> 50	02	0	1	0	0	9	4	9	9	
	06	1029.6	0	÷34.3	..	÷34.3	82	> 50	02	0	1	0	0	9	4	0	8	0.0
	09	1029.6	0	÷34.2	84	> 50	02	0	1	0	0	9	0	0	3	
8	12	1028.1	0	÷34.1	83	> 50	00	0	0	0	0	9	0	0	9	
	15	1026.0	0	÷34.1	82	> 50	00	0	0	0	0	9	0	0	8	
	18	1024.6	0	÷34.0	÷30.3	..	80	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1021.6	0	÷34.4	80	> 50	00	0	0	0	0	9	0	0	9	
	00	1019.2	0	÷34.2	79	> 50	00	0	0	0	0	9	0	0	8	
	03	1017.9	0 ¹	÷34.3	79	> 50	02	0	1	0	0	9	0	5	8	
	06	1014.4	0	÷34.8	..	÷35.2	80	> 50	02	0	1	0	0	9	4	0	9	0.0
9	09	1010.3	0	÷34.9	82	> 50	03	2	8	0	0	9	1	×	8	
	12	1006.9	0	÷33.9	82	> 50	03	2	8	0	0	9	7	×	8	
	15	1004.5	W 6	÷30.1	80	> 50	02	2	8	0	0	9	7	×	8	
	18	1003.5	W 8	÷25.3	÷25.3	..	82	0.5—1	71	7	8	0	0	9	2	×	6	0.1
	21	1003.7	W 11	÷24.2	88	2—4	37	3	8	0	0	9	2	9	4	
	00	1004.9	W 11	÷22.8	90	0.05—0.2	37	3	8	0	0	9	2	9	3	
	03	1006.5	W 18	÷21.9	84	0.05—0.2	37	3	4	0	0	9	0	9	3	
9	06	1009.0	W 18	÷21.9	..	÷35.0	85	0.2—0.5	37	3	3	1	9	5	0	9	3	trace
	09	1011.3	W 13	÷24.3	88	2—4	02	3	3	0	0	9	2	0	3	
	12	1014.0	W 17	÷23.5	77	1—2	03	3	8	0	0	9	7	×	0	
	15	1013.0	W 12	÷22.1	72	> 50	01	2	4	0	0	9	7	9	8	
	18	1012.9	W 11	÷22.3	÷21.5	..	72	20—50	03	2	8	0	0	9	7	9	6	0.0
	21	1011.7	W 13	÷21.5	80	0.5—1	36	3	8	0	0	9	1	7	9	

¹ 0030—0200 Wind from W. 3—4 m/sec.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
10	00	1010.7	W 13	÷21.7	82	0.5-1	36	3	8	0	0	9	1	7	8	
	03	1008.4	W 13	÷21.8	84	0.5-1	35	3	4	0	0	9	0	7	9	
	06	1005.1	W 13	÷21.8	..	÷25.2	85	0.5-1	36	3	8	0	0	9	1	7	9	0.0
	09	1002.8	W 14	÷22.3	85	0.5-1	36	3	8	0	0	9	2	×	8	
	12	1000.5	W 13	÷23.3	×	0.5-1	36	3	8	0	0	9	2	×	8	
	15	999.1	W 16	÷23.4	×	< 0.02	39	3	8	0	0	9	2	×	6	
	18	999.0	W 16	÷23.7	÷21.0	..	×	< 0.02	75	7	9	0	0	9	×	×	6	×
11	21	999.4	W 22	÷24.3	×	< 0.02	75	7	9	0	0	9	×	×	3	
	00	999.6	W 20	÷24.7	×	< 0.02	75	7	9	9	×	×	×	×	3	
	03	1000.5	W 22	÷25.1	×	< 0.02	75	7	9	9	×	×	×	×	3	
	06	1001.4	W 16	÷24.8	..	÷25.5	×	< 0.05	37	3	9	9	×	×	×	×	3	×
	09	1003.3	W 14	÷22.3	×	< 0.05	37	3	9	9	×	×	×	×	4	
	12	1003.9	W 14	÷22.7	×	< 0.05	37	3	9	9	×	×	×	×	3	
	15	1004.2	W 13	÷22.4	×	0.5-1	36	3	4	0	0	0	3	0	3	
12	18	1004.4	W 12	÷22.1	÷22.0	..	×	20-50	03	2	8	0	0	0	7	×	3	0.0
	21	1008.1	W 5	÷23.8	×	> 50	01	1	3	0	0	0	4	2	4	
	00	1009.9	W 8	÷23.5	66	> 50	01	0	1	1	1	6	0	0	3	
	03	1013.3	W 10	÷24.7	67	> 50	00	0	0	0	0	9	0	0	3	
	06	1016.2	W 12	÷24.5	..	÷25.2	67	> 50	03	0	1	0	0	9	0	2	3	0.0
	09	1019.3	W 13	÷23.5	65	> 50	03	2	8	0	0	9	2	×	3	
	12	1020.1	W 14	÷22.5	72	> 50	02	2	8	0	0	9	2	×	1	
13	15	1021.0	W 16	÷20.6	70	0.5-1	37	3	8	0	0	9	2	×	3	
	18	1022.1	W 17	÷20.1	÷19.8	..	×	< 0.05	37	3	8	0	0	9	2	×	3	0.0
	21	1023.4	W 20	÷19.9	×	< 0.05	37	3	8	0	0	9	2	×	3	
	00	1024.4	W 20	÷20.2	×	< 0.05	37	3	8	0	0	9	2	×	3	
	03	1025.5	W 20	÷20.2	×	< 0.05	37	3	8	0	0	9	2	×	3	
	06	1027.0	W 18	÷20.2	..	÷25.0	×	< 0.05	37	3	8	0	0	9	2	×	3	0.0
	09	1027.4	W 17	÷19.7	×	0.5-1	37	3	8	0	0	9	2	×	1	
14	12	1028.1	W 18	÷19.7	×	< 0.05	37	3	8	0	0	9	2	×	9	
	15	1027.1	W 18	÷19.2	×	< 0.05	37	3	8	0	0	9	2	×	8	
	18	1026.6	W 18	÷19.2	÷19.0	..	×	< 0.02	37	3	8	0	0	9	2	×	8	0.0
	21	1026.9	W 20	÷19.1	×	< 0.02	37	3	8	0	0	9	2	×	4	
	00	1028.0	W 21	÷19.2	×	< 0.02	37	3	8	0	0	9	2	×	3	
	03	1028.0	W 21	÷18.9	×	< 0.02	37	3	9	0	0	9	2	×	3	
	06	1028.9	W 19	÷18.3	..	÷20.4	×	0.02-0.04	37	3	8	0	0	9	2	×	9	0.0
15	09	1030.3	W 18	÷17.9	×	0.02-0.04	37	3	8	0	0	9	2	×	4	
	12	1031.3	W 19	÷17.5	×	0.02-0.04	37	3	8	0	0	9	2	×	3	
	15	1031.6	W 16	÷17.0	×	0.05-0.2	37	3	8	0	0	9	2	×	3	
	18	1031.6	W 16	÷17.0	÷17.0	..	×	0.05-0.2	37	3	8	0	0	9	2	×	3	0.0
	21	1031.9	W 11	÷16.5	×	0.5-1	36	3	8	0	0	9	2	×	3	
	00	1033.0	W 10	÷16.1	×	20-50	02	2	8	0	0	9	2	×	3	
	03	1033.2	W 5	÷16.8	×	20-50	02	2	8	0	0	9	2	×	3	
15	06	1031.9	W 4	÷17.1	..	÷18.3	82	20-50	02	2	8	0	0	9	2	×	9	trace
	09	1029.8	W 3	÷17.1	85	20-50	02	2	8	0	0	9	7	×	8	
	12	1029.5	W 2	÷16.3	84	> 50	01	2	6	0	0	9	7	0	6	
	15	1026.1	W 2	÷17.8	85	> 50	01	0	4	0	0	9	0	2	9	
	18	1023.9	W 1	÷19.8	÷15.8	..	86	> 50	02	0	4	0	0	9	0	2	8	0.0
21	1022.1	W 3	÷20.2	88	> 50	00	0	0	0	0	9	0	0	8		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
16	00	1019.0	0	÷21.9	89	> 50	00	0	0	0	0	9	0	0	9	
	03	1016.1	W 5	÷21.5	88	> 50	00	0	0	0	0	9	0	0	8	
	06	1014.9	W 1	÷21.2	..	÷23.4	85	> 50	00	0	0	0	0	9	0	0	8	
	09	1014.8	W 2	÷20.3	86	> 50	03	0	1	0	0	9	0	5	6	
	12	1014.8	W 9	÷13.5	70	> 50	00	0	0	0	0	9	0	0	3	
	15	1015.4	SW 4	÷14.9	66	> 50	00	0	0	0	0	9	0	0	3	
	18	1015.7	0	÷16.9	÷11.5	..	64	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1015.9	0	÷20.1	71	> 50	00	0	0	0	0	9	0	0	3	
17	00	1016.3	0	÷21.5	74	> 50	00	0	0	0	0	9	0	0	3	
	03	1018.4	0	÷25.1	78	> 50	00	0	0	0	0	9	0	0	4	
	06	1020.2	SE 3	÷24.2	..	÷25.5	82	> 50	03	0	1	0	0	9	4	0	3	0.0
	09	1023.0	0	÷26.5	80	> 50	02	0	1	0	0	9	4	0	3	
	12	1025.3	0	÷26.9	81	> 50	03	0	1	0	0	9	2	0	3	
	15	1026.3	0	÷25.3	82	> 50	03	2	7	0	0	9	7	0	3	
	18	1028.1	0	÷24.8	÷17.0	..	82	> 50	02	2	7	0	0	9	5	0	3	0.0
	21	1031.2	0	÷27.5	86	> 50	01	2	6	0	0	9	4	0	3	
18	00	1030.9	0	÷28.5	87	> 50	02	0	1	0	0	9	4	0	1	
	03	1030.1	0	÷28.8	87	> 50	00	0	0	0	0	9	0	0	9	
	06	1028.1	0	÷29.5	..	÷30.4	87	> 50	00 ¹	0	0	0	0	9	0	0	8	0.0
	09	1028.3	0	÷30.5	86	> 50	03	0	1	0	0	9	4	0	4	
	12	1025.6	0	÷30.0	87	> 50	02	0	1	0	0	9	4	0	9	
	15	1020.3	0	÷30.1	90	> 50	02	0	1	0	0	9	4	0	9	
	18	1017.0	E 2	÷31.1	÷24.8	..	90	> 50	03	0	2	2	5	4	0	0	8	0.0
	21	1011.7	0	÷32.5	89	> 50	03	2	6	0	0	9	5	0	8	
19	00	1008.7	0	÷32.9	88	10—20	40	0	0	0	0	9	0	0	6	
	03	1007.6	W 6	÷32.9	89	> 50	40	0	0	0	0	9	0	0	8	
	06	1006.6	0	÷33.5	..	÷34.7	89	> 50	00 ²	0	0	0	0	9	0	0	8	0.0
	09	1004.1	0	÷32.5	88	> 50	00	0	0	0	0	9	0	0	9	
	12	1003.6	W 3	÷30.3	88	> 50	00	0	0	0	0	9	0	0	8	
	15	1002.5	0	÷30.2	88	> 50	00	0	0	0	0	9	0	0	8	
	18	1002.2	NE 2	÷32.1	÷29.2	..	87	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1001.7	W 3	÷33.2	87	> 50	00	0	0	0	0	9	0	0	8	
20	00	1000.4	W 4	÷33.4	86	> 50	00	0	0	0	0	9	0	0	8	
	03	1001.6	0	÷30.8	87	> 50	00	0	0	0	0	9	0	0	4	
	06	1001.9	W 1	÷30.5	..	÷34.0	86	> 50	03	0	1	0	0	9	4	0	3	0.0
	09	1002.2	0	÷30.1	84	> 50	03	2	5	0	0	9	5	0	3	
	12	1004.8	0	÷32.1	84	> 50	03	2	7	0	0	9	5	×	4	
	15	1005.3	0	÷30.5	85	> 50	02	2	7	0	0	9	5	×	3	
	18	1006.1	0	÷30.0	÷30.0	..	85	> 50	02	2	7	0	0	9	5	0	3	0.0
	21	1006.9	0	÷29.9	84	> 50	02	2	7	0	0	9	5	0	3	
21	00	1006.3	0	÷30.2	82	> 50	01	0	1	0	0	9	5	0	9	
	03	1005.9	W 3	÷30.8	81	> 50	02	0	1	0	0	9	5	0	8	
	06	1004.3	NW 1	÷30.9	..	÷32.8	82	> 50	03	2	8	0	0	9	2	0	9	0.0
	09	1001.6	W 5	÷24.5	82	> 50	02	2	8	0	0	9	2	×	9	
	12	998.3	W 7	÷24.3	80	> 50	02	2	8	0	0	9	2	×	8	
	15	994.5	W 7	÷21.6	80	0.5—1	40	2	8	0	0	9	2	×	8	
	18	991.6	W 4	÷21.3	÷21.2	..	89	1—2	71	7	8	0	0	9	2	×	8	trace
	21	990.6	W 1	÷21.3	90	1—2	71	7	8	0	0	9	2	×	8	

¹ Frost haze on Independence Fjord 0800. ² Soft rime.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
22	00	990.4	W 1	÷21.3	91	1—2	02	2	7	0	0	9	7	×	6	
	03	991.0	W 1	÷23.2	91	> 50	01	2	5	0	0	9	7	0	3	
	06	995.1	0	÷26.5	..	÷31.0	91	> 50	01	0	3	0	0	9	4	0	4	0.1
	09	1001.7	0	÷25.5	90	> 50	03	2	5	5	0	8	2	0	3	
	12	1004.1	0	÷23.3	90	> 50	02	2	5	5	0	8	2	0	3	
	15	1007.1	0	÷22.5	84	> 50	01	2	4	0	0	9	5	0	3	
18	1008.4	0	÷23.4	÷20.2	78	> 50	01	0	3	0	0	9	5	0	3	0.0
	21	1010.4	0	÷25.2	80	> 50	01	0	2	0	0	9	5	0	3	
	00	1011.8	S 2	÷27.9	81	> 50	01	0	1	0	0	9	5	0	3	
23	03	1012.8	0	÷30.5	85	> 50	02	0	1	0	0	9	5	0	3	
	06	1013.7	0	÷32.5	..	÷32.5	86	> 50	02	0	1	0	0	9	1	0	3	0.0
	09	1013.4	S 2	÷31.1	81	> 50	00	0	0	0	0	9	0	0	9	
	12	1014.0	0	÷30.5	79	> 50	03	0	1	0	0	9	1	0	9	
	15	1014.6	0	÷30.9	74	> 50	00	0	0	0	0	9	0	0	4	
	18	1014.1	0	÷29.9	÷23.7	..	74	> 50	00	0	0	0	0	9	0	0	9	0.0
24	21	1014.3	0	÷29.8	74	> 50	00	0	0	0	0	9	0	0	4	
	00	1013.9	0	÷31.3	76	> 50	02	0	1	0	0	9	4	0	8	
	03	1014.0	0	÷32.0	77	> 50	02	0	1	0	0	9	4	0	4	
	06	1014.3	0	÷32.8	..	÷33.4	78	> 50	02	0	1	0	0	9	4	0	3	0.0
	09	1014.2	0	÷29.5	77	> 50	02	0	1	0	0	9	4	0	9	
	12	1014.0	0	÷28.1	76	> 50	03	0	3	0	0	9	4	0	8	
25	15	1013.4	0	÷25.3	72	> 50	03	0	4	2	1	6	4	2	8	
	18	1013.0	W 4	÷25.1	÷24.2	..	75	> 50	03	0	4	2	1	6	4	2	8	0.0
	21	1012.7	0	÷28.1	78	> 50	03	0	5	2	1	6	4	0	8	
	00	1012.6	W 1	÷27.5	78	> 50	03	2	8	0	0	9	7	0	8	
	03	1012.0	0	÷27.7	80	> 50	02	2	8	0	0	9	7	0	9	
	06	1009.4	0	÷28.1	..	÷33.0	81	> 50	02	2	8	0	0	9	7	0	8	0.0
26	09	1009.0	0	÷28.5	80	> 50	02	2	8	0	0	9	7	0	8	
	12	1007.2	0	÷29.5	80	> 50	01	1	3	0	0	9	4	0	9	
	15	1004.9	0	÷27.2	81	> 50	03	2	8	0	0	9	4	0	8	
	18	1001.1	SE 4	÷23.2	÷23.2	..	78	> 50	76	7	8	0	0	9	7	0	9	trace
	21	997.6	SE 6	÷21.2	76	2—4	71	7	8	7	6	5	2	×	8	
	00	996.1	0	÷21.3	82	2—4	71	7	8	7	6	5	2	×	8	
27	03	992.6	SE 7	÷19.8	85	0.2—0.5	71	7	8	8	6	4	×	×	9	
	06	991.0	ESE 3	÷17.3	..	÷30.4	88	> 50	02	2	8	0	0	9	7	0	6	0.2
	09	991.2	0	÷13.3	72	10—20	02	2	8	8	6	4	×	×	4	
	12	992.2	SW 4	÷13.5	90	2—4	72	7	8	8	6	4	×	×	4	
	15	994.2	W 10	÷17.5	80	20—50	36	3	2	2	6	6	0	0	3	
	18	997.1	W 15	÷21.3	÷ 9.6	..	82	0.5—1	37	3	1	1	2	6	0	0	3	×
27	21	1003.9	W 16	÷24.8	78	0.5—1	37	3	5	1	2	6	4	0	4	
	00	1006.1	W 16	÷26.9	78	1—2	03	2	8	0	0	9	7	0	3	
	03	1009.5	W 15	÷28.5	80	1—2	02	2	8	0	0	9	7	0	3	
	06	1011.5	W 16	÷29.8	..	÷30.0	82	0.2—0.5	37	3	8	0	0	9	7	0	3	0.0
	09	1013.3	W 13	÷30.1	77	4—10	01	2	6	4	3	7	4	1	3	
	12	1012.7	W 14	÷28.9	78	4—10	02	2	6	4	3	7	4	1	9	
27	15	1010.5	W 16	÷26.8	80	0.5—1	37	3	8	0	0	9	7	0	8	
	18	1009.3	W 14	÷24.1	÷21.0	..	86	0.5—1	37	3	8	0	0	9	7	0	8	0.0
	21	1010.0	W 16	÷22.9	88	0.5—1	36	3	8	0	0	9	7	×	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
28	00	1009.5	W 17	÷22.3	×	0.5—1	37	3	8	0	0	9	2	×	9	
	03	1011.8	W 14	÷20.8	×	2—4	02	2	8	0	0	9	2	×	2	
	06	1011.2	W 14	÷20.2	..	÷29.9	×	4—10	02	2	8	0	0	9	2	×	9	0.0
	09	1013.1	W 10	÷18.5	×	20—50	02	2	8	0	0	9	2	×	2	
	12	1014.6	W 11	÷18.1	×	20—50	02	2	8	0	0	9	2	×	3	
	15	1015.2	W 12	÷17.3	70	> 50	01	2	6	2	9	6	7	4	3	
29	18	1015.0	W 12	÷17.1	÷17.0	..	70	> 50	01	2	5	2	9	6	7	4	9	0.0
	21	1016.2	W 15	÷18.5	70	> 50	01	0	4	2	9	6	4	0	4	
	00	1016.4	W 11	÷18.3	71	> 50	02	0	4	2	9	6	4	0	3	
	03	1016.8	W 13	÷19.0	71	> 50	03	2	6	1	9	6	4	0	3	
	06	1017.4	W 12	÷20.3	..	÷20.5	76	> 50	03	2	7	2	9	6	4	0	3	0.0
	09	1018.4	W 10	÷19.5	71	> 50	03	2	7	2	9	6	4	2	3	
30	12	1018.5	W 8	÷19.1	74	> 50	01	2	6	0	0	9	4	2	0	
	15	1018.0	W 9	÷18.5	70	> 50	02	2	6	0	0	9	4	2	9	
	18	1016.5	W 12	÷18.2	÷18.1	..	69	> 50	03	2	8	0	0	9	7	×	8	0.0
	21	1017.6	W 14	÷16.7	64	> 50	02	2	8	0	0	9	7	×	4	
	00	1018.0	W 16	÷17.3	66	> 50	02	2	8	0	0	9	7	×	3	
	03	1018.2	W 13	÷18.1	70	> 50	02	2	8	0	0	9	7	×	3	
31	06	1018.4	W 15	÷17.9	..	÷20.4	88	> 50	37	3	8	0	0	9	7	×	3	0.0
	09	1019.4	W 19	÷18.5	78	0.5—1	02	2	8	0	0	9	7	×	1	
	12	1021.8	W 16	÷17.5	72	> 50	02	2	8	0	0	9	7	×	2	
	15	1022.0	W 17	÷16.7	68	> 50	02	2	8	0	0	9	7	×	1	
	18	1022.5	W 10	÷17.5	÷16.4	..	73	> 50	01	2	5	2	9	6	4	4	3	0.0
	21	1022.5	W 10	÷17.5	73	> 50	01	2	4	1	9	6	4	4	3	
Mean	00	1022.6	W 6	÷16.8	72	> 50	03	2	8	0	0	9	7	×	3	
	03	1020.4	W 7	÷17.3	70	> 50	02	2	8	0	0	9	7	×	9	
	06	1018.9	W 10	÷16.5	..	÷19.2	63	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1019.3	W 8	÷17.4	67	> 50	02	2	8	0	0	9	7	×	4	
	12	1018.4	W 6	÷16.6	65	> 50	02	2	8	0	0	9	7	×	9	
	15	1018.3	W 10	÷15.2	62	> 50	02	2	8	0	0	9	7	×	8	
18	1018.2	W 11	÷15.2	÷15.0	..	70	> 50	02	2	8	0	0	9	7	×	8	0.0	
21	1019.0	W 9	÷15.3	68	> 50	02	2	8	0	0	9	7	×	4		
Mean	1014.4	7.9	÷24.5	÷21.7	÷28.4	78	0.3

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1020.2	W 9	÷16.3	70	> 50	02	2	8	0	0	9	7	×	3	
	03	1020.7	W 8	÷16.5	70	> 50	02	2	8	0	0	9	7	×	3	
	06	1021.0	W 11	÷17.6	..	÷17.7	72	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1020.4	W 11	÷19.3	70	> 50	01	2	7	0	0	9	7	0	9	
	12	1022.7	W 16	÷19.5	68	> 50	01	2	6	0	0	9	7	0	4	
	15	1023.5	W 15	÷19.9	72	> 50	02	2	6	0	0	9	7	0	3	
2	18	1021.1	W 9	÷19.5	÷15.0	..	73	> 50	01	2	5	0	0	9	7	4	3	0.0
	21	1024.7	W 10	÷19.5	69	> 50	03	2	6	0	0	9	7	4	3	
	00	1025.4	W 10	÷19.4	72	> 50	03	2	8	0	0	9	7	×	3	
	03	1025.2	W 6	÷19.9	70	> 50	02	2	8	0	0	9	7	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1025.4	W 4	÷20.5	..	÷20.5	71	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1025.6	S 2	÷22.5	70	> 50	00	0	0	0	0	9	0	0	3	
	12	1025.6	SE 6	÷21.5	74	> 50	03	0	2	0	0	9	3	0	3	
	15	1024.6	E 5	÷21.5	74	> 50	03	2	8	0	0	9	0	7	9	
	18	1023.9	E 5	÷22.1	÷19.2	..	80	> 50	02	2	8	0	0	9	0	7	8	0.0
	21	1023.1	E 3	÷24.5	85	> 50	02	2	8	0	0	9	0	7	8	
3	00	1022.1	0	÷26.3	84	> 50	02	2	8	0	0	9	0	7	8	
	03	1020.8	0	÷28.0	86	> 50	01	0	0	0	0	9	0	0	8	
	06	1020.3	0	÷28.3	..	÷28.3	87	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1019.1	0	÷28.5	84	> 50	03	2	4	0	0	9	0	0	9	
	12	1018.3	W 2	÷25.5	82	> 50	02	2	4	0	0	9	0	6	8	
	15	1017.3	W 3	÷24.6	76	> 50	02	2	4	0	0	9	0	6	8	
	18	1015.6	0	÷24.1	÷22.0	..	75	> 50	03	2	5	0	0	9	0	6	8	0.0
	21	1015.6	0	÷25.7	85	> 50	03	2	7	0	0	9	7	6	3	
4	00	1014.1	0	÷26.5	86	> 50	03	2	8	0	0	9	0	7	9	
	03	1016.0	0	÷26.9	86	> 50	02	2	8	0	0	9	0	7	4	
	06	1018.6	0	÷27.3	..	÷28.4	87	2—4	02	2	8	0	0	9	0	7	3	trace
	09	1019.2	SSW 1	÷27.5	86	20—50	02	2	8	0	0	9	0	7	3	
	12	1019.6	0	÷26.1	80	20—50	01	2	5	0	0	9	0	7	3	
	15	1019.0	0	÷26.1	76	> 50	01	0	3	0	0	9	0	7	9	
	18	1018.5	0	÷26.1	÷24.0	..	78	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1018.2	0	÷28.2	79	> 50	00	0	0	0	0	9	0	0	8	
5	00	1018.0	0	÷30.0	81	> 50	00	0	0	0	0	9	0	0	8	
	03	1018.4	SSW 1	÷31.4	81	> 50	00	0	0	0	0	9	0	0	4	
	06	1018.4	0	÷32.3	..	÷32.3	82	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1018.3	0	÷31.3	81	> 50	00	0	0	0	0	9	0	0	3	
	12	1019.0	0	÷28.6	74	> 50	00	0	0	0	0	9	0	0	3	
	15	1018.6	0	÷27.1	71	> 50	00	0	0	0	0	9	0	0	9	
	18	1017.9	W 11	÷23.5	÷23.5	..	71	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1018.4	W 11	÷23.1	69	> 50	03	0	2	0	0	9	4	0	4	
6	00	1019.0	W 9	÷23.1	66	> 50	03	2	8	0	0	9	7	×	3	
	03	1020.3	W 8	÷23.3	67	> 50	02	2	6	0	0	9	7	×	3	
	06	1020.4	W 2	÷23.9	..	÷32.8	68	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1019.2	0	÷25.1	68	> 50	01	2	4	0	0	9	7	0	9	
	12	1018.3	0	÷24.3	68	> 50	00	0	0	0	0	9	0	0	8	
	15	1017.1	0	÷23.5	69	> 50	00	0	0	0	0	9	0	0	8	
	18	1015.1	0	÷22.0	÷21.8	..	66	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1013.9	0	÷25.5	74	> 50	00	0	0	0	0	9	0	0	8	
7	00	1013.4	0	÷27.7	78	> 50	00	0	0	0	0	9	0	0	6	
	03	1013.0	0	÷28.6	79	> 50	00	0	0	0	0	9	0	0	6	
	06	1013.0	0	÷29.3	..	÷29.9	78	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1013.4	0	÷26.7	74	> 50	00	0	0	0	0	9	0	0	4	
	12	1013.6	0	÷24.3	68	> 50	00	0	0	0	0	9	0	0	3	
	15	1014.2	E 3	÷24.7	72	> 50	00	0	0	0	0	9	0	0	3	
	18	1014.4	E 4	÷24.5	÷22.0	..	74	> 50	03	0	1	0	0	9	0	5	3	0.0
	21	1015.1	E 4	÷26.7	80	> 50	03	2	5	0	0	9	5	0	3	
8	00	1015.6	0	÷28.1	82	> 50	01	0	2	0	0	9	4	0	3	
	03	1016.4	0	÷29.1	83	> 50	03	2	4	0	0	9	4	9	3	
	06	1017.5	0	÷30.5	..	÷30.8	84	> 50	02	2	4	0	0	9	4	9	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1018.8	E 3	÷27.1	83	10—20	03	2	8	8	6	5	×	×	3	
	12	1019.9	NE 5	÷28.3	84	4—10	71	7	8	8	6	5	×	×	3	
	15	1022.3	E 6	÷27.7	85	4—10	71	7	5	6	6	5	0	9	4	
	18	1023.5	E 5	÷27.5	÷24.3	..	85	20—50	01	0	1	1	6	5	0	0	1	trace
	21	1025.9	E 4	÷28.0	84	> 50	00	0	0	0	0	9	0	0	4	
9	00	1027.1	0	÷28.6	84	> 50	00	0	0	0	0	9	0	0	3	
	03	1028.1	0	÷30.5	85	> 50	00	0	0	0	0	9	0	0	1	
	06	1028.1	0	÷30.5	..	÷30.8	85	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1027.9	0	÷28.7	84	> 50	00	0	0	0	0	9	0	0	9	
	12	1027.0	W 2	÷26.7	82	> 50	00	0	0	0	0	9	0	0	8	
	15	1024.2	W 4	÷24.1	77	> 50	00	0	0	0	0	9	0	0	9	
	18	1023.3	W 2	÷23.1	÷23.1	..	74	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1021.3	W 5	÷23.6	74	> 50	00	0	0	0	0	9	0	0	8	
10	00	1019.9	W 2	÷26.1	76	> 50	03	2	4	0	0	9	7	0	8	
	03	1018.2	W 3	÷25.5	76	> 50	03	2	8	0	0	9	7	0	8	
	06	1017.2	W 2	÷25.1	..	÷30.5	76	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1015.2	0	÷22.5	76	> 50	02	2	8	0	0	9	7	×	9	
	12	1015.9	W 2	÷22.9	75	> 50	01	2	7	0	0	9	7	0	4	
	15	1013.6	0	÷22.1	70	> 50	01	2	5	0	0	9	7	0	9	
	18	1012.8	W 3	÷20.7	÷20.4	..	72	> 50	03	2	7	0	0	9	7	0	8	0.0
	21	1011.3	0	÷21.9	73	> 50	03	2	8	0	0	9	7	0	8	
11	00	1011.3	E 2	÷24.3	81	> 50	02	2	8	0	0	9	7	0	9	
	03	1010.8	S 2	÷24.2	82	> 50	02	2	8	0	0	9	7	0	9	
	06	1011.2	W 4	÷23.5	..	÷25.0	82	> 50	02	2	8	0	0	9	7	0	9	0.0
	09	1011.2	W 2	÷23.1	80	> 50	02	2	8	0	0	9	7	0	9	
	12	1011.4	W 3	÷21.5	79	> 50	02	2	8	0	0	9	7	0	9	
	15	1010.9	W 3	÷18.1	71	> 50	02	2	8	0	0	9	7	0	9	
	18	1010.7	W 7	÷15.8	÷15.4	..	70	> 50	02	2	8	0	0	9	7	0	9	0.0
	21	1010.1	E 7	÷20.2	76	> 50	02	2	8	0	0	9	7	0	9	
12	00	1011.4	E 3	÷21.1	78	> 50	02	2	8	0	0	9	7	0	9	
	03	1010.5	SE 5	÷20.4	86	1—2	71	7	8	0	0	9	7	0	8	
	06	1009.4	SE 9	÷20.4	..	÷23.5	86	1—2	71	7	8	0	0	9	7	0	4	0.1
	09	1008.9	0	÷21.3	87	10—20	01	2	5	2	6	4	7	9	4	
	12	1008.1	0	÷20.7	85	10—20	03	2	8	1	6	4	7	×	4	
	15	1005.6	W 2	÷21.5	84	10—20	01	2	5	1	6	4	7	×	4	
	18	1003.4	W 5	÷20.5	÷14.3	..	88	1—2	70 ¹	7	8	3	7	5	2	×	5	trace
	21	1002.1	W 10	÷20.1	90	0.5—1	70	7	8	3	7	5	2	×	5	
13	00	999.7	W 10	÷19.5	92	0.5—1	70	7	8	3	7	5	2	×	5	
	03	998.6	W 15	÷19.3	92	1—2	70	7	8	3	7	5	2	×	5	
	06	997.7	W 15	÷19.6	..	÷21.7	85	1—2	70	7	8	0	0	9	7	×	9	×
	09	998.5	W 15	÷20.5	85	4—10	01	2	6	0	0	9	7	0	9	
	12	1000.7	W 14	÷20.2	80	4—10	03	2	8	0	0	9	7	×	4	
	15	1001.4	W 10	÷19.9	72	> 50	01	0	0	0	0	9	0	0	3	
	18	1002.1	W 11	÷20.1	÷19.0	..	68	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1002.6	W 9	÷20.6	66	> 50	00	0	0	0	0	9	0	0	3	
14	00	1003.6	W 6	÷22.1	66	> 50	03	2	7	0	0	9	0	2	3	
	03	1006.1	W 7	÷23.5	67	> 50	02	2	7	0	0	9	0	2	4	
	06	1008.1	0	÷24.0	..	÷24.0	68	> 50	01	0	1	0	0	9	0	2	3	0.0
	09	1010.1	E 4	÷23.2	76	> 50	03	2	8	0	0	9	1	×	3	

¹ Fog.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1012.0	E 4	÷24.1	78	> 50	02	2	8	0	0	9	1	×	3	
	15	1012.6	E 2	÷23.9	78	2-4	70	7	8	0	0	9	2	×	3	
	18	1013.0	0	÷23.3	÷19.8	..	82	2-4	70	7	8	8	6	6	×	×	3	0.2
	21	1010.8	W 7	÷22.5	85	2-4	70	7	8	8	6	6	×	×	9	
15	00	1008.7	W 11	÷22.3	86	1-2	70	7	8	8	6	6	×	×	8	
	03	1006.6	W 13	÷22.3	91	0.2-0.5	70	7	8	8	6	6	×	×	8	
	06	1004.8	W 16	÷21.8	..	÷24.6	96	0.2-0.5	70	7	8	8	6	6	×	×	8	×
	09	1003.8	W 16	÷21.8	96	0.2-0.5	70	7	8	8	6	6	×	×	8	
	12	1003.6	W 17	÷21.8	96	0.2-0.5	70	7	8	0	0	9	7	×	6	
	15	1003.0	W 17	÷21.5	96	< 0.05	70	7	8	0	0	9	7	×	9	
	18	1002.8	W 19	÷21.5	÷21.3	..	98	< 0.05	39	3	8	0	0	9	7	×	8	×
	21	1002.6	W 19	÷21.8	98	< 0.05	39	3	8	0	0	9	7	×	8	
16	00	1003.2	W 19	÷22.3	98	0.05-0.2	39	3	8	0	0	9	7	×	4	
	03	1005.0	W 16	÷23.2	98	0.05-0.2	39	3	8	0	0	9	7	×	4	
	06	1005.7	W 15	÷23.2	..	÷23.3	97	0.2-0.5	39	3	8	0	0	9	7	×	3	×
	09	1006.4	W 15	÷22.3	×	0.5-1	37	3	8	0	0	9	7	×	3	
	12	1007.7	W 16	÷21.9	×	0.5-1	37	3	8	0	0	9	7	×	4	
	15	1008.5	W 15	÷21.3	×	2-4	02	3	8	0	0	9	7	×	3	
	18	1009.0	W 14	÷21.2	÷21.0	..	×	> 50	01	2	6	0	0	9	4	3	3	0.0
	21	1009.2	W 8	÷21.8	69	> 50	01	0	0	0	0	9	0	0	3	
17	00	1009.6	W 8	÷22.0	69	> 50	03	2	6	0	0	9	2	0	3	
	03	1010.5	W 6	÷22.6	69	> 50	02	2	6	0	0	9	2	3	4	
	06	1010.5	SE 6	÷24.1	..	÷24.3	72	20-50	40	2	8	0	0	9	7	×	3	0.0
	09	1011.9	E 4	÷23.8	86	2-4	03 ¹	2	8	8	6	0	×	×	4	
	12	1012.0	0	÷23.5	88	2-4	02 ¹	2	8	8	6	0	×	×	1	
	15	1011.6	0	÷23.5	89	4-10	02 ²	2	8	5	6	0	7	×	9	
	18	1010.9	0	÷23.5	÷21.0	..	94	> 50	01	0	0	0	0	9	0	0	8	0.0
	21	1010.8	0	÷24.5	89	> 50	00	0	0	0	0	9	0	0	8	
18	00	1010.4	0	÷25.5	92	> 50	00	0	0	0	0	9	0	0	8	
	03	1010.2	0	÷25.8	86	> 50	00	0	0	0	0	9	0	0	8	
	06	1010.2	0	÷25.0	..	÷26.3	80	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1010.0	W 6	÷24.4	76	> 50	00	0	0	0	0	9	0	0	9	
	12	1010.2	W 8	÷22.5	74	> 50	00	0	0	0	0	9	0	0	4	
	15	1009.0	W 8	÷21.5	74	> 50	00	0	0	0	0	9	0	0	9	
	18	1009.0	W 7	÷20.5	÷20.5	..	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1009.0	W 11	÷20.5	68	> 50	00	0	0	0	0	9	0	0	3	
19	00	1009.5	W 10	÷21.5	69	> 50	00	0	0	0	0	9	0	0	4	
	03	1009.8	W 11	÷23.1	70	> 50	00	0	0	0	0	9	0	0	3	
	06	1010.1	W 12	÷23.0	..	÷24.1	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1010.9	W 16	÷21.0	72	> 50	00	0	0	0	0	9	0	0	4	
	12	1011.6	W 17	÷20.5	72	> 50	00	0	0	0	0	9	0	0	3	
	15	1012.4	W 12	÷19.6	72	> 50	00	0	0	0	0	9	0	0	3	
	18	1013.4	W 12	÷19.2	÷19.1	..	72	> 50	03	0	2	0	0	9	4	0	3	0.0
	21	1015.3	W 15	÷19.6	72	> 50	03	2	4	0	0	9	4	0	4	
20	00	1016.5	W 15	÷20.5	72	> 50	02	2	4	0	0	9	4	0	3	
	03	1018.2	W 11	÷22.1	74	> 50	02	0	2	0	0	9	4	0	3	
	06	1019.7	W 12	÷21.4	..	÷23.0	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1021.2	W 12	÷21.1	72	> 50	00	0	0	0	0	9	0	0	3	
	12	1023.0	W 12	÷20.0	70	> 50	00	0	0	0	0	9	0	0	3	

¹ Mist. ² Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1024.8	W 12	÷18.8	70	> 50	00	0	0	0	0	9	0	0	3	
	18	1025.9	W 12	÷18.2	÷17.8	..	69	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1027.1	W 11	÷18.5	68	> 50	00	0	0	0	0	9	0	0	3	
21	00	1029.4	W 11	÷19.4	68	> 50	00	0	0	0	0	9	0	0	4	
	03	1031.2	W 8	÷20.8	70	> 50	00	0	0	0	0	9	0	0	3	
	06	1033.0	W 3	÷21.8	..	÷22.4	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1034.0	0	÷20.5	70	> 50	03	0	3	0	0	9	7	0	1	
	12	1034.0	0	÷19.5	70	> 50	01	0	1	0	0	9	4	4	3	
	15	1033.1	0 ¹	÷19.8	68	> 50	02	0	1	0	0	9	4	4	9	
	18	1032.1	0	÷19.2	÷18.9	..	68	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1031.4	E 2	÷20.0	73	> 50	00	0	0	0	0	9	0	0	8	
22	00	1030.5	SE 4	÷22.0	72	> 50	03	0	1	0	0	9	0	2	8	
	03	1029.8	SE 3	÷23.3	77	> 50	02	0	1	0	0	9	0	2	8	
	06	1029.1	0	÷24.2	..	÷24.9	80	> 50	01	0	0	0	0	9	0	0	8	0.0
	09	1029.0	0	÷22.5	80	> 50	03	0	2	0	0	9	0	5	3	
	12	1028.7	0	÷21.5	78	> 50	02	0	2	0	0	9	0	5	9	
	15	1027.5	ENE 2	÷19.9	76	> 50	01	0	0	0	0	9	0	0	8	
	18	1026.8	E 2	÷20.2	÷19.4	..	76	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1026.7	ENE 3	÷21.8	78	> 50	00	0	0	0	0	9	0	0	6	
23	00	1026.6	E 1	÷22.7	78	> 50	00	0	0	0	0	9	0	0	8	
	03	1026.6	0	÷24.4	86	> 50	00	0	0	0	0	9	0	0	8	
	06	1025.8	0	÷24.2	..	÷25.3	84	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1026.1	0	÷22.0	84	> 50	00	0	0	0	0	9	0	0	9	
	12	1025.8	W 2	÷21.0	82	> 50	00	0	0	0	0	9	0	0	9	
	15	1024.9	0	÷18.8	77	> 50	00	0	0	0	0	9	0	0	8	
	18	1024.9	ENE 3	÷19.7	÷18.4	..	78	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1025.1	ENE 4	÷21.3	79	> 50	00	0	0	0	0	9	0	0	3	
24	00	1026.2	0	÷22.6	82	> 50	00	0	0	0	0	9	0	0	4	
	03	1026.0	SW 2	÷24.4	84	> 50	00	0	0	0	0	9	0	0	9	
	06	1026.2	0	÷23.3	..	÷24.8	84	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1026.2	0	÷21.6	83	> 50	00	0	0	0	0	9	0	0	3	
	12	1026.2	0	÷20.0	81	> 50	00	0	0	0	0	9	0	0	3	
	15	1024.7	0	÷18.2	77	> 50	00	0	0	0	0	9	0	0	9	
	18	1024.4	ENE 4	÷18.8	÷17.6	..	80	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1023.9	E 2	÷20.5	82	> 50	00	0	0	0	0	9	0	0	8	
25	00	1023.0	0	÷21.5	82	> 50	00	0	0	0	0	9	0	0	8	
	03	1022.5	0	÷22.9	89	> 50	00	0	0	0	0	9	0	0	8	
	06	1022.8	W 1	÷23.6	..	÷24.9	87	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1022.6	0	÷20.0	86	> 50	00	0	0	0	0	9	0	0	9	
	12	1022.4	W 3	÷17.5	78	> 50	00	0	0	0	0	9	0	0	8	
	15	1021.4	W 4	÷15.8	70	> 50	00	0	0	0	0	9	0	0	9	
	18	1020.6	0	÷14.4	÷13.6	..	65	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1019.9	0	÷14.4	68	> 50	00	0	0	0	0	9	0	0	8	
26	00	1019.0	0	÷16.8	72	> 50	03 ²	0	2	0	0	9	0	6	8	
	03	1018.5	0	÷20.6	80	> 50	03	2	6	0	0	9	0	6	8	
	06	1017.5	NW 3	÷18.8	..	÷23.5	82	> 50	03	2	7	0	0	9	0	6	8	0.0
	09	1016.6	W 5	÷15.6	76	> 50	02	2	7	0	0	9	0	6	8	
	12	1015.3	W 8	÷14.0	69	> 50	01	2	2	0	0	9	0	3	9	

¹ 1400 Wind 2-4 m/sec. E.² Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1012.7	W 11	÷12.1	62	> 50	02	0	2	0	0	9	0	3	8	
	18	1011.0	W 11	÷10.6	÷10.4	..	60	> 50	03	2	8	0	0	9	0	7	8	0.0
	21	1009.6	W 12	÷ 9.8	60	2-4	02	2	8	4	6	1	2	7	8	
27	00	1009.0	W 11	÷11.2	88	2-4	02	2	8	8	6	0	2	7	8	
	03	1009.6	W 14	÷11.5	100	2-4	70 ¹	7	6	0	0	9	7	7	4	
	06	1011.1	W 12	÷12.2	..	÷18.8	96	2-4	03	2	8	4	6	2	7	×	4	0.3
	09	1011.8	W 13	÷13.0	92	4-10	01	2	7	3	6	3	7	0	1	
	12	1012.2	W 13	÷12.9	87	4-10	01	2	5	0	0	9	4	2	3	
	15	1012.9	W 15	÷12.1	81	> 50	01	2	4	0	0	9	4	2	3	
	18	1012.9	W 13	÷12.8	÷ 9.0	..	77	> 50	03	2	6	0	0	9	7	2	3	0.0
	21	1013.7	W 11	÷13.1	76	> 50	02	2	6	1	9	9	7	2	4	
28	00	1014.5	W 12	÷13.9	76	> 50	03 ²	2	8	0	0	9	7	×	3	
	03	1014.7	W 15	÷14.3	100	0.5-1	36	3	8	8	6	0	7	×	3	
	06	1013.5	W 16	÷14.1	..	÷14.9	100	0.5-1	36	3	8	8	6	0	7	×	9	×
	09	1013.5	W 15	÷13.2	100	0.5-1	36	3	8	8	6	4	×	×	3	
	12	1013.6	W 15	÷12.0	89	4-10	02	2	8	8	6	4	×	×	4	
	15	1013.6	W 11	÷11.6	76	4-10	02	2	8	8	6	4	×	×	3	
	18	1013.9	W 8	÷11.8	÷11.2	..	70	4-10	02	2	8	2	6	4	2	×	3	0.0
	21	1015.9	W 12	÷13.6	79	20-50	01	0	2	0	0	9	4	0	4	
29	00	1019.2	W 7	÷15.5	80	> 50	01	0	1	0	0	9	4	0	4	
	03	1019.8	W 12	÷16.6	78	> 50	01	0	0	0	0	9	0	0	1	
	06	1021.0	W 14	÷15.4	..	÷17.8	74	> 50	03	0	1	0	0	9	4	9	3	0.0
	09	1022.6	W 14	÷15.2	76	20-50	03	2	7	0	0	9	4	9	3	
	12	1023.0	W 16	÷15.0	84	10-20	03	2	8	0	0	9	2	×	1	
	15	1022.2	W 17	÷13.2	80	4-10	02	2	8	0	0	9	2	×	9	
	18	1021.5	W 16	÷13.8	÷11.1	..	90	4-10	02	2	8	2	6	4	2	×	8	0.0
	21	1021.5	W 18	÷14.2	100	4-10	02 ³	2	8	2	6	4	2	×	3	
30	00	1021.7	W 16	÷14.5	100	0.5-1	37	3	8	8	6	1	×	×	3	
	03	1023.2	W 20	÷14.5	100	0.5-1	37	3	8	8	6	1	×	×	4	
	06	1023.9	W 15	÷14.3	..	÷15.4	100	0.05-0.2	37	3	8	8	6	0	×	×	1	0.0
	09	1025.6	W 15	÷13.7	100	0.05-0.2	37	3	8	8	6	0	×	×	4	
	12	1027.6	W 17	÷12.8	×	0.05-0.2	37	3	8	8	6	0	×	×	3	
	15	1028.2	W 16	÷12.3	×	10-20	02	2	8	0	0	9	7	×	1	
	18	1029.0	W 16	÷12.2	÷12.0	..	×	> 50	01	2	7	0	0	9	7	2	3	0.0
	21	1030.1	W 14	÷12.0	60	> 50	01	2	6	0	0	9	7	9	4	
	Mean	1017.0		6.3	÷21.2	÷18.3	÷2 4.4	80	×

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1031.3	W 12	÷12.3	80	> 50	02	2	6	0	0	9	7	9	3	
	03	1032.1	W 12	÷12.5	81	> 50	01	0	4	0	0	9	4	9	3	
	06	1032.4	W 10	÷11.9	..	÷14.5	78	> 50	01	0	1	0	0	9	4	9	1	0.0
	09	1032.8	W 7	÷12.0	80	> 50	02	0	1	0	0	9	0	9	3	
	12	1032.8	W 5	÷10.9	80	> 50	03 ⁴	2	8	0	0	9	0	7	3	
	15	1031.1	W 5	÷ 9.6	77	> 50	02	2	5	0	0	9	0	8	9	

¹ Snow drift. ² Fog coming from Wandels Dal. ³ Snow and sand drift. ⁴ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1030.6	W 4	÷ 9.0	÷ 9.0	..	74	> 50	01	0	2	0	0	9	0	8	8	0.0
	21	1028.3	W 1	÷ 8.9	75	> 50	00	0	0	0	0	9	0	0	9	
2	00	1028.3	E'S 4	÷ 11.0	84	> 50	00	0	0	0	0	9	0	0	3	
	03	1027.2	E 2	÷ 14.9	100	> 50	03	0	1	0	0	9	0	6	9	
	06	1026.5	0	÷ 14.3	..	÷ 15.2	90	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1026.0	0	÷ 13.2	90	> 50	00	0	0	0	0	9	0	0	8	
	12	1025.4	W 3	÷ 10.5	84	> 50	03 ¹	2	4	0	0	9	0	6	8	
	15	1023.2	W 4	÷ 8.2	75	> 50	01	0	1	0	0	9	0	5	9	
	18	1023.2	0	÷ 7.3	÷ 7.1	..	74	> 50	02	0	1	0	0	9	0	5	3	0.0
	21	1023.2	0	÷ 7.5	70	> 50	02	0	1	0	0	9	0	5	3	
3	00	1024.2	0	÷ 10.8	90	> 50	03	2	7	0	0	9	0	6	9	
	03	1024.9	0	÷ 11.0	100	> 50	01	2	4	0	0	9	0	6	3	
	06	1025.6	0	÷ 11.5	..	÷ 14.2	100	> 50	03	2	4	0	0	9	2	6	3	0.0
	09	1026.3	W 5	÷ 7.5	84	> 50	03	2	6	0	0	9	2	6	3	
	12	1027.1	W 8	÷ 6.8	70	> 50	03	2	7	0	0	9	2	5	3	
	15	1027.8	W 11	÷ 4.7	62	> 50	01	0	1	0	0	9	4	0	3	
	18	1028.1	W 12	÷ 4.4	÷ 3.7	..	62	> 50	03	0	1	0	0	9	4	5	1	0.0
	21	1028.9	W 9	÷ 5.0	62	> 50	03	2	4	0	0	9	4	0	4	
4	00	1030.1	E 5	÷ 8.5	80	> 50	03	2	7	0	0	9	7	0	4	
	03	1030.4	E'N 4	÷ 10.2	97	> 50	01	0	1	0	0	9	7	0	1	
	06	1031.4	E'N 3	÷ 10.5	..	÷ 11.5	100	> 50	02	0	1	0	0	9	7	0	4	0.0
	09	1031.4	E'N 3	÷ 10.1	90	> 50	02	0	1	0	0	9	7	0	3	
	12	1031.0	W 7	÷ 5.0	68	> 50	03	0	2	0	0	9	0	5	9	
	15	1030.4	W 6	÷ 4.2	64	> 50	00	0	0	0	0	9	0	0	8	
	18	1029.6	W 8	÷ 3.2	÷ 2.8	..	64	> 50	03	0	2	0	0	9	4	5	8	0.0
	21	1030.1	E 7	÷ 8.5	90	> 50	01	0	1	0	0	9	0	5	4	
5	00	1030.4	E 7	÷ 10.0	88	> 50	00	0	0	0	0	9	0	0	3	
	03	1030.6	E 4	÷ 12.0	93	> 50	00	0	0	0	0	9	0	0	1	
	06	1030.9	E 7	÷ 14.6	..	÷ 14.6	90	> 50	03	0	1	0	0	9	0	5	3	0.0
	09	1030.6	E 7	÷ 14.1	90	> 50	02	0	1	0	0	9	0	5	9	
	12	1030.2	E 7	÷ 15.0	90	> 50	40	0	1	0	0	9	0	5	8	
	15	1029.1	E 5	÷ 15.0	90	> 50	40	0	0	0	0	9	0	0	9	
	18	1028.3	E 4	÷ 14.2	÷ 3.0	..	90	> 50	40	0	0	0	0	9	0	0	8	0.0
	21	1027.0	E 3	÷ 15.0	90	> 50	40	0	0	0	0	9	0	0	9	
6	00	1026.3	E 4	÷ 15.8	90	10-20	40	0	0	0	0	9	0	0	8	
	03	1025.5	E 3	÷ 16.7	90	10-20	40	0	0	0	0	9	0	0	8	
	06	1024.7	E 3	÷ 16.2	..	÷ 16.9	90	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1023.7	E 3	÷ 15.0	90	> 50	00	0	0	0	0	9	0	0	8	
	12	1022.9	E 3	÷ 13.5	90	> 50	03	0	1	0	0	9	0	0	8	
	15	1021.8	E 6	÷ 13.8	90	> 50	02	0	1	0	0	9	0	0	8	
	18	1020.6	E 6	÷ 12.7	÷ 12.4	..	90	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1019.6	E 7	÷ 13.3	90	> 50	00	0	0	0	0	9	0	0	8	
7	00	1018.6	E'S 6	÷ 13.2	90	> 50	00	0	0	0	0	9	0	0	8	
	03	1017.5	E'S 4	÷ 14.1	90	> 50	00	0	0	0	0	9	0	0	8	
	06	1016.4	E'S 4	÷ 13.0	..	÷ 14.3	90	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1016.9	E'S 6	÷ 12.6	86	> 50	00	0	0	0	0	9	0	0	4	
	12	1016.5	E 6	÷ 12.5	85	> 50	03	0	1	0	0	9	0	0	9	
	15	1015.5	E'N 6	÷ 12.0	80	> 50	03	2	4	0	0	9	0	0	9	
	18	1016.0	E'N 6	÷ 11.6	÷ 11.4	..	82	> 50	03	2	5	0	0	9	0	0	4	0.0

¹ Solar halo and 4 par helion.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	21	1016.1	E'N 6	÷11.5	80	> 50	03	2	7	0	0	9	0	0	3	
8	00	1016.2	SE 5	÷11.3	75	> 50	03	2	8	0	0	9	0	0	3	
	03	1016.4	E 4	÷12.6	80	> 50	02	2	8	0	0	9	0	0	3	
	06	1016.5	E 3	÷14.5	..	÷14.6	83	> 50	01	0	1	0	0	9	0	0	3	0.0
	09	1016.7	0	÷12.6	80	> 50	02	0	1	0	0	9	0	0	3	
	12	1016.7	E 3	÷11.5	85	> 50	02	0	1	0	0	9	0	5	3	
	15	1014.5	ENE 3	÷11.4	81	> 50	01	0	1	0	0	9	0	5	9	
	18	1012.5	ENE 8	÷11.5	÷11.2	..	83	> 50	02	0	1	0	0	9	0	5	8	0.0
	21	1010.9	ENE 5	÷11.3	80	> 50	03	0	2	0	0	9	4	0	8	
9	00	1009.5	SE 10	÷11.6	76	> 50	01	0	1	0	0	9	4	0	8	
	03	1008.4	SE 7	÷12.7	75	> 50	00	0	0	0	0	9	0	0	8	
	06	1007.5	SE 6	÷12.6	..	÷12.9	64	> 50	03	0	1	0	0	9	0	5	8	0.0
	09	1007.0	SE 3	÷12.5	72	> 50	03	2	6	0	0	9	0	6	8	
	12	1007.6	SE 3	÷12.8	72	> 50	03	2	6	0	0	9	0	6	4	
	15	1007.3	SE 1	÷11.0	80	> 50	02	2	7	0	0	9	0	6	8	
	18	1007.8	SE 4	÷11.0	÷11.0	..	82	> 50	03	2	7	0	0	9	0	6	4	0.0
	21	1008.5	SE 4	÷10.4	86	> 50	01	2	6	0	0	9	0	6	3	
10	00	1009.6	SE 4	÷11.0	86	> 50	03	2	7	0	0	9	0	6	3	
	03	1010.7	0	÷12.3	84	> 50	01	2	4	0	0	9	7	0	3	
	06	1011.5	NE 2	÷12.0	..	÷12.8	84	> 50	03	2	7	0	0	9	7	2	3	0.0
	09	1012.4	E 3	÷10.1	82	> 50	01	0	2	0	0	9	7	5	3	
	12	1013.2	E'S 5	÷ 9.0	82	> 50	01	0	1	0	0	9	0	5	3	
	15	1013.3	SE 7	÷ 9.3	80	> 50	01	0	0	0	0	9	0	0	3	
	18	1011.9	SE 7	÷ 9.0	÷ 8.6	..	80	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1013.0	SE 6	÷10.4	82	> 50	00	0	0	0	0	9	0	0	4	
11	00	1013.0	NE 4	÷10.8	82	> 50	00	0	0	0	0	9	0	0	3	
	03	1013.2	SE 3	÷11.6	84	> 50	00	0	0	0	0	9	0	0	3	
	06	1013.6	W 2	÷11.6	..	÷12.3	82	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1014.3	0	÷ 9.2	74	> 50	00	0	0	0	0	9	0	0	3	
	12	1014.8	E 4	÷ 9.0	72	> 50	00	0	0	0	0	9	0	0	3	
	15	1014.0	E 6	÷10.9	79	> 50	00	0	0	0	0	9	0	0	9	
	18	1013.4	E 6	÷11.6	÷ 8.8	..	80	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1015.0	E 6	÷11.6	78	> 50	00	0	0	0	0	9	0	0	4	
12	00	1015.4	E 4	÷12.5	88	> 50	03	0	1	0	0	9	0	2	3	
	03	1015.9	E 3	÷13.2	88	> 50	03	0	2	0	0	9	0	2	3	
	06	1016.7	0	÷11.8	..	÷13.9	82	> 50	01	0	0	0	0	9	0	0	3	0.0
	09	1017.6	0	÷10.8	75	> 50	03	0	1	0	0	9	0	5	3	
	12	1018.6	E 3	÷10.2	78	> 50	03	2	7	0	0	9	0	6	3	
	15	1018.9	E 5	÷10.4	80	> 50	01	2	7	0	0	9	0	6	3	
	18	1019.1	E 5	÷10.5	÷10.2	..	78	> 50	02	2	7	0	0	9	0	6	3	0.0
	21	1019.6	SE 4	÷10.0	75	> 50	02	2	7	0	0	9	0	6	3	
13	00	1020.1	SE 4	÷11.4	80	> 50	02	2	7	0	0	9	0	6	3	
	03	1020.7	SE 2	÷10.6	82	> 50	02	2	7	0	0	9	0	6	3	
	06	1021.4	SE 2	÷10.5	..	÷12.3	80	> 50	01	0	2	0	0	9	0	6	3	0.0
	09	1021.6	E'N 3	÷ 9.5	70	> 50	03	2	6	0	0	9	0	6	1	
	12	1021.8	E'N 3	÷ 7.8	66	> 50	03	2	6	0	0	9	0	6	3	
	15	1022.4	E 4	÷ 7.4	60	> 50	02	2	6	0	0	9	0	6	3	
	18	1023.4	E 4	÷ 8.6	÷ 7.0	..	75	> 50	02	2	7	0	0	9	0	6	3	0.0
	21	1024.5	NE 3	÷ 7.6	65	> 50	01	2	6	0	0	9	0	3	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
14	00	1026.0	W 10	÷ 6.3	54	> 50	02	2	6	0	0	9	7	3	4	
	03	1026.6	W 10	÷ 7.2	54	> 50	01	2	4	0	0	9	0	3	3	
	06	1027.1	W 10	÷ 8.3	..	÷10.5	58	> 50	02	2	4	0	0	9	0	3	3	0.0
	09	1028.4	W 8	÷ 7.5	54	> 50	02	2	4	0	0	9	0	3	4	
	12	1028.4	W 6	÷ 6.5	52	> 50	02	2	4	0	0	9	0	3	3	
	15	1028.4	SE 7	÷ 7.6	59	> 50	03	2	5	0	0	9	0	3	3	
15	18	1028.4	SE 6	÷ 7.6	÷ 6.1	..	60	> 50	02	2	5	0	0	9	0	3	3	0.0
	21	1026.8	SE 7	÷ 8.3	64	> 50	02	2	5	0	0	9	0	3	9	
	00	1025.7	SE 6	÷ 9.5	65	> 50	01	0	2	0	0	9	0	3	8	
	03	1024.7	SE 5	÷ 10.4	70	> 50	01	0	1	0	0	9	0	3	8	
	06	1024.3	SE 5	÷ 11.2	..	÷11.3	75	> 50	02	0	1	0	0	9	0	3	6	0.0
	09	1024.2	SE 5	÷ 11.1	72	> 50	02	0	1	0	0	9	0	3	8	
16	12	1024.1	SE 6	÷ 11.0	72	> 50	02	0	1	0	0	9	0	3	8	
	15	1023.5	SE 6	÷ 11.0	72	> 50	01	0	0	0	0	9	0	0	8	
	18	1023.4	ESE 5	÷ 11.5	÷ 7.5	..	78	> 50	03	0	1	0	0	9	0	3	4	0.0
	21	1023.0	ESE 5	÷ 11.9	81	> 50	02	0	1	0	0	9	0	3	9	
	00	1023.3	ESE 6	÷ 12.5	78	> 50	02	0	1	0	0	9	0	3	4	
	03	1023.5	E 6	÷ 13.2	78	> 50	01	0	0	0	0	9	0	0	3	
17	06	1023.3	NE 6	÷ 14.6	..	÷14.8	87	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1024.1	NE 6	÷ 9.2	90	> 50	00	0	0	0	0	9	0	0	4	
	12	1024.1	NE 6	÷ 9.2	90	> 50	00 ¹	0	0	0	0	9	0	0	3	
	15	1023.4	NE 5	÷ 13.4	92	> 50	00	0	0	0	0	9	0	0	9	
	18	1022.9	E 6	÷ 13.7	÷ 9.0	..	94	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1022.5	NE 7	÷ 13.3	92	> 50	00	0	0	0	0	9	0	0	8	
18	00	1022.2	E 6	÷ 14.0	92	> 50	00	0	0	0	0	9	0	0	8	
	03	1022.8	E 6	÷ 14.5	95	> 50	00	0	0	0	0	9	0	0	4	
	06	1023.2	NE 5	÷ 14.7	..	÷15.0	95	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1025.2	NE 3	÷ 12.5	84	> 50	00	0	0	0	0	9	0	0	3	
	12	1025.2	NE 5	÷ 12.5	84	> 50	03	0	1	0	0	9	0	3	3	
	15	1025.0	NE 6	÷ 12.0	82	> 50	02	0	1	0	0	9	0	3	3	
19	18	1025.1	NE 6	÷ 11.9	÷11.8	..	81	> 50	02	0	1	0	0	9	0	3	3	0.0
	21	1025.6	E 6	÷ 12.2	82	> 50	00	0	0	0	0	9	0	0	4	
	00	1025.8	SE 7	÷ 12.9	82	> 50	00	0	0	0	0	9	0	0	3	
	03	1026.4	SE 6	÷ 13.0	82	> 50	00	0	0	0	0	9	0	0	4	
	06	1027.4	NE 9	÷ 13.8	..	÷15.0	84	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1028.9	E'N 9	÷ 12.5	83	> 50	00	0	0	0	0	9	0	0	4	
20	12	1029.3	E'N 5	÷ 12.0	83	> 50	00	0	0	0	0	9	0	0	3	
	15	1028.9	NE 7	÷ 13.3	84	> 50	03	0	4	0	0	9	0	3	9	
	18	1029.3	NE 6	÷ 11.7	÷11.5	..	83	> 50	02	0	4	0	0	9	0	3	3	0.0
	21	1030.8	E'S 8	÷ 12.6	84	> 50	00	0	0	0	0	9	0	0	4	
	00	1031.4	E'S 8	÷ 14.0	90	> 50	00	0	0	0	0	9	0	0	1	
	03	1031.5	E 3	÷ 14.1	84	> 50	00	0	0	0	0	9	0	0	1	
20	06	1031.6	E'N 5	÷ 15.5	..	÷15.5	100	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1031.7	E'N 5	÷ 15.0	94	> 50	00	0	0	0	0	9	0	0	3	
	12	1032.0	E'S 5	÷ 15.0	92	> 50	00	0	0	0	0	9	0	0	3	
	15	1031.7	E'S 6	÷ 14.5	92	> 50	00	0	0	0	0	9	0	0	9	
	18	1031.0	E'S 5	÷ 14.0	÷11.7	..	93	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1031.2	E 6	÷ 14.6	95	> 50	00	0	0	0	0	9	0	0	4	
20	00	1031.4	E 5	÷ 14.8	99	> 50	00	0	0	0	0	9	0	0	9	

¹ Mist on Independence Fjord.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1030.6	E'N 4	÷15.8	100	> 50	40	0	0	0	0	9	0	0	4	
	06	1029.9	E 3	÷14.5	..	÷16.1	100	> 50	40	0	0	0	0	9	0	0	9	0.0
	09	1029.8	E 2	÷12.5	90	> 50	00	0	0	0	0	9	0	0	8	
	12	1029.7	E'S 6	÷11.0	80	> 50	00	0	0	0	0	9	0	0	8	
	15	1029.6	E'S 5	÷11.5	82	> 50	00	0	0	0	0	9	0	0	8	
	18	1029.5	E'S 6	÷11.2	÷10.8	..	86	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1030.2	E'N 5	÷11.6	86	> 50	00	0	0	0	0	9	0	0	4	
21	00	1030.9	E 4	÷12.5	86	> 50	00	0	0	0	0	9	0	0	3	
	03	1031.9	E 4	÷11.9	84	> 50	00	0	0	0	0	9	0	0	3	
	06	1032.6	E'N 4	÷11.7	..	÷14.9	84	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1033.7	E'N 4	÷10.7	80	> 50	00	0	0	0	0	9	0	0	4	
	12	1034.6	E'N 6	÷10.6	83	> 50	00	0	0	0	0	9	0	0	3	
	15	1035.1	E'S 9	÷10.7	84	> 50	00	0	0	0	0	9	0	0	1	
	18	1035.5	E'S 10	÷10.2	÷10.0	..	85	> 50	03	0	1	0	0	9	0	3	3	0.0
	21	1036.3	E'N 6	÷10.5	85	> 50	03	0	1	0	0	9	0	3	3	
22	00	1037.0	E'N 6	÷11.0	88	> 50	03	0	1	1	6	4	0	3	3	
	03	1037.3	E'N 6	÷11.0	88	10—20	03	2	7	7	6	4	×	×	3	
	06	1037.6	E'N 6	÷11.2	..	÷11.7	88	10—20	03	2	8	8	6	4	×	×	3	0.0
	09	1037.9	E'N 5	÷11.1	87	20—50	02	2	8	8	6	4	×	×	3	
	12	1038.5	E'N 4	÷10.5	86	20—50	02	2	8	8	6	4	×	×	4	
	15	1038.2	E'S 4	÷10.0	84	> 50	01	0	1	1	6	4	0	3	9	
	18	1037.9	E'S 6	÷ 9.8	÷ 9.8	..	84	> 50	01	0	1	0	0	9	0	3	8	0.0
	21	1037.8	E'N 6	÷ 9.3	83	> 50	03	0	2	2	5	7	0	0	8	
23	00	1037.5	E'N 5	÷ 9.5	83	> 50	03	2	7	7	5	7	×	×	8	
	03	1037.0	ENE 5	÷ 9.4	83	20—50	03	2	8	8	5	7	×	×	8	
	06	1036.5	NE 4	÷ 9.3	..	÷11.2	84	20—50	02	2	8	8	5	7	×	×	8	0.0
	09	1036.7	ESE 3	÷ 9.0	80	20—50	02	2	8	8	5	4	×	×	4	
	12	1036.5	E 1	÷ 8.5	78	20—50	02	2	8	8	5	4	×	×	9	
	15	1026.4	E 2	÷ 7.8	76	20—50	02	2	8	8	5	5	×	×	8	
	18	1036.2	NE 3	÷ 6.5	÷ 6.2	..	72	> 50	01	0	1	1	5	5	0	0	8	0.0
	21	1036.0	NE 3	÷ 5.4	70	> 50	02	0	1	0	0	9	0	3	8	
24	00	1035.6	SE 3	÷ 5.2	70	> 50	03	2	7	0	5	7	0	2	8	
	03	1034.7	W 15	÷ 4.8	65	> 50	01	0	2	0	0	9	4	2	9	
	06	1033.5	W 16	÷ 5.3	..	÷ 9.5	63	> 50	03	2	7	0	0	9	7	×	8	0.0
	09	1032.8	W 16	÷ 5.4	66	> 50	02	2	7	0	0	9	7	×	6	
	12	1032.6	W 16	÷ 5.6	×	0.05—0.2	75	7	9	9	×	×	×	×	8	
	15	1031.4	W 16	÷ 4.3	×	0.05—0.2	75	7	9	9	×	×	×	×	9	
	18	1030.5	W 17	÷ 3.4	÷ 2.8	..	85	2—4	37	3	8	0	0	9	7	×	8	0.2
	21	1029.5	W 16	÷ 1.8	72	10—20	02	2	8	0	0	9	7	×	8	
25	00	1030.4	W 14	÷ 0.8	70	20—50	02	2	8	0	0	9	7	×	4	
	03	1032.9	E 5	÷ 3.8	70	> 50	02	2	8	0	0	9	7	×	4	
	06	1034.3	E 5	÷ 3.3	..	÷ 5.8	68	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1036.0	E'S 6	÷ 2.6	68	> 50	01	2	7	0	0	9	7	×	8	
	12	1037.2	SE 4	÷ 2.0	68	> 50	01	2	6	0	0	9	7	0	4	
	15	1037.9	SE 4	÷ 1.7	66	> 50	01	2	4	0	0	9	7	0	3	
	18	1038.1	SE 6	÷ 1.4	÷ 0.4	..	70	> 50	03	2	6	1	2	7	7	2	3	0.0
	21	1038.0	SE 6	÷ 2.2	76	> 50	03	2	7	1	6	5	7	0	9	
26	00	1038.3	SE 5	÷ 2.0	74	> 50	01	0	1	0	0	9	0	4	4	
	03	1039.9	SE 6	÷ 2.7	74	> 50	01	0	0	0	0	9	0	0	9	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1021.1	E'N 4	2.4	75	> 50	03	2	6	0	0	9	4	3	6	
	03	1020.9	0	2.8	65	> 50	01	0	2	0	0	9	4	3	6	
	06	1020.9	0	3.5	..	0.5	66	> 50	03	2	8	0	0	9	2	×	3	0.0
	09	1020.2	0	3.6	60	> 50	02	2	8	0	0	9	2	×	4	
	12	1021.2	W 5	7.2	53	> 50	01	2	7	0	0	9	7	×	3	
	15	1020.8	W'S 5	10.0	46	> 50	01	2	6	0	0	9	7	0	9	
	18	1021.5	E'S 9	3.9	11.4	..	72	> 50	01	0	2	0	0	9	7	0	4	0.0
	21	1021.7	E'S 10	3.6	73	> 50	02	0	2	0	0	9	7	0	3	
2	00	1021.9	E'N 5	2.6	77	> 50	01	0	1	0	0	9	7	0	3	
	03	1022.0	E'N 5	1.6	86	> 50	03	0	1	0	0	9	0	3	3	
	06	1021.8	0	1.5	..	1.2	85	> 50	02	0	1	0	0	9	0	3	9	0.0
	09	1021.4	0	2.0	76	> 50	00	0	0	0	0	9	0	0	8	
	12	1020.9	0	5.4	66	> 50	00	0	0	0	0	9	0	0	8	
	15	1020.4	E'S 5	3.8	79	> 50	00	0	0	0	0	9	0	0	8	
	18	1020.2	E'N 5	2.8	5.9	..	81	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1021.0	E'S 12	3.1	80	> 50	01	0	1	1	3	6	0	0	4	
3	00	1022.3	E'S 10	÷ 0.6	94	0.5-1	43	4	9	9	×	×	×	×	3	
	03	1023.4	E 8	÷ 2.2	97	10-20	03	2	8	8	6	2	×	×	3	
	06	1024.2	E 8	÷ 2.0	..	÷ 2.2	90	10-20	02	2	8	8	6	2	×	×	3	0.0
	09	1024.4	E 9	÷ 2.1	87	10-20	02	2	8	8	6	2	×	×	1	
	12	1024.6	E'S 10	÷ 2.5	90	10-20	02	2	8	8	6	2	×	×	3	
	15	1024.5	E'S 9	÷ 2.6	84	20-50	01	2	7	5	6	3	7	×	9	
	18	1024.3	E 8	÷ 3.6	3.1	..	82	20-50	01	2	5	2	6	4	7	0	8	0.0
	21	1024.1	E 9	÷ 4.0	85	20-50	03	2	8	8	6	4	×	×	8	
4	00	1023.9	E'S 9	÷ 4.0	86	20-50	02	2	8	8	6	4	×	×	8	
	03	1023.8	E 8	÷ 4.0	87	20-50	02	2	8	8	6	3	×	×	8	
	06	1023.7	E 8	÷ 3.6	..	÷ 4.0	86	20-50	02	2	8	8	6	3	×	×	8	0.0
	09	1023.7	E 7	÷ 3.0	86	20-50	02	2	8	8	6	3	×	×	3	
	12	1023.7	E 6	÷ 3.0	83	> 50	03	2	8	1	6	4	2	×	3	
	15	1023.3	E'S 6	÷ 2.6	82	20-50	02	2	8	1	6	4	2	×	9	
	18	1022.8	E'S 6	÷ 2.2	÷ 2.2	..	82	> 50	02	2	8	1	6	4	2	×	8	0.0
	21	1022.7	E'S 7	÷ 2.0	82	> 50	03	2	8	1	6	4	7	×	6	
5	00	1022.6	E'S 7	÷ 1.7	83	> 50	02	2	8	1	6	4	7	×	8	
	03	1022.4	E'S 4	÷ 1.3	86	> 50	02	2	8	3	6	4	7	×	8	
	06	1022.2	E 6	÷ 1.3	..	÷ 3.8	90	20-50	02	2	8	3	6	4	7	×	8	0.0
	09	1021.8	E 5	÷ 1.6	85	20-50	02	2	8	1	6	4	7	×	8	
	12	1021.5	E'N 6	÷ 1.4	84	20-50	02	2	8	1	6	4	7	×	8	
	15	1021.3	E 6	÷ 0.8	82	> 50	01	2	6	0	0	9	7	0	8	
	18	1021.1	E 8	÷ 0.7	÷ 0.4	..	82	> 50	01	2	4	1	6	4	4	0	8	0.0
	21	1021.1	E 7	÷ 1.1	84	20-50	01	2	1	1	6	4	0	0	3	
6	00	1021.9	E 7	÷ 0.3	80	> 50	02	0	1	1	6	4	0	0	4	
	03	1022.5	E 6	÷ 0.6	79	> 50	00	0	0	0	0	9	0	0	3	
	06	1022.5	E 5	÷ 1.3	..	÷ 2.1	80	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1023.2	E'N 5	÷ 0.7	82	> 50	00	0	0	0	0	9	0	0	4	
	12	1023.3	E 6	0.5	74	> 50	00	0	0	0	0	9	0	0	3	
	15	1022.5	E 6	0.9	70	> 50	00	0	0	0	0	9	0	0	9	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1021.9	E 8	1.5	1.8	..	68	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1021.9	E 8	1.5	66	> 50	00	0	0	0	0	9	0	0	3	
7	00	1021.8	E 7	0.3	74	> 50	00	0	0	0	0	9	0	0	8	
	03	1022.0	E 7	÷ 1.1	82	> 50	00	0	0	0	0	9	0	0	4	
	06	1022.2	E 6	0.0	..	÷ 1.5	80	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1022.4	E 5	0.5	75	> 50	00	0	0	0	0	9	0	0	3	
	12	1023.0	E 7	0.6	76	> 50	00	0	0	0	0	9	0	0	0	
	15	1022.5	E 7	1.0	70	> 50	00	0	0	0	0	9	0	0	8	
	18	1022.0	E 8	1.0	1.6	..	73	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1021.3	E'S 8	÷ 0.2	78	> 50	01	0	1	0	0	9	0	3	8	
8	00	1020.8	NE 7	÷ 0.3	85	> 50	01	0	0	0	0	9	0	0	9	
	03	1020.0	NE 7	÷ 0.3	82	> 50	00	0	0	0	0	9	0	0	8	
	06	1019.3	NE 7	0.2	..	÷ 0.7	80	> 50	00 ¹	0	0	0	0	9	0	0	8	0.0
	09	1018.9	E'S 5	0.3	78	> 50	03	2	8	0	0	9	0	7	3	
	12	1018.1	E'N 5	÷ 0.5	74	> 50	01	2	5	0	0	9	0	6	9	
	15	1017.2	E'N 5	0.0	84	> 50	01	0	1	0	0	9	0	6	8	
	18	1017.0	E'N 4	0.2	1.0	..	86	> 50	02	0	1	0	0	9	0	3	8	0.0
	21	1017.0	E'N 4	0.3	82	> 50	02	0	1	0	0	9	0	3	3	
9	00	1017.0	SE 6	0.3	84	> 50	02	0	1	0	0	9	0	3	3	
	03	1016.8	NE 4	÷ 0.3	80	> 50	03	0	3	0	0	9	5	0	9	
	06	1016.4	E 4	0.5	..	÷ 0.6	80	> 50	02	0	3	0	0	9	5	0	8	0.0
	09	1016.6	E 6	2.0	72	> 50	01	0	1	0	0	9	5	0	4	
	12	1016.6	E 6	3.0	69	> 50	02	0	1	0	0	9	5	0	3	
	15	1016.7	E 5	3.2	70	> 50	01	0	0	0	0	9	0	0	9	
	18	1016.7	E 7	2.5	3.5	..	70	> 50	03	0	2	0	0	9	7	0	3	0.0
	21	1016.8	E 5	2.7	70	> 50	03	2	6	0	0	9	7	0	3	
10	00	1016.8	E 5	3.0	73	> 50	02	2	6	0	0	9	7	0	3	
	03	1017.4	E 5	1.3	77	> 50	01	2	5	0	0	9	7	0	4	
	06	1017.6	NE 5	1.2	..	÷ 0.8	70	> 50	01	0	3	0	0	9	7	0	3	0.0
	09	1018.1	SE 6	1.2	78	> 50	01	0	1	0	0	9	7	0	3	
	12	1018.1	E 4	1.0	82	> 50	03	0	1	0	0	9	2	3	3	
	15	1018.5	E 6	1.0	88	> 50	02	0	1	0	0	9	2	3	9	
	18	1017.3	E 5	2.6	2.8	..	78	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1016.7	E 7	2.3	80	> 50	00	0	0	0	0	9	0	0	8	
11	00	1016.1	E 7	2.4	75	> 50	00	0	0	0	0	9	0	0	8	
	03	1015.7	E 7	2.7	74	> 50	03	0	1	0	0	9	0	0	8	
	06	1016.2	E 7	2.6	..	0.7	75	> 50	03	0	2	0	0	9	0	2	4	0.0
	09	1015.7	E 7	1.5	80	> 50	03	2	5	0	0	9	0	4	3	
	12	1015.4	E 6	2.0	82	> 50	02	2	5	0	0	9	0	4	9	
	15	1015.3	E 6	3.1	80	> 50	02	2	5	0	0	9	0	4	8	
	18	1014.9	E 7	3.7	5.7	..	72	> 50	02	2	5	0	0	9	0	4	8	0.0
	21	1014.7	E 7	3.1	75	> 50	03	2	6	0	0	9	0	4	8	
12	00	1013.3	E 10	1.8	83	> 50	02	2	6	0	0	9	0	4	4	
	03	1014.2	E 8	0.7	82	> 50	01	2	4	0	0	9	0	4	3	
	06	1015.7	E 6	0.0	..	÷ 0.6	84	> 50	02	2	4	0	0	9	0	4	3	0.0
	09	1017.6	SE 8	0.4	81	> 50	02	2	4	0	0	9	0	3	4	
	12	1017.8	E 9	0.5	81	> 50	40	2	4	0	0	9	0	6	3	
	15	1018.4	E 8	0.7	83	> 50	40	2	4	0	0	9	0	3	3	

¹ The clouds are drifting to E.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
13	18	1018.7	E 6	1.3	3.8	..	83	20—50	02	2	4	1	6	4	0	4	9	0.0
	21	1018.9	E 7	÷ 0.8	92	2—4	40	2	5	4	6	3	0	4	8	
	00	1018.9	E 6	÷ 1.3	98	2—4	40	2	8	8	6	3	×	×	3	
	03	1019.5	E 5	÷ 1.8	98	2—4	50	2	8	8	6	3	×	×	4	
	06	1020.2	E 6	÷ 1.5	..	÷ 2.0	96	10—20	02	2	8	8	6	3	×	×	3	trace
	09	1021.2	E 7	÷ 1.3	84	10—20	02	2	6	5	6	3	×	×	3	
14	12	1021.2	E 7	÷ 1.0	88	10—20	02	2	5	3	6	3	0	5	3	
	15	1021.0	E 7	÷ 0.8	82	20—50	01	0	3	2	6	3	0	5	9	
	18	1021.3	E 10	÷ 0.8	1.3	..	82	> 50	01 ¹	0	2	2	4	5	0	2	4	0.0
	21	1021.1	E 9	÷ 1.6	86	> 50	03	2	6	4	6	3	0	2	9	
	00	1021.2	E 8	÷ 1.9	87	> 50	02	2	6	6	4	4	0	2	3	
	03	1021.0	E 7	÷ 2.4	88	> 50	02	2	6	6	4	4	0	2	9	
15	06	1020.5	E 7	÷ 2.8	..	÷ 2.8	88	> 50	03	2	8	1	6	4	7	×	8	0.0
	09	1019.5	E 7	÷ 2.5	89	> 50	01	2	5	1	6	4	7	0	8	
	12	1018.5	E 8	÷ 1.5	96	> 50	02	2	5	1	6	4	7	0	9	
	15	1016.9	E 8	÷ 0.7	72	> 50	02	2	5	1	6	4	7	0	9	
	18	1015.4	E 6	÷ 1.0	÷ 0.6	..	84	> 50	02	2	5	1	6	4	7	0	8	0.0
	21	1014.5	E 7	÷ 0.6	80	> 50	03	0	2	1	6	4	0	4	6	
16	00	1014.0	E 5	÷ 0.5	83	> 50	01	0	1	1	6	4	0	0	8	
	03	1013.6	E 5	÷ 0.2	84	> 50	02	0	1	1	6	4	0	0	8	
	06	1013.2	E'N 6	0.4	..	÷ 2.8	84	> 50	02	0	1	1	6	4	0	0	8	0.0
	09	1013.6	E'N 6	0.1	83	> 50	02	0	1	1	2	6	0	0	4	
	12	1014.1	E'N 7	1.3	80	> 50	02	0	1	1	2	6	0	0	3	
	15	1015.1	E'N 6	1.4	76	> 50	02	0	1	1	2	6	0	0	4	
17	18	1015.7	E'N 6	1.5	1.6	..	81	> 50	02	0	1	1	2	7	0	0	3	0.0
	21	1017.7	E'S 5	1.5	73	> 50	03	0	2	2	2	7	0	0	4	
	00	1018.7	E'N 4	1.5	76	> 50	03	2	7	0	0	9	7	×	3	
	03	1019.7	E'S 6	1.8	72	> 50	02	2	7	0	0	9	7	×	3	
	06	1020.6	E'S 5	3.0	..	0.0	60	> 50	02	2	7	0	0	9	7	×	3	0.0
	09	1021.7	E'N 4	1.5	76	> 50	03	2	8	0	0	9	7	×	3	
18	12	1021.8	E'N 5	2.0	72	> 50	01	2	6	0	0	9	7	0	3	
	15	1021.7	E'N 5	3.2	71	> 50	01	0	2	0	0	9	6	0	9	
	18	1021.5	E 5	3.5	3.7	..	68	> 50	03	2	4	0	0	9	6	3	8	0.0
	21	1021.5	E'S 5	3.5	69	> 50	03	2	7	0	0	9	7	×	3	
	00	1021.5	E'S 7	3.0	68	> 50	01	2	6	0	0	9	7	0	3	
	03	1020.6	E'S 6	1.5	73	> 50	03	2	7	0	0	9	7	×	9	
18	06	1019.8	E'N 6	1.5	..	1.3	76	> 50	01	2	6	0	0	9	7	4	8	0.0
	09	1019.0	E'N 6	1.4	83	> 50	03	2	7	0	0	9	7	×	9	
	12	1018.2	E'N 6	1.4	79	> 50	01	2	6	0	0	9	7	0	6	
	15	1017.4	E'N 5	1.6	75	> 50	01	2	5	0	0	9	7	0	8	
	18	1016.5	E'N 5	2.5	3.5	..	72	> 50	02	2	5	0	0	9	7	0	4	0.0
	21	1016.9	E'N 5	2.8	79	> 50	03	2	7	0	0	9	7	0	3	
18	00	1016.9	E'N 5	1.8	74	> 50	03	2	8	0	0	9	7	×	3	
	03	1017.2	E 5	1.8	78	> 50	02	2	8	0	0	9	7	×	3	
	06	1017.5	E'S 5	1.5	..	3.0	78	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1017.8	E'S 7	1.3	78	> 50	01	2	5	0	0	9	7	0	3	
	12	1018.0	E'S 7	1.5	76	> 50	01	0	1	0	0	9	5	0	9	
15	1017.6	E 8	2.0	76	> 50	01	0	1	0	0	9	5	0	8		

¹ St. along "Buen".

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
19	18	1017.2	E 10	2.0	3.1	..	77	> 50	03	0	1	1	5	5	0	0	8	0.0
	21	1016.7	NE 5	0.5	91	20-50	03	2	8	8	6	1	×	×	3	
	00	1016.8	E'S 6	÷ 0.6	94	4-10	02	2	8	8	6	1	×	×	3	
	03	1016.6	E'S 6	÷ 1.0	99	4-10	22	2	8	8	6	0	×	×	3	
	06	1016.2	E'S 5	÷ 1.5	..	÷ 1.7	96	2-4	02	2	8	8	6	1	×	×	9	0.0
	09	1016.3	E'S 6	÷ 1.0	96	4-10	01	2	7	8	6	2	×	×	4	
	12	1016.6	E 6	÷ 0.6	95	4-10	02	2	8	8	6	2	×	×	3	
	15	1016.6	E 6	÷ 0.3	88	4-10	70	7	7	7	6	2	×	×	9	
	18	1016.2	E 9	0.0	2.0	..	86	2-4	03	2	8	8	6	2	×	×	4	0.0
20	21	1016.1	E'S 7	÷ 0.2	90	2-4	02	2	8	8	6	2	×	×	4	
	00	1016.3	E'S 9	÷ 0.5	90	4-10	02	2	8	8	6	2	×	×	9	
	03	1015.9	E'S 9	÷ 1.5	91	4-10	02	2	8	8	6	2	×	×	8	
	06	1015.1	E'S 9	÷ 1.5	..	÷ 1.7	91	4-10	02	2	8	8	6	3	×	×	8	0.0
	09	1014.4	E'S 8	÷ 1.2	98	4-10	02	2	8	8	6	3	×	×	8	
	12	1013.9	E'S 8	÷ 1.0	86	4-10	02	2	8	8	6	3	×	×	9	
	15	1012.2	E'S 8	÷ 0.6	86	4-10	02	2	8	8	6	3	×	×	8	
	18	1010.9	E'S 6	÷ 0.5	0.0	..	87	4-10	02	2	8	8	6	3	×	×	6	0.0
	21	1009.4	E'S 4	÷ 0.5	89	4-10	02	2	8	8	6	3	×	×	8	
21	00	1008.8	E'S 5	0.0	88	4-10	02	2	8	8	6	3	×	×	8	
	03	1008.0	0	0.0	84	4-10	02	2	8	8	6	4	×	×	8	
	06	1007.5	W'N 4	1.2	..	÷ 1.5	79	> 50	03	2	5	0	0	9	4	0	8	0.0
	09	1008.9	W 6	7.6	50	> 50	03	2	6	0	0	9	4	0	4	
	12	1008.9	E 1	8.3	48	> 50	01	0	1	0	0	9	4	0	0	
	15	1009.6	W 6	13.2	22	> 50	00	0	0	0	0	9	0	0	9	
	18	1006.6	W 6	13.6	13.8	..	24	> 50	03	0	1	0	0	9	4	0	8	0.0
	21	1006.0	W 6	13.4	28	> 50	03	0	2	0	0	9	4	2	8	
	00	1005.6	N 3	8.1	45	> 50	00	0	0	0	0	9	0	0	8	
22	03	1005.2	0	7.7	53	> 50	03	0	1	0	0	9	4	0	8	
	06	1005.6	W 9	12.2	..	1.2	38	> 50	03	0	4	0	0	9	4	0	4	0.0
	09	1007.3	W 12	8.9	48	> 50	02	2	4	0	0	9	4	0	3	
	12	1008.3	W 13	11.5	50	> 50	03	2	5	0	0	9	4	0	3	
	15	1009.9	W 13	9.2	54	> 50	03	2	7	0	0	9	7	0	3	
	18	1010.0	W 9	9.6	13.9	..	44	> 50	02	2	7	0	0	9	7	0	3	0.0
	21	1010.2	W 6	10.2	38	> 50	02	2	7	0	0	9	7	0	3	
	00	1010.8	E 4	4.6	72	> 50	01	0	3	0	0	9	7	0	3	
	03	1011.6	E 5	3.6	84	> 50	01	0	0	0	0	9	0	0	3	
23	06	1010.3	NE 4	4.0	..	3.4	86	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1009.9	NE 5	..	4.5	..	75	> 50	00	0	0	0	0	9	0	0	8	
	12	1009.0	E 7	4.0	76	> 50	01	0	1	0	0	9	0	0	6	
	15	1007.5	E 7	4.6	72	> 50	03	0	1	0	0	9	5	0	8	
	18	1005.8	E 8	4.5	10.1	..	72	> 50	02	0	1	0	0	9	5	0	8	0.0
	21	1005.5	NE 6	6.3	65	> 50	00	0	0	0	0	9	0	0	6	
	00	1005.5	0	5.0	70	> 50	01	0	1	0	0	9	0	3	3	
	03	1005.7	0	7.5	62	> 50	02	0	1	0	0	9	0	5	4	
	06	1006.9	0	6.0	..	3.7	58	> 50	02	0	1	0	0	9	0	5	4	0.0
24	09	1008.5	W 2	11.5	52	> 50	02	0	1	0	0	9	0	5	3	
	12	1009.9	W 8	16.0	38	> 50	02	0	1	0	0	9	0	4	3	
	15	1010.2	E 7	5.7	69	> 50	02	0	1	0	0	9	0	4	1	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
25	18	1010.8	E'N 8	7.0	16.5	..	72	> 50	02	0	1	0	0	9	0	4	3	0.0
	21	1011.2	E'N 6	8.7	65	> 50	02	0	1	0	0	9	0	4	3	
	00	1010.7	E'N 5	7.5	62	> 50	03	2	5	0	0	9	0	4	9	
	03	1008.9	E'S 5	8.2	60	> 50	01	2	4	0	0	9	0	4	9	
	06	1008.2	E'N 5	6.0	..	5.6	77	> 50	01	0	2	0	0	9	0	4	8	0.0
	09	1007.1	E'N 5	6.0	72	> 50	01	0	1	0	0	9	0	3	9	
	12	1006.8	E'N 6	6.0	74	> 50	02	0	1	0	0	9	0	3	8	
	15	1006.9	E'S 5	6.3	74	> 50	02	0	1	0	0	9	0	3	8	
	18	1007.2	E'S 6	6.6	7.6	..	78	> 50	03	0	2	0	0	9	0	4	4	0.0
26	21	1007.3	E'S 5	8.8	62	> 50	03	2	7	0	0	9	0	6	3	
	00	1007.6	E'S 2	8.3	62	> 50	02	2	7	0	0	9	0	6	3	
	03	1008.1	E'S 4	4.8	77	> 50	03	2	7	0	0	9	0	4	3	
	06	1008.8	E'N 3	4.0	..	4.0	81	> 50	03	2	7	0	0	9	5	0	3	0.0
	09	1010.1	E'N 2	8.1	67	> 50	01 ¹	2	4	0	0	9	5	0	4	
	12	1010.4	W 14	13.8	49	> 50	01	0	1	0	0	9	4	0	1	
	15	1012.2	W 10	7.0	63	> 50	02	0	1	0	0	9	4	0	4	
	18	1012.4	E'N 5	7.5	14.4	..	67	> 50	03	2	4	0	0	9	4	0	1	0.0
	21	1012.6	E'N 8	5.5	74	> 50	03	0	3	0	0	9	0	4	3	
27	00	1012.0	E'N 5	5.3	80	> 50	02	0	3	0	0	9	0	4	9	
	03	1010.9	E'N 5	5.0	81	> 50	01	0	1	0	0	9	0	4	9	
	06	1010.6	E'N 7	5.5	..	4.0	76	> 50	02	0	1	0	0	9	0	4	1	0.0
	09	1010.1	E'N 4	4.4	81	> 50	03	2	7	0	0	9	4	6	8	
	12	1009.8	E'N 5	5.0	77	> 50	03	2	8	0	0	9	7	×	8	
	15	1009.1	E'S 5	7.5	67	> 50	02	2	8	0	0	9	7	×	8	
	18	1008.8	E'S 5	4.5	7.6	..	76	> 50	02	2	8	0	0	9	2	×	8	0.0
	21	1010.1	W 14	9.5	63	> 50	01	2	5	1	2	6	4	0	4	
	00	1011.2	W 11	10.5	62	> 50	03	2	6	2	2	6	4	0	3	
28	03	1012.1	0	10.5	55	> 50	01	0	4	2	2	6	4	0	2	
	06	1013.2	E'S 8	7.0	..	4.2	72	> 50	03	0	3	1	4	6	0	5	2	0.0
	09	1014.3	E'S 8	6.3	71	> 50	03	2	5	0	0	9	4	3	2	
	12	1014.4	E'S 9	7.0	71	> 50	03	2	8	0	0	9	4	7	1	
	15	1013.3	E'S 7	6.9	71	> 50	03	2	8	2	6	7	2	×	9	
	18	1013.0	E'S 9	5.7	11.8	..	69	> 50	03	2	8	3	6	7	2	×	8	0.0
	21	1012.6	E'S 10	3.8	72	20-50	25	8	8	3	6	6	2	×	8	
	00	1012.0	E'S 5	3.0	81	20-50	80	8	8	4	6	4	2	×	8	
	03	1011.8	E 6	2.0	95	10-20	61	6	8	4	6	3	2	×	8	
29	06	1011.0	E 6	1.5	..	1.5	95	10-20	61	6	8	3	6	3	2	×	9	3.4
	09	1010.8	E 4	1.5	91	4-10	61	6	8	4	6	2	2	×	7	
	12	1010.6	0	1.5	91	4-10	61	6	8	4	6	2	2	×	7	
	15	1010.3	W 4	3.6	91	4-10	25	8	8	4	6	2	2	×	8	
	18	1010.7	W 12	3.6	5.8	..	80	10-20	80	8	8	4	6	5	2	×	4	3.2
	21	1012.3	W 11	3.5	72	10-20	02	2	8	4	6	5	2	×	4	
	00	1013.4	W 12	3.8	70	20-50	02	2	8	2	6	6	2	×	3	
	03	1015.0	W 12	3.2	68	20-50	02	2	8	2	6	6	2	×	3	
	06	1016.5	W 11	3.2	..	1.0	66	20-50	02	2	8	2	6	6	2	×	3	0.2
30	09	1018.8	W 10	3.3	68	20-50	02	2	8	3	6	6	2	×	4	
	12	1020.1	W 10	4.2	64	20-50	02	2	8	4	6	6	2	×	3	
	15	1021.1	W 9	5.3	62	20-50	02	2	8	3	6	6	2	×	3	

¹ 0915 Dust and sand drift at the head of Brønlands Fjord.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1021.2	W 7	6.5	6.7	..	57	> 50	01	2	7	1	6	6	5	×	1	0.0
	21	1022.0	W 8	3.0	74	> 50	01	2	4	1	6	4	5	0	3	
Mean		1016.2	6.2	2.5	5.2	0.4	76	6.8

July 1949

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1022.2	SE 8	3.0	78	20—50	03	2	6	2	6	4	5	0	1	
	03	1022.5	SE 7	1.5	81	20—50	03	2	6	4	6	4	5	0	3	
	06	1022.2	SE 9	1.6	..	1.3	80	20—50	02	2	6	4	6	4	5	0	9	0.0
	09	1021.5	SE 11	2.3	76	20—50	02	2	6	4	6	4	5	0	8	
	12	1020.2	E'S 8	3.5	73	20—50	02	2	6	3	6	4	5	0	8	
	15	1018.9	E'S 11	4.1	68	> 50	01	2	4	1	6	4	5	0	9	
	18	1018.2	E'S 12	4.3	6.5	..	73	> 50	03	2	6	1	6	4	5	0	8	0.0
	21	1018.0	E'S 4	2.0	85	> 50	01	2	5	4	6	4	5	0	8	
	2	00	1017.7	E'S 6	2.3	83	20—50	03	2	6	4	6	4	5	0	8
03		1017.2	E'S 7	1.8	88	20—50	03	2	8	5	6	4	5	0	8	
06		1017.1	E'S 4	1.6	..	1.2	88	20—50	02	2	8	5	6	4	5	0	8	0.0
09		1016.8	NE 5	3.2	84	> 50	02	2	8	1	6	5	7	0	8	
12		1016.7	E'N 6	2.6	84	> 50	02	2	8	1	6	5	7	0	8	
15		1016.6	E'N 6	3.3	82	> 50	02	2	8	1	6	5	7	0	8	
18		1015.7	E 5	4.3	4.5	..	78	> 50	01	2	6	0	0	9	7	0	8	0.0
21		1014.5	SE 4	4.5	78	> 50	01	2	4	0	0	9	7	3	8	
3		00	1014.0	NE 4	3.7	76	> 50	02	2	4	0	0	9	0	3	8
	03	1013.4	NE 4	4.3	76	> 50	02	2	4	0	0	9	0	3	6	
	06	1013.0	NE 6	4.2	..	1.6	76	> 50	02	2	2	0	0	9	0	3	8	0.0
	09	1012.6	E'S 6	5.0	74	> 50	03	2	4	1	6	4	5	0	8	
	12	1012.9	E'S 9	4.2	71	> 50	03	2	5	0	0	9	6	0	8	
	15	1011.4	E'S 8	3.4	74	> 50	03	2	6	3	6	4	7	0	8	
	18	1010.3	E'S 6	2.3	5.3	..	76	20—50	03	2	8	4	6	4	7	0	8	0.0
	21	1009.7	E'S 5	1.8	92	20—50	50	5	8	8	6	4	7	0	8	
	4	00	1008.8	ENE 5	1.6	96	20—50	50	5	8	7	6	4	7	0	8
03		1007.9	E 3	1.3	96	20—50	50	5	8	7	6	4	7	0	8	
06		1007.1	E 5	2.0	..	0.8	96	20—50	50	5	8	7	6	4	7	×	8	trace
09		1006.2	E 6	0.9	98	20—50	02	2	8	3	6	4	2	×	8	
12		1007.4	E'N 3	1.5	81	20—50	02	2	8	3	6	4	2	×	4	
15		1006.9	E 3	3.1	80	> 50	02	2	8	1	6	4	2	×	8	
18		1006.7	0	4.6	4.6	..	72	> 50	02	2	8	0	0	9	7	0	8	0.0
21		1006.3	W 4	7.8	64	> 50	01	2	5	0	0	9	7	0	8	
5		00	1006.1	W 7	8.2	58	> 50	02	2	5	0	0	9	7	0	8
	03	1006.3	W 9	7.7	60	20—50	03	2	6	0	0	9	7	0	4	
	06	1007.1	W 9	6.3	..	0.8	64	20—50	80	8	7	0	0	9	2	0	3	trace
	09	1007.9	NE 5	4.8	68	20—50	02	2	8	0	0	9	2	0	3	
	12	1008.9	NE 5	4.0	81	20—50	03	2	8	1	6	4	2	×	3	
	15	1009.1	NE 6	4.7	80	20—50	02	2	8	2	6	4	2	×	1	
	18	1008.9	NE 6	4.7	9.2	..	76	20—50	02	2	8	1	6	5	7	×	9	×

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
6	21	1008.5	E 6	5.1	70	20—50	01	2	7	0	0	9	7	0	8	
	00	1008.3	E 7	3.6	72	> 50	02	2	7	1	6	5	7	0	8	
	03	1007.7	E 6	3.5	74	> 50	02	2	7	2	6	4	7	0	8	
	06	1007.4	E 6	2.6	..	2.4	72	20—50	02	2	7	1	6	4	7	0	8	0.0
	09	1007.1	E 6	2.2	85	20—50	02	2	8	4	6	3	7	×	8	
	12	1007.3	E 6	2.0	87	20—50	01	2	7	4	6	3	7	×	4	
7	15	1006.7	E 6	3.6	82	> 50	01	2	5	1	6	4	7	0	9	
	18	1005.9	E 6	4.2	5.3	..	80	> 50	03	2	6	0	0	9	7	0	8	0.0
	21	1006.5	E 4	3.5	80	> 50	03	2	7	0	0	9	7	0	8	
	00	1006.5	E 3	3.1	80	> 50	03	2	7	0	0	9	7	0	3	
	03	1006.8	E 3	2.8	80	> 50	01	2	5	0	0	9	7	0	3	
	06	1007.1	E 4	3.6	..	1.8	78	> 50	01	0	2	0	0	9	7	0	3	0.0
8	09	1007.7	E 4	5.0	76	> 50	02	0	2	0	0	9	4	0	3	
	12	1007.3	E 4	6.0	61	> 50	01	0	1	0	0	9	4	0	9	
	15	1006.5	E 6	6.0	66	> 50	00	0	0	0	0	9	0	0	8	
	18	1005.6	E 9	6.2	9.0	..	63	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1005.0	E 8	6.2	67	> 50	00	0	0	0	0	9	0	0	8	
	00	1003.9	E 6	8.5	59	> 50	00	0	0	0	0	9	0	0	9	
9	03	1003.6	E 7	6.4	72	> 50	00	0	0	0	0	9	0	0	6	
	06	1003.3	E 6	4.5	..	3.6	76	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1002.6	E 6	3.5	78	> 50	00	0	0	0	0	9	0	0	8	
	12	1002.1	E 5	4.0	81	> 50	00	0	0	0	0	9	0	0	8	
	15	1001.9	E 3	4.8	72	> 50	03	0	3	0	0	9	0	5	8	
	18	1001.6	E 4	4.5	9.1	..	79	> 50	01	0	1	0	0	9	0	5	8	0.0
10	21	1001.8	E 3	6.8	58	> 50	03	0	3	0	0	9	0	5	4	
	00	1001.8	E 1	7.3	67	> 50	03	2	4	0	0	9	0	5	3	
	03	1002.1	W 6	15.2	49	> 50	11	0	3	0	0	9	0	5	3	
	06	1002.1	W 8	12.3	..	3.5	49	> 50	02	0	3	0	0	9	0	5	3	0.0
	09	1002.1	W 9	12.0	49	> 50	03	0	3	0	0	9	4	2	3	
	12	1002.1	W 13	14.5	49	> 50	02	0	3	0	0	9	4	2	3	
11	15	1002.1	W 12	15.0	48	> 50	03	2	6	0	0	9	4	6	3	
	18	1002.3	W 10	15.2	15.7	..	47	> 50	03	2	7	0	0	9	4	6	4	0.0
	21	1002.8	E 8	10.5	46	> 50	02	2	7	0	0	9	4	×	3	
	00	1003.7	E 8	6.5	49	> 50	03	2	8	0	0	9	4	6	4	
	03	1004.2	E 5	4.5	×	20—50	03	2	8	1	6	5	2	×	3	
	06	1004.6	E 5	2.5	..	2.0	98	10—20	61	6	8	4	6	4	2	×	3	0.3
11	09	1005.7	E'S 10	2.5	98	10—20	61	6	8	5	6	3	2	×	4	
	12	1007.1	E'S 6	2.0	96	20—50	02	2	8	6	6	3	2	×	4	
	15	1008.9	E'S 2	2.0	96	20—50	15	2	8	5	6	4	2	×	4	
	18	1009.9	0	2.5	15.3	..	92	> 50	01	2	7	7	5	7	2	×	3	1.0
	21	1012.1	E 5	3.5	90	> 50	02	2	7	5	5	7	4	0	4	
	00	1013.3	E'N 5	3.5	88	> 50	01	2	6	0	0	9	4	0	1	
11	03	1014.1	E'S 6	2.7	80	> 50	01	2	4	0	0	9	7	0	3	
	06	1015.0	E'S 5	2.5	..	1.4	80	> 50	01	0	1	0	0	9	7	3	3	0.0
	09	1015.3	E'N 6	3.5	74	> 50	02	0	1	0	0	9	0	3	1	
	12	1014.9	E 6	3.5	84	> 50	03	0	3	0	0	9	0	2	9	
	15	1014.5	E 6	3.8	84	> 50	00	0	0	0	0	9	0	0	8	
	18	1012.8	E 6	4.3	4.7	..	82	> 50	01	0	1	0	0	9	0	2	9	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
12	21	1012.2	E 7	5.1	70	> 50	02	0	1	0	0	9	4	0	8	0.0
	00	1011.6	E 6	4.4	80	> 50	03	2	5	0	0	9	4	2	8	
	03	1011.0	E 4	3.6	82	> 50	03	2	7	0	0	9	4	5	8	
	06	1009.3	E 3	5.1	..	2.5	76	> 50	02	2	7	0	0	9	4	6	9	
	09	1009.0	E 5	5.0	78	> 50	02	2	7	0	0	9	7	×	6	
	12	1008.4	E 3	6.8	62	> 50	03	2	8	0	0	9	2	×	8	
	15	1008.1	W 12	12.6	45	> 50	02	2	8	0	0	9	2	×	8	
	18	1008.5	W 12	10.1	13.2	..	58	> 50	01	2	5	0	0	9	4	0	4	
13	21	1011.4	W 7	8.9	68	> 50	03	2	7	0	0	9	7	×	4	0.0
	00	1012.3	W 11	9.5	63	> 50	02	2	7	0	0	9	7	×	1	
	03	1013.7	W 9	9.7	62	> 50	03	2	8	0	0	9	7	×	3	
	06	1014.7	W 10	8.0	..	5.0	63	> 50	01	2	5	0	0	9	7	0	3	
	09	1016.7	W 10	7.5	63	> 50	02	2	5	0	0	9	7	0	4	
	12	1017.2	W 12	8.0	61	> 50	03	2	7	0	0	9	7	×	3	
	15	1017.3	W 8	10.0	53	> 50	01	2	6	0	0	9	7	0	1	
	18	1016.1	W 13	10.0	10.3	..	53	> 50	01	2	5	0	0	9	4	4	9	
14	21	1015.4	W 15	9.5	51	> 50	02	2	5	0	0	9	4	4	7	0.0
	00	1015.5	W 9	9.0	51	> 50	03	2	7	0	0	9	4	4	2	
	03	1016.0	W 12	10.2	50	> 50	03	2	8	0	0	9	4	9	2	
	06	1016.6	W 12	10.2	..	7.1	50	> 50	01	2	6	0	0	9	4	9	3	
	09	1017.9	W 14	9.5	51	> 50	02	2	6	0	0	9	4	3	4	
	12	1017.8	W 20	10.6	51	> 50	01 ¹	2	5	0	0	9	4	0	9	
	15	1018.8	W 19	11.0	51	> 50	02 ¹	2	5	0	0	9	4	0	4	
	18	1019.6	W 16	9.6	11.4	..	53	> 50	03 ¹	2	8	0	0	9	7	×	3	
15	21	1021.7	W 12	8.5	59	> 50	03	2	8	1	6	5	2	×	4	0.0
	00	1022.1	W 15	10.5	53	> 50	03	2	8	1	6	5	4	2	1	
	03	1022.5	W 10	8.5	54	> 50	02	2	8	0	0	9	4	2	3	
	06	1021.8	W 10	7.8	..	7.5	62	> 50	01	2	7	0	0	9	4	2	9	
	09	1021.4	W 13	12.5	54	> 50	01	2	5	0	0	9	4	2	8	
	12	1020.2	W 16	13.5	50	> 50	03	2	6	1	1	7	5	2	9	
	15	1020.0	W 14	14.8	45	> 50	01	2	5	0	0	9	4	2	6	
	18	1019.3	W 14	15.5	15.9	..	43	> 50	01	2	4	0	0	9	4	2	9	
16	21	1019.0	W 11	16.0	42	> 50	01	0	2	0	0	9	4	2	8	0.0
	00	1018.9	W 14	15.3	39	> 50	03	0	4	0	0	9	4	2	8	
	03	1018.8	W 13	13.4	52	> 50	03	2	6	0	0	9	4	2	8	
	06	1018.4	W 10	14.6	..	7.8	58	> 50	03	2	7	0	0	9	4	0	9	
	09	1018.3	W 10	11.8	61	> 50	03	2	8	0	0	9	4	×	3	
	12	1018.3	W 10	11.0	63	> 50	15	2	8	0	0	9	7	×	3	
	15	1018.3	W 10	13.4	66	> 50	02	2	8	0	0	9	7	×	3	
	18	1015.9	W 10	12.5	16.4	..	62	> 50	02	2	8	0	0	9	7	×	9	
17	21	1015.2	W 10	14.3	52	> 50	01	2	7	0	0	9	4	2	8	0.0
	00	1014.8	W 9	12.8	58	> 50	02	2	7	0	0	9	4	2	8	
	03	1013.9	W 10	12.0	60	> 50	03	2	8	0	0	9	4	×	9	
	06	1013.9	W 13	9.3	..	9.3	75	> 50	02	2	8	0	0	9	4	×	3	
	09	1015.8	W 17	8.4	69	> 50	03	2	8	0	0	9	4	×	4	
	12	1017.5	W 15	6.6	71	> 50	03	2	8	1	4	7	4	6	2	
	15	1017.4	W 19 ²	7.6	60	> 50	02	2	8	1	4	7	4	×	9	
	18	1017.9	W 17	8.5	14.8	..	58	> 50	01	2	7	0	0	9	4	2	4	

Sand drift. ² In the gusts 24 m/sec., sand drift.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
18	21	1016.1	W 17	6.5	65	> 50	03	2	7	0	0	9	4	×	9	0.0	
	00	1014.4	W 10	6.5	69	> 50	03	2	8	0	0	9	4	×	8		
	03	1012.4	W 12	7.0	67	> 50	02	2	8	0	0	9	4	×	8		
	06	1010.6	W 12	6.0	..	6.0	72	> 50	02	2	8	0	0	9	4	×	8		
	09	1010.3	W 13	6.3	70	> 50	02	2	8	0	0	9	4	×	6		
	12	1009.0	W 14	5.8	64	> 50	02	2	8	0	0	9	4	×	7		
	15	1006.5	W 16	4.8	72	> 50	02	2	8	0	0	9	4	×	7		
19	18	1002.4	W 29	4.8	72	20-50	02	2	8	0	0	9	4	×	8	0.0	
	21	1005.9	W 21	6.3	65	20-50	09	2	7	0	0	9	4	9	4		
	00	1008.6	W 21	6.0	60	20-50	09	2	7	0	0	9	4	9	2		
	03	1010.8	W 15	5.0	65	> 50	03	2	8	0	0	9	7	×	3		
	06	1010.8	W 11	4.9	..	4.7	61	20-50	03	2	8	2	6	5	7	×	3		0.0
	09	1011.4	W 11	3.1	86	10-20	60	6	8	8	6	4	×	×	3		
	12	1012.3	W 8	1.5	100	4-10	68	7	8	8	6	1	×	×	2		
20	15	1012.7	W 8	3.5	67	20-50	02	2	8	8	6	3	×	×	9	0.3	
	18	1012.9	W 10	2.5	6.5	..	83	10-20	83	7	8	8	6	2	×	×	4		
	21	1014.0	W 7	2.8	87	10-20	02	2	8	8	6	2	×	×	2		
	00	1014.6	W 6	2.5	85	10-20	83	7	8	8	6	2	×	×	1		
	03	1014.9	W 4	2.5	83	10-20	02	2	8	8	6	2	×	×	3		
	06	1015.1	W 2	2.6	..	1.3	81	10-20	02	2	8	8	6	2	×	×	3		0.6
	09	1015.3	W 10	3.5	78	20-50	02	2	8	8	6	4	×	×	3		
21	12	1015.2	W 6	4.0	74	20-50	03	2	8	3	6	5	7	×	9	0.0	
	15	1014.6	W 4	4.5	65	> 50	01	2	7	2	6	5	7	2	8		
	18	1014.2	E'S 3	4.8	4.8	..	64	> 50	01	2	6	0	0	9	7	0	8		
	21	1013.8	E 2	4.8	68	> 50	01	2	4	2	4	7	4	0	8		
	00	1013.0	E'S 7	2.4	73	> 50	00	0	0	0	0	9	0	0	8		
	03	1011.4	E 6	2.5	73	> 50	03	0	1	0	0	9	5	0	8		
	06	1010.9	E 6	2.5	..	2.3	74	> 50	03	2	6	0	0	9	5	2	8		0.0
09	1010.5	E 7	4.3	71	> 50	01	0	2	0	0	9	5	0	8			
12	1010.6	E'S 8	2.3	71	> 50	01	0	1	0	0	9	4	0	4			
22	15	1011.3	E 7	5.6	5.8	..	68	> 50	01	0	1	0	0	9	4	0	3	0.0	
	18	1011.6	E'S 10	5.5	66	> 50	00	0	0	0	0	9	0	0	3		
	21	1013.0	E'S 8	5.6	60	> 50	00	0	0	0	0	9	0	0	3		
	00	1012.4	E'S 8	5.5	60	> 50	00	0	0	0	0	9	0	0	3		
	03	1012.8	E'S 4	5.0	60	> 50	00	0	0	0	0	9	0	0	3		
	06	1013.4	E 6	4.8	..	2.3	61	> 50	00	0	0	0	0	9	0	0	3		
	09	1013.8	E'N 5	3.5	69	> 50	00	0	0	0	0	9	0	0	3		
23	12	1014.2	E'N 7	2.5	76	> 50	00	0	0	0	0	9	0	0	3	0.0	
	15	1014.2	E 4	4.4	78	> 50	00	0	0	0	0	9	0	0	3		
	18	1014.2	E 6	4.5	5.7	..	79	> 50	00	0	0	0	0	9	0	0	3		
	21	1014.7	E 5	4.0	70	> 50	00	0	0	0	0	9	0	0	4		
	00	1015.2	E 6	3.2	64	> 50	00	0	0	0	0	9	0	0	3		
	03	1016.0	E 5	4.1	64	> 50	00	0	0	0	0	9	0	0	3		
	06	1016.8	E 5	4.3	..	3.0	60	> 50	00	0	0	0	0	9	0	0	3		0.0
09	1017.6	E 4	3.3	60	> 50	00	0	0	0	0	9	0	0	3			
12	1017.6	E'S 6	6.0	54	> 50	03	0	1	0	0	9	0	2	8			
23	15	1017.9	E'N 6	5.2	63	> 50	00	0	0	0	0	9	0	0	3	0.0	
	18	1017.5	E'N 8	4.8	6.2	..	73	> 50	00	0	0	0	0	9	0	0	9		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	21	1017.0	E'N 6	6.4	70	> 50	00	0	0	0	0	9	0	0	8	
24	00	1016.5	E'S 10	6.5	63	> 50	00	0	0	0	0	9	0	0	8	
	03	1016.7	E'S 6	4.5	66	> 50	00	0	0	0	0	9	0	0	4	
	06	1017.0	E'S 8	3.5	..	3.2	73	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1017.0	E'N 5	4.5	75	> 50	00	0	0	0	0	9	0	0	3	
	12	1016.7	E 5	4.0	75	> 50	01	0	1	0	0	9	0	5	9	
	15	1016.4	E 6	5.4	66	> 50	03	0	2	0	0	9	0	2	8	
	18	1016.4	E 6	5.6	7.8	..	67	> 50	02	0	2	0	0	9	0	2	3	0.0
	21	1016.2	E'N 5	5.4	67	> 50	03	0	3	0	0	9	0	2	9	
25	00	1016.1	E 4	6.1	66	> 50	01	0	2	0	0	9	0	4	8	
	03	1016.1	E'S 2	5.4	65	> 50	01	0	1	0	0	9	0	4	3	
	06	1016.1	E 1	7.9	..	3.4	59	> 50	02	0	1	0	0	9	0	4	3	0.0
	09	1016.0	E'S 2	8.6	58	> 50	02	0	1	0	0	9	0	4	9	
	12	1015.6	E'S 4	9.5	56	> 50	00	0	0	0	0	9	0	0	8	
	15	1014.6	E 7	7.6	63	> 50	00	0	0	0	0	9	0	0	9	
	18	1014.0	E'S 10	9.0	10.0	..	50	> 50	03	0	1	0	0	9	0	4	8	0.0
	21	1013.1	E'S 7	8.5	62	> 50	03	0	2	0	0	9	0	4	8	
26	00	1012.7	E'N 5	7.5	66	> 50	03	0	3	0	0	9	0	4	8	
	03	1012.5	E'N 4	5.6	69	> 50	01	0	1	0	0	9	0	4	8	
	06	1012.5	E'N 4	5.3	..	5.1	72	> 50	02	0	1	0	0	9	0	4	3	0.0
	09	1012.6	NE 1	9.3	60	> 50	02	0	1	0	0	9	0	4	4	
	12	1012.4	SE 4	9.6	60	> 50	02	0	1	0	0	9	0	4	9	
	15	1011.6	E'S 4	10.5	54	> 50	00	0	0	0	0	9	0	0	9	
	18	1011.7	E 6	8.5	11.6	..	66	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1012.2	E'S 8	7.5	63	> 50	00	0	0	0	0	9	0	0	3	
27	00	1012.6	NE 7	6.5	66	> 50	00	0	0	0	0	9	0	0	3	
	03	1013.0	E 6	5.4	71	> 50	00	0	0	0	0	9	0	0	3	
	06	1013.3	E 6	3.8	..	3.8	77	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1013.0	E 4	4.2	77	> 50	00	0	0	0	0	9	0	0	9	
	12	1012.8	ESE 5	5.0	72	> 50	00	0	0	0	0	9	0	0	8	
	15	1012.5	ESE 5	5.0	73	> 50	00	0	0	0	0	9	0	0	8	
	18	1012.0	ESE 6	4.8	8.6	..	75	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1011.5	ENE 6	4.7	74	> 50	00	0	0	0	0	9	0	0	8	
28	00	1012.0	ENE 7	4.6	72	> 50	00	0	0	0	0	9	0	0	4	
	03	1012.5	E'N 6	3.6	71	> 50	00	0	0	0	0	9	0	0	3	
	06	1012.9	E'N 7	4.0	..	3.4	71	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1013.4	E'N 5	3.2	76	> 50	00	0	0	0	0	9	0	0	3	
	12	1013.4	E'N 5	4.3	77	> 50	00	0	0	0	0	9	0	0	1	
	15	1013.7	E'N 6	3.6	66	> 50	00	0	0	0	0	9	0	0	3	
	18	1012.5	E'N 5	3.9	5.0	..	76	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1012.4	E'N 5	4.9	74	> 50	00	0	0	0	0	9	0	0	8	
29	00	1012.3	E 4	4.9	74	> 50	00	0	0	0	0	9	0	0	8	
	03	1012.3	E 4	5.2	74	> 50	00	0	0	0	0	9	0	0	8	
	06	1012.5	E 4	5.4	..	3.0	76	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1011.8	0	8.1	64	> 50	00	0	0	0	0	9	0	0	9	
	12	1011.3	E'N 2	11.0	60	> 50	00	0	0	0	0	9	0	0	8	
	15	1009.8	SE 4	10.4	59	> 50	00	0	0	0	0	9	0	0	9	
	18	1009.0	SE 5	7.7	12.1	..	60	> 50	00	0	0	0	0	9	0	0	8	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
30	21	1008.7	SE 6	8.1	62	> 50	00	0	0	0	0	9	0	0	8	0.0
	00	1009.7	E 5	8.3	64	> 50	00	0	0	0	0	9	0	0	4	
	03	1009.9	E 5	6.7	64	> 50	03	0	1	0	0	9	0	1	3	
	06	1010.5	E 3	7.0	..	4.9	70	> 50	02	0	1	0	0	9	0	2	3	
	09	1011.2	NE 3	7.6	70	> 50	02	0	1	0	0	9	0	2	3	
	12	1011.2	SE 4	8.5	67	> 50	02	0	1	0	0	9	0	2	1	
31	15	1011.2	E 6	6.6	69	> 50	00	0	0	0	0	9	0	0	3	0.0
	18	1011.0	NE 6	8.6	9.5	..	62	> 50	00	0	0	0	0	9	0	0	9	
	21	1010.8	E 7	11.6	62	> 50	00	0	0	0	0	9	0	0	8	
	00	1011.0	E 5	10.0	67	> 50	03	0	1	0	0	9	4	0	4	
	03	1011.0	E 5	8.9	68	> 50	03	0	3	0	0	9	4	0	3	
	06	1011.0	E 5	9.1	..	6.9	69	> 50	02	0	3	0	0	9	4	1	3	
Mean	09	1011.3	ENE 4	9.2	69	> 50	03	0	4	0	0	9	4	1	4	0.1
	12	1011.4	ENE 7	8.6	69	> 50	60	6	4	0	0	9	4	1	3	
	15	1011.7	ENE 6	8.1	72	> 50	02	2	4	0	0	9	4	1	3	
	18	1011.8	E S 8	7.0	11.9	..	72	> 50	25	2	5	0	0	9	7	0	3	
	21	1012.2	SE 7	6.6	72	> 50	60	6	5	0	0	9	7	0	3	
	Mean	1012.3	7.4	6.0	9.0	3.7	61	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1012.8	NE 6	5.6	76	> 50	01	2	4	0	0	9	7	0	3	0.0
	03	1014.0	NE 4	3.7	80	> 50	01	0	3	0	0	9	7	0	4	
	06	1014.7	NE 3	4.1	..	3.1	84	> 50	02	0	3	0	0	9	7	0	3	
	09	1015.2	E 4	4.2	79	> 50	01	0	2	0	0	9	7	0	3	
	12	1015.8	E'S 2	6.0	72	> 50	01	0	1	0	0	9	5	2	3	
	15	1015.8	E'S 8	3.7	77	> 50	02	0	1	1	2	8	4	2	3	
2	18	1016.8	E'S 7	7.5	8.0	..	77	> 50	03	0	2	1	2	8	4	2	4	0.0
	21	1017.0	E'S 5	8.6	74	> 50	02	0	2	1	2	8	4	2	3	
	00	1017.3	E'S 7	7.7	66	> 50	02	0	2	1	2	8	4	2	3	
	03	1017.5	ENE 4	6.4	69	> 50	01	0	1	0	0	9	0	2	3	
	06	1017.5	ENE 4	6.8	..	5.8	72	> 50	01	0	0	0	0	9	0	0	3	
	09	1017.5	ESE 3	6.5	71	> 50	01	0	1	0	0	9	0	1	3	
3	12	1016.8	E'N 4	..	5.8	..	74	> 50	00	0	0	0	0	9	0	0	9	0.0
	15	1015.9	E'N 6	5.8	76	> 50	00	0	0	0	0	9	0	0	8	
	18	1015.5	E'S 7	6.0	8.8	..	77	> 50	03	0	1	0	0	9	4	2	8	
	21	1015.7	SE 6	6.2	69	> 50	02	0	4	0	0	9	4	5	4	
	00	1015.9	SE 5	6.6	69	> 50	03	1	4	0	0	9	4	5	4	
	03	1016.1	E'N 5	4.4	67	> 50	03	2	6	0	0	9	4	6	3	
Mean	06	1016.0	E'N 5	4.3	..	4.3	68	> 50	03	2	7	0	0	9	4	6	9	0.0
	09	1015.7	NE'E 4	5.5	65	> 50	03	2	7	0	0	9	4	6	4	
	12	1015.9	E'N 6	4.5	66	> 50	02	2	7	0	0	9	4	7	8	
	15	1016.8	SE 7	5.8	65	> 50	01	2	6	0	0	9	4	8	4	
	18	1017.1	E'S 7	5.2	5.8	..	67	> 50	01	2	5	0	0	9	4	8	1	
	21	1018.2	SE'E 8	4.2	70	> 50	01	1	4	0	0	9	4	1	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
4	00	1018.7	SE 5	3.5	73	> 50	03	1	7	0	0	9	5	0	1	
	03	1018.6	0	4.0	76	> 50	60	6	8	8	0	7	9	×	0	
	06	1018.1	W 6	6.6	..	3.1	72	20—50	63	6	8	8	0	6	9	×	6	×
	09	1017.9	W 9	7.2	77	10—20	50	6	8	8	0	6	9	×	6	
	12	1017.7	W 8	7.5	77	10—20	63	6	8	8	0	6	9	×	8	
	15	1017.6	W 10	8.3	76	10—20	21	2	8	8	0	6	9	×	6	
5	18	1017.2	W 10	8.5	9.0	..	74	10—20	50	6	8	8	0	6	9	×	9	×
	21	1017.3	W 10	8.8	74	10—20	51	6	8	8	0	6	2	×	6	
	00	1016.9	W 9	9.0	73	10—20	60	6	8	8	0	6	2	×	9	
	03	1016.8	W 8	9.0	74	10—20	21	6	8	8	0	6	2	×	6	
	06	1016.5	W 7	9.0	..	5.8	74	10—20	60	6	8	8	0	6	2	×	9	×
	09	1017.0	SE'E 4	7.7	76	20—50	01	6	8	8	0	8	4	×	5	
	12	1017.1	E 3	6.8	85	> 50	01	1	8	0	0	9	4	×	1	
	15	1016.8	SE'E 4	6.5	84	> 50	01	2	7	0	0	9	4	2	9	
	18	1016.4	SE 3	8.5	9.1	..	79	> 50	01	2	7	0	0	9	4	2	8	×
6	21	1016.4	SE 4	6.5	75	> 50	02	2	7	0	0	9	5	×	3	
	00	1016.4	ENE 3	6.0	75	> 50	01	1	6	0	0	9	5	1	3	
	03	1016.2	ENE 2	5.6	84	> 50	01	1	4	0	0	9	5	1	9	
	06	1015.6	WSW 8	9.0	..	4.3	48	> 50	01	1	3	0	0	9	4	2	9	0.0
	09	1015.4	WSW 6	10.8	45	> 50	01	0	7	0	0	9	4	1	6	
	12	1015.6	WSW 11	12.4	41	> 50	03	1	7	0	0	9	4	6	4	
	15	1015.7	WNW 9	11.8	40	> 50	03	1	8	0	0	9	4	7	3	
	18	1016.2	W 10	10.4	12.5	..	45	> 50	03	1	8	0	0	4	4	7	4	0.0
	21	1016.8	NW'W 8	8.0	56	10—20	60	6	8	8	0	7	2	×	3	
7	00	1017.6	W'S 7	7.5	70	10—20	02	6	8	3	6	5	2	×	3	
	03	1018.3	E 5	3.4	78	20—50	01	2	7	0	0	9	4	0	3	
	06	1018.5	E 5	2.2	..	2.2	82	20—50	03	2	8	1	6	4	4	×	1	trace
	09	1018.4	E 4	2.8	85	> 50	02	2	8	1	6	4	4	×	4	
	12	1017.8	WNW 10	7.0	85	4—10	62	6	8	8	6	5	×	×	9	
	15	1017.1	W 13	8.3	72	10—20	61	6	8	1	6	4	×	×	8	
	18	1016.3	W 13	10.5	12.8	..	65	20—50	02	6	8	8	0	8	7	×	8	×
	21	1016.3	WSW 7	10.0	60	> 50	01	1	8	0	0	9	4	×	3	
	00	1017.3	W 7	9.9	60	> 50	01	1	8	0	0	9	4	×	4	
8	03	1017.6	W 7	4.0	61	> 50	02	2	8	0	0	9	4	×	3	
	06	1017.7	E 4	4.3	..	1.6	62	> 50	01	1	5	0	0	9	4	0	3	0.0
	09	1017.5	SE'E 3	5.0	62	> 50	02	2	5	0	0	9	4	2	9	
	12	1017.2	SE 2	4.5	79	> 50	03	2	8	0	0	9	2	×	9	
	15	1016.0	E 3	6.0	77	> 50	03	2	8	0	0	9	2	×	8	
	18	1015.3	WNW 3	11.4	11.7	..	66	> 50	01	1	7	0	0	9	4	8	8	0.0
	21	1014.9	E 2	8.2	57	> 50	03	2	7	0	0	9	7	×	6	
	00	1014.6	0	8.2	63	> 50	01	1	4	0	0	9	4	1	8	
	03	1014.5	E 1	4.0	65	> 50	01	1	1	0	0	9	0	2	8	
9	06	1013.0	0	4.5	..	3.5	70	> 50	01	0	6	0	0	9	0	2	9	0.0
	09	1012.8	W 6	11.7	45	> 50	02	0	6	0	0	9	0	2	7	
	12	1013.2	W 8	12.6	39	> 50	02	0	6	0	0	9	0	2	4	
	15	1013.2	W 8	13.2	44	> 50	02	2	6	0	0	9	4	2	3	
	18	1013.5	W 8	14.0	16.0	..	41	> 50	02	2	5	0	0	9	4	2	4	0.0
	21	1014.8	W 9	13.0	45	> 50	03	2	7	0	0	9	4	2	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
10	00	1016.8	W 6	12.9	44	> 50	03	2	7	0	0	9	4	2	3	
	03	1017.6	E 3	16.7	52	> 50	03	2	7	0	0	9	4	2	4	
	06	1017.9	NE'E 3	7.1	..	4.5	60	20—50	03	2	7	0	0	9	4	2	3	0.0
	09	1018.7	NE'E 5	5.4	70	> 50	03	2	7	0	0	9	4	×	4	
	12	1019.9	SE 6	4.9	78	> 50	02	2	8	6	0	8	7	×	4	
	15	1020.3	SE'E 5	4.4	82	20—50	02	2	8	8	0	8	7	×	1	
	18	1020.8	SE'E 6	5.2	17.1	..	81	> 50	02	2	7	7	0	8	7	×	3	0.0
	21	1020.7	SE 6	3.8	82	20—50	02	2	7	7	0	7	7	×	1	
11	00	1020.6	E 6	2.9	92	> 50	02	2	7	0	0	9	7	×	9	
	03	1020.6	E 5	2.1	90	> 50	03	2	8	0	0	9	7	×	3	
	06	1020.8	0	2.5	..	1.0	94	> 50	02	2	8	0	0	9	7	×	4	0.0
	09	1019.0	0	4.8	84	> 50	01	1	5	0	0	9	3	×	9	
	12	1018.2	SE'E 4	5.0	82	> 50	01	1	3	0	0	9	3	0	6	
	15	1017.1	SE'E 6	4.3	80	> 50	01	0	2	0	0	9	3	0	9	
	18	1016.1	SE'E 5	3.3	5.3	..	82	> 50	01	0	1	0	0	9	3	0	8	0.0
	21	1015.1	E 5	4.1	83	> 50	01	0	1	0	0	9	0	1	8	
12	00	1014.4	SE'E 4	4.1	84	> 50	01	0	1	1	1	4	0	9	8	
	03	1014.2	0	2.0	88	> 50	01	0	1	0	0	9	4	1	6	
	06	1013.9	0	4.7	..	1.0	90	> 50	01	0	1	0	0	9	4	1	8	0.0
	09	1013.5	E 3	5.3	82	> 50	03	0	3	0	0	9	4	1	8	
	12	1012.9	E 2	7.0	60	> 50	02	0	3	0	0	9	0	9	8	
	15	1012.9	SE'E 4	7.4	56	> 50	03	2	6	0	0	9	3	1	3	
	18	1012.4	SE 4	6.2	8.0	..	62	> 50	03	2	8	0	0	9	4	×	9	0.0
	21	1012.2	SE'E 5	5.2	59	> 50	01	2	6	0	0	9	3	0	6	
13	00	1012.8	NE'E 5	4.9	64	> 50	02	2	6	0	0	9	4	0	4	
	03	1013.3	SE'E 4	4.5	66	> 50	01	2	4	0	0	9	3	0	3	
	06	1013.5	SE'E 4	5.5	..	3.2	66	> 50	01	1	1	0	0	9	4	1	3	0.0
	09	1013.8	E 5	5.0	67	> 50	00	1	0	0	0	9	0	0	3	
	12	1014.3	NE'E 7	4.8	72	> 50	00	0	0	0	0	9	0	0	3	
	15	1014.2	SE'E 8	5.5	76	> 50	00	0	0	0	0	9	0	0	1	
	18	1013.8	SE'E 7	4.2	6.3	..	77	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1013.6	E 7	4.0	79	> 50	00	0	0	0	0	9	0	0	8	
14	00	1013.5	NE'E 7	4.2	79	> 50	00	0	0	0	0	9	0	0	8	
	03	1013.4	NE'E 4	2.4	82	> 50	00	0	0	0	0	9	0	0	8	
	06	1013.6	E 6	2.1	..	1.1	82	> 50	03	0	1	0	0	9	0	1	4	0.0
	09	1013.4	0	5.2	72	> 50	03	0	3	0	0	9	0	4	9	
	12	1013.4	0	6.0	68	> 50	02	0	3	0	0	9	0	4	3	
	15	1013.1	E 4	6.9	60	> 50	02	0	3	0	0	9	0	4	9	
	18	1013.2	E 2	8.2	8.5	..	50	> 50	03	1	6	0	0	9	3	4	6	0.0
	21	1013.5	W 10	10.8	29	> 50	01	1	3	0	0	9	3	0	4	
15	00	1014.7	W 10	9.0	35	> 50	01	2	7	0	0	9	4	2	4	
	03	1015.7	W 7	8.0	42	> 50	03	2	7	0	0	9	5	0	3	
	06	1016.4	E'N 10	3.5	..	1.0	50	> 50	02	2	7	0	0	9	4	2	3	0.0
	09	1016.9	NE'E 5	3.4	85	> 50	02	2	8	0	0	9	4	2	1	
	12	1016.7	W 7	9.0	42	> 50	03	2	8	0	0	9	4	×	9	
	15	1016.4	W 8	10.3	44	> 50	03	2	8	0	0	9	4	2	9	
	18	1016.0	W 10	10.4	11.2	..	45	> 50	02	2	8	0	0	9	4	×	8	0.0
	21	1015.6	WSW 9	10.3	43	> 50	02	2	8	0	0	9	4	×	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
16	00	1015.8	WSW 6	8.5	56	> 50	01	2	7	0	0	9	4	4	4	
	03	1015.7	WSW 9	8.5	61	> 50	02	2	8	0	0	9	7	×	9	
	06	1015.6	WSW 7	7.2	..	2.7	72	20-50	60	6	8	0	0	9	2	×	8	trace
	09	1015.2	WSW 8	7.6	68	> 50	02	6	8	0	0	9	2	×	8	
	12	1014.3	W 8	7.2	72	20-50	62	6	8	0	0	9	2	×	9	
	15	1012.0	W 6	8.9	62	> 50	02	6	8	0	0	9	7	×	9	
17	18	1010.0	W 6	10.2	10.3	..	52	> 50	01	2	7	0	0	9	4	×	9	trace
	21	1008.7	NE'E 9	4.2	61	> 50	40	1	4	0	0	9	4	2	8	
	00	1007.7	SE'E 6	2.9	71	> 50	03	1	4	2	6	3	4	4	8	
	03	1006.2	E'S 3	2.0	82	0.5-1	47	4	9	9	×	0	×	×	8	
	06	1004.6	E 4	1.0	..	0.5	84	0.5-1	47	4	9	9	×	0	×	×	9	0.0
	09	1004.4	E 2	0.6	85	0.5-1	45	4	9	9	×	0	×	×	6	
18	12	1004.3	SE'E 2	1.6	83	20-50	01	4	7	1	6	2	4	×	8	
	15	1003.7	SE'E 5	2.8	79	20-50	01	2	7	1	6	2	4	×	9	
	18	1003.9	NE'E 4	2.9	10.4	..	72	> 50	03	2	8	1	6	2	7	×	4	0.0
	21	1004.1	NE'E 5	3.5	75	20-50	03	2	8	6	6	3	7	×	3	
	00	1004.4	E'S 5	2.5	74	20-50	02	2	8	8	5	3	×	×	3	
	03	1005.1	E 4	2.5	73	20-50	02	2	8	8	5	4	×	×	3	
19	06	1006.3	E 6	2.7	..	0.1	72	20-50	02	2	8	8	5	4	×	×	4	0.0
	09	1009.1	SE'E 5	2.2	72	20-50	02	2	8	8	5	3	×	×	4	
	12	1009.9	E 4	1.8	73	10-20	60	6	8	8	5	2	×	×	1	
	15	1011.3	E 5	1.5	78	20-50	02	6	8	8	5	3	×	×	4	
	18	1012.0	E 3	1.7	3.5	..	76	20-50	02	1	7	5	6	3	4	×	1	trace
	21	1012.6	SE'E 6	2.2	76	20-50	02	6	8	8	5	3	×	×	3	
20	00	1013.1	0	2.0	80	2-4	63	6	8	8	7	4	×	×	3	
	03	1013.3	WSW 10	3.2	76	1-2	63	6	8	8	7	4	×	×	3	
	06	1013.6	W 10	2.7	..	1.0	76	1-2	63	6	8	8	7	3	×	×	3	×
	09	1013.6	W 10	2.0	78	1-2	68	6	8	8	7	3	×	×	3	
	12	1013.6	W 8	1.5	82	4-10	61	6	8	8	7	3	×	×	3	
	15	1013.6	W 7	1.5	82	2-4	70	7	8	8	7	3	×	×	3	
21	18	1014.1	E 4	0.0	3.5	..	83	2-4	70	7	8	8	7	3	×	×	4	×
	21	1014.3	E 1	0.2	88	2-4	71	7	8	8	7	3	×	×	3	
	00	1014.6	E 3	0.2	86	2-4	02	7	8	8	5	4	×	×	3	
	03	1014.4	E 4	÷ 0.5	84	2-4	01	2	7	7	5	3	0	0	9	
	06	1014.3	E 4	÷ 1.3	..	÷ 2.0	84	1-2	03	2	8	8	6	2	×	×	8	trace
	09	1014.2	E 3	÷ 1.0	84	2-4	01	2	6	4	6	2	0	2	8	
22	12	1014.2	SE'E 6	÷ 0.8	81	4-10	03	2	8	7	6	2	×	×	4	
	15	1013.8	E 6	0.5	71	10-20	01	2	7	5	2	0	×	×	9	
	18	1014.0	ESE 2	0.2	1.5	..	71	> 50	01	2	8	1	1	3	0	7	4	0.0
	21	1014.2	0	0.9	66	> 50	01	2	8	1	1	4	0	7	3	
	00	1014.3	0	0.8	66	> 50	01	2	7	0	0	9	0	4	3	
	03	1014.1	0	÷ 0.4	68	> 50	02	2	7	0	0	9	0	2	9	
23	06	1014.0	0	1.2	..	÷ 1.6	70	> 50	02	2	6	0	0	9	0	2	8	0.0
	09	1013.7	0	1.4	68	> 50	02	2	6	0	0	9	4	2	8	
	12	1012.8	WSW 1	2.7	45	> 50	01	1	1	0	0	9	0	2	9	
	15	1011.1	SE'E 3	2.0	52	> 50	01	1	1	0	0	9	0	2	9	
	18	1009.7	0	3.7	3.7	..	45	> 50	01	0	1	0	0	9	4	0	8	0.0
	21	1008.2	WSW 8	4.4	41	> 50	01	0	1	0	0	9	4	0	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
22	00	1006.4	SW'W3	3.3	50	> 50	02	0	1	0	0	9	4	0	8	0.0	
	03	1004.6	E 1	÷ 0.1	64	> 50	02	0	1	0	0	9	4	0	8		
	06	1003.3	E 5	÷ 1.2	..	÷ 1.9	68	> 50	03	0	2	0	0	9	4	4	8		
	09	1001.9	E 5	0.5	61	> 50	02	0	3	0	0	9	4	4	8		
	12	1000.6	SE'E 6	0.5	59	> 50	03	2	6	0	0	9	5	6	8		
	15	1000.0	ENE 7	1.5	59	> 50	03	2	7	0	0	9	5	6	6		
23	18	1000.2	SE'E 7	1.5	4.6	..	59	> 50	03	2	8	0	0	9	7	×	5	0.0	
	21	1000.4	E 6	1.0	57	> 50	02	2	8	0	0	9	7	×	3		
	00	1000.7	E 4	÷ 0.3	60	> 50	02	2	8	0	0	9	7	×	3		
	03	1000.9	E 2	÷ 1.0	75	> 50	02	2	8	0	0	9	7	×	3		
	06	1000.6	0	÷ 0.2	..	÷ 1.8	80	> 50	01	2	6	0	0	9	7	2	9		0.0
	09	1000.3	0	1.8	75	> 50	03	2	7	0	0	9	5	5	8		
24	12	999.4	WSW 6	4.1	54	> 50	03	2	8	0	0	9	5	5	9	trace	
	15	998.6	WSW 8	5.0	50	> 50	02	2	7	0	0	9	7	0	8		
	18	998.3	WSW 8	3.5	5.4	..	54	10-20	21	2	8	6	6	4	2	×	6		
	21	998.3	W 8	2.0	66	4-10	71	7	8	8	5	2	2	×	3		
	00	998.3	W 8	1.5	77	4-10	71	7	8	5	5	2	2	×	3		
	03	998.7	W 8	1.2	77	4-10	71	7	8	1	5	2	2	×	3		
25	06	998.6	W 9	1.2	..	1.0	73	20-50	01	7	8	1	5	4	2	×	9	trace	
	09	998.1	W 9	1.4	65	20-50	01	2	8	1	5	4	2	×	9		
	12	998.6	W 8	1.7	60	20-50	02	2	8	0	0	9	7	×	4		
	15	998.3	W 7	2.2	59	> 50	02	2	8	0	0	9	7	×	9		
	18	997.8	W 6	2.3	3.5	..	56	> 50	02	2	8	0	0	9	7	×	8		0.0
	21	997.1	W 5	2.2	56	> 50	02	2	8	0	0	9	7	×	8		
26	00	997.0	W 5	1.5	59	> 50	02	2	8	0	0	9	7	×	6	0.0	
	03	997.6	SE'E 2	1.6	63	10-20	70	7	8	1	5	3	7	×	4		
	06	998.0	SE 3	÷ 0.6	..	÷ 1.0	71	1-2	73	7	8	8	6	3	×	×	3		trace
	09	998.8	SE'E 3	÷ 0.3	79	10-20	01	7	8	8	6	3	×	×	3		
	12	999.2	E 4	0.1	82	10-20	02	2	8	8	6	3	×	×	3		
	15	999.2	E 5	÷ 0.2	80	10-20	02	2	8	8	6	3	×	×	3		
18	999.1	E'S 8	÷ 0.6	2.1	..	80	10-20	02	2	8	5	6	3	5	×	9	0.0		
21	998.0	NE 5	÷ 1.6	80	10-20	01	2	5	3	6	3	4	×	9			
27	00	997.6	E 5	÷ 1.6	80	20-50	03	2	8	8	5	6	×	×	6	0.0	
	03	996.8	E 4	÷ 2.0	80	> 50	02	2	8	1	5	3	7	×	9		
	06	996.8	E 1	÷ 2.3	..	÷ 3.1	80	> 50	02	2	8	1	5	3	7	×	9		
	09	996.5	0	÷ 1.1	71	> 50	02	2	8	1	5	6	7	×	3		
	12	997.4	0	÷ 0.1	63	> 50	01	2	7	7	0	7	7	×	4		
	15	998.1	0	1.0	50	> 50	01	2	3	0	0	9	4	0	3		
28	18	999.9	0	1.4	1.5	..	46	> 50	01	0	1	1	1	8	0	0	4	0.0	
	21	1001.8	E 3	0.3	52	> 50	00	0	0	0	0	9	0	0	3		
	00	1004.3	E 1	÷ 2.0	62	> 50	03	0	2	0	0	9	0	2	3		
	03	1006.4	0	÷ 2.2	66	> 50	01	0	1	0	0	9	0	1	3		
	06	1008.5	WSW 5	÷ 1.6	..	÷ 3.5	48	> 50	01	0	1	0	0	9	0	1	3		0.0
	09	1009.6	WSW 3	÷ 0.2	44	> 50	00	0	0	0	0	9	0	0	3		
29	12	1010.3	E 2	0.4	44	> 50	00	0	0	0	0	9	0	0	3		
	15	1010.6	E 2	1.4	45	> 50	03	0	4	0	0	9	0	5	3		
	18	1010.5	E 2	1.4	1.4	..	45	> 50	01	0	3	0	0	9	0	2	9	0.0	
	21	1010.4	0	1.7	50	> 50	00	0	0	0	0	9	0	0	8		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
28	00	1010.3	E 5	÷ 1.8	56	> 50	00	0	0	0	0	9	0	0	8	
	03	1010.3	E 3	÷ 2.9	62	> 50	00	0	0	0	0	9	0	0	3	
	06	1010.4	E 1	÷ 2.5	..	÷ 4.0	60	> 50	01	0	1	0	0	9	0	1	3	0.0
	09	1010.1	E 3	÷ 2.2	59	> 50	00	0	0	0	0	9	0	0	9	
	12	1009.8	E 3	÷ 1.4	58	> 50	00	0	0	0	0	9	0	0	8	
	15	1008.2	E 2	÷ 0.3	52	> 50	00	0	0	0	0	9	0	0	9	
	18	1007.3	E 2	0.2	2.2	..	46	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1006.5	E 5	÷ 2.3	62	> 50	00	0	0	0	0	9	0	0	8	
29	00	1005.7	E 6	÷ 4.0	66	> 50	00	0	0	0	0	9	0	0	8	
	03	1004.3	E 5	÷ 4.4	54	> 50	03	1	5	0	0	9	0	2	8	0.0
	06	1003.5	E 4	÷ 4.1	..	÷ 4.5	66	> 50	02	1	3	0	0	9	0	2	8	0.0
	09	1003.3	E 3	÷ 4.0	58	> 50	03	2	7	0	0	9	5	4	6	
	12	1003.8	E 1	÷ 4.1	58	> 50	02	2	8	0	0	9	2	×	4	
	15	1004.9	0	÷ 3.5	68	> 50	02	2	8	0	0	9	2	×	3	
	18	1005.8	W 11	1.5	1.5	..	40	> 50	02	2	8	0	0	9	2	×	3	0.0
	21	1008.5	W 10	1.2	37	> 50	02	2	8	0	0	9	7	×	4	
30	00	1010.9	W 11	0.9	46	> 50	02	2	8	0	0	9	7	×	3	
	03	1012.1	W 12	0.2	44	> 50	01	2	7	0	0	9	4	0	1	
	06	1013.9	W 10	0.2	..	÷ 4.0	50	> 50	01	2	6	0	0	9	4	0	3	0.0
	09	1015.3	W 11	0.4	50	> 50	01	2	5	0	0	9	4	2	3	
	12	1015.9	W 9	1.4	52	> 50	01	1	1	0	0	9	4	2	4	
	15	1015.3	W 6	2.6	42	> 50	01	0	1	0	0	9	4	2	9	
	18	1015.2	W 8	2.6	2.8	..	41	> 50	01	0	1	0	0	9	4	0	3	0.0
	21	1015.5	W 6	2.3	44	> 50	02	0	1	0	0	9	0	2	3	
31	00	1016.3	W 3	0.5	45	> 50	01	0	1	0	0	9	0	2	4	
	03	1018.1	ENE 3	÷ 3.6	78	> 50	00	0	0	0	0	9	0	0	4	
	06	1019.2	0	÷ 4.5	..	÷ 5.1	86	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1020.7	W 6	÷ 0.4	50	> 50	03	0	1	0	0	9	5	0	3	
	12	1021.0	WSW 7	0.8	45	> 50	02	0	1	0	0	9	4	0	1	
	15	1021.1	WSW 5	1.6	43	> 50	00	0	0	0	0	9	0	0	1	
	18	1021.2	WSW 7	2.4	2.7	..	40	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1022.1	WSW 6	2.1	41	> 50	02	0	1	0	0	9	4	0	4	
Mean		1011.7		5.0		3.7	5.9	1.0	66	×

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1023.4	WSW 6	0.6	48	> 50	02	0	1	0	0	9	4	0	3	
	03	1024.4	WSW 5	÷ 0.6	53	> 50	03	0	1	0	0	9	5	1	3	
	06	1024.9	SW'S 3	÷ 1.2	..	÷ 1.6	50	> 50	03	0	2	0	0	9	5	2	3	0.0
	09	1025.9	W 5	1.2	54	> 50	03	2	7	0	0	9	5	2	3	
	12	1026.2	W 6	1.6	49	> 50	03	2	7	0	0	9	5	2	6	
	15	1026.1	W 6	2.6	44	> 50	01	2	7	0	0	9	4	0	3	
	18	1026.0	W 7	1.5	2.9	..	54	> 50	01	2	6	0	0	9	4	0	9	0.0
	21	1026.4	SW'W 3	1.3	52	> 50	03	2	7	0	0	9	4	×	4	
2	00	1026.9	WSW 3	1.3	52	> 50	02	2	7	0	0	9	4	×	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1027.1	W 7	1.0	54	> 50	02	2	7	0	0	9	4	4	3	
	06	1027.4	W 2	1.0	..	÷ 1.2	55	> 50	01	2	6	0	0	9	5	0	3	0.0
	09	1027.8	E 2	1.1	56	> 50	03	2	7	0	0	9	5	0	3	
	12	1027.5	0	1.4	54	> 50	03	2	8	0	0	9	4	7	9	
	15	1025.7	0	2.0	54	> 50	02	2	8	0	0	9	2	×	8	
	18	1024.3	W 3	3.0	3.0	..	53	> 50	02	2	8	0	0	9	4	6	8	0.0
	21	1023.3	W 4	2.6	60	> 50	02	2	8	2	5	8	4	7	8	
3	00	1022.5	W 4	3.6	70	> 50	02	2	8	1	5	8	4	4	8	
	03	1021.6	W 1	3.1	71	> 50	02	2	8	1	5	8	4	4	8	
	06	1020.7	W 2	3.0	..	1.0	72	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1020.5	W 6	4.5	64	> 50	02	2	8	0	0	9	7	×	6	
	12	1020.4	W 9	5.0	63	> 50	02	2	8	0	0	9	7	4	8	
	15	1020.0	W 8	4.6	61	> 50	02	2	8	0	0	9	7	6	8	
	18	1019.7	W 6	4.7	5.3	..	60	> 50	01	2	7	0	0	9	4	0	8	0.0
	21	1020.7	E 2	1.2	65	> 50	01	2	7	0	0	9	4	4	4	
4	00	1021.2	E 2	0.5	70	> 50	02	2	7	2	5	8	4	3	3	
	03	1021.7	E 2	0.0	74	> 50	01	2	5	4	5	7	4	0	3	
	06	1021.0	E 3	÷ 0.2	..	÷ 1.0	76	> 50	03	2	7	7	5	8	4	0	3	0.0
	09	1021.2	E 4	÷ 0.4	78	> 50	03	2	8	7	5	5	5	×	9	
	12	1020.8	E 1	÷ 0.4	82	> 50	03	2	8	2	6	6	7	×	9	
	15	1019.9	E 3	÷ 0.6	83	> 50	02	2	8	1	6	4	2	×	8	
	18	1018.9	E 1	÷ 0.6	4.7	..	83	> 50	02	2	8	1	6	4	2	×	8	0.0
	21	1017.9	E 4	÷ 1.0	84	> 50	02	2	8	2	6	4	2	×	8	
5	00	1017.6	E 4	÷ 1.3	84	20-50	77	7	8	3	6	4	2	×	8	
	03	1017.6	0	÷ 1.6	84	20-50	77	7	8	6	6	4	2	×	3	
	06	1017.1	0	÷ 2.0	86	4-10	77	7	8	8	6	2	×	×	9	trace
	09	1015.7	0	÷ 1.5	74	4-10	77	7	8	6	6	2	5	×	9	
	12	1014.9	W 5	÷ 0.2	70	> 50	01	2	7	3	6	2	5	4	8	
	15	1013.9	W 5	0.3	62	> 50	02	2	7	1	6	2	5	0	8	
	18	1012.8	W 2	0.1	0.4	..	62	> 50	02	2	7	1	6	2	5	0	8	trace
	21	1012.1	E 6	÷ 2.5	72	4-10	77	7	8	8	6	2	×	×	8	
6	00	1011.2	E 6	÷ 2.6	75	4-10	77	7	8	8	6	2	×	×	8	
	03	1009.7	E 5	÷ 3.3	77	4-10	77	7	8	8	6	2	2	×	8	
	06	1008.6	E 6	÷ 3.0	..	÷ 3.7	78	4-10	77	7	8	8	6	2	×	×	8	trace
	09	1007.5	E 5	÷ 4.0	80	10-20	77	7	8	8	6	2	×	×	8	
	12	1006.6	E 5	÷ 4.1	80	4-10	77	7	8	8	6	2	×	×	8	
	15	1004.9	E 4	÷ 4.1	81	4-10	77	7	8	8	6	2	×	×	9	
	18	1003.5	E 4	÷ 4.0	0.0	..	80	4-10	77	7	8	8	6	2	×	×	8	trace
	21	1002.4	E 4	÷ 4.5	80	4-10	77	7	8	8	6	2	×	×	8	
7	00	1001.3	E 2	÷ 4.5	80	4-10	77	7	8	8	6	2	×	×	8	
	03	1000.0	0	÷ 6.5	81	20-50	01	7	7	1	6	4	2	0	8	
	06	999.3	0	÷ 5.0	..	÷ 6.5	81	20-50	01	2	6	5	6	2	4	0	8	trace
	09	998.4	0	÷ 5.1	78	> 50	02	2	6	3	6	2	5	0	8	
	12	997.1	W 3	÷ 0.9	74	> 50	01	1	3	1	6	3	4	0	8	
	15	996.2	WSW 2	÷ 5.0	60	> 50	00	0	0	0	0	9	0	0	8	
	18	995.5	0	÷ 3.6	÷ 0.9	..	52	> 50	00	0	0	0	0	9	0	0	8	trace
	21	994.5	0	÷ 5.4	59	> 50	03	0	1	0	0	9	0	5	8	
8	90	993.8	0	÷ 7.2	62	> 50	03	0	2	0	0	9	0	5	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	993.0	SW 1	÷ 7.6	65	> 50	03	0	3	0	0	9	0	5	8	
	06	992.8	S 3	÷ 8.3	..	÷ 8.9	66	> 50	03	2	6	0	0	9	0	6	6	0.0
	09	992.6	0	÷ 5.7	62	> 50	01	1	3	0	0	9	0	2	8	
	12	992.5	0	÷ 7.5	64	> 50	01	0	2	0	0	9	0	2	8	
	15	993.2	0	÷ 7.2	64	> 50	00	0	0	0	0	9	0	0	4	
	18	993.9	0	÷ 8.3	÷ 3.5	..	74	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	995.5	0	÷ 8.8	64	> 50	03	0	1	0	0	9	5	0	4	
9	00	996.3	0	÷ 8.2	74	> 50	02	0	1	0	0	9	5	0	3	
	03	997.2	SW W 3	÷ 5.5	62	> 50	02	0	1	0	0	9	0	5	3	
	06	997.5	E 6	÷ 8.0	..	÷ 9.0	59	> 50	02	0	1	0	0	9	0	5	3	0.0
	09	997.2	E 5	÷ 8.0	58	> 50	02	0	1	0	0	9	0	5	9	
	12	996.4	S'E 5	÷ 6.4	56	> 50	02	0	1	0	0	9	0	5	8	
	15	996.4	0	÷ 7.0	56	> 50	00	0	0	0	0	9	0	0	3	
	18	997.4	WSW 6	÷ 6.2	÷ 6.2	..	58	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	998.8	WSW 4	÷ 5.4	57	> 50	00	0	0	0	0	9	0	0	3	
10	00	1000.4	ESE 3	÷ 8.5	62	> 50	00	0	0	0	0	9	0	0	3	
	03	1000.5	0	÷ 8.5	62	> 50	00	0	0	0	0	9	0	0	3	
	06	1001.7	0	÷ 8.4	..	÷ 9.8	62	> 50	03	2	7	0	0	9	0	7	4	0.0
	09	1002.2	0	÷ 7.3	62	> 50	03	2	8	0	0	9	2	7	3	
	12	1002.0	SW 1	÷ 6.0	62	> 50	01	0	3	0	0	9	0	2	9	
	15	1001.4	WSW 3	÷ 5.1	56	> 50	01	0	1	0	0	9	0	2	9	
	18	1001.1	WSW 1	÷ 4.1	÷ 3.9	..	54	> 50	01	0	1	0	0	9	0	2	8	0.0
	21	1001.1	WSW 4	÷ 4.5	54	> 50	03	0	3	0	0	9	0	2	3	
11	00	1001.6	SW 5	÷ 4.0	56	> 50	01	0	1	0	0	9	4	2	3	
	03	1002.6	SW 3	÷ 5.6	58	> 50	02	1	4	0	0	9	4	2	4	
	06	1002.0	WSW 3	÷ 5.6	..	÷ 8.0	60	> 50	02	2	8	0	0	9	5	6	9	0.0
	09	1001.6	E 5	÷ 3.5	61	> 50	02 ¹	2	8	0	0	9	4	7	8	
	12	1000.2	E 6	÷ 2.5	58	> 50	02	2	8	0	0	9	7	7	9	
	15	997.1	E 7	÷ 3.7	58	> 50	02	2	8	0	0	9	7	7	9	
	18	996.1	E 1	÷ 4.2	÷ 2.2	..	61	> 50	01	2	6	0	0	9	0	6	6	0.0
	21	994.3	0	÷ 6.8	63	> 50	01	1	1	0	0	9	4	0	8	
12	00	993.8	WSW 5	÷ 5.0	66	> 50	02	0	1	0	0	9	4	0	6	
	03	994.5	W 8	÷ 4.5	58	> 50	03	0	4	0	0	9	4	5	4	
	06	995.5	W 10	÷ 4.6	..	÷ 5.7	58	> 50	03	2	8	0	0	9	0	7	3	0.0
	09	997.4	W 11	÷ 4.5	60	> 50	01	2	7	0	0	9	7	7	4	
	12	998.9	W 13	÷ 3.4	52	> 50	03	2	8	0	0	9	7	×	3	
	15	1000.0	W 14	÷ 3.2	56	20-50	09	3	8	0	0	9	7	×	3	
	18	1000.7	W 16	÷ 3.0	÷ 2.5	..	44	20-50	09	3	8	0	0	9	7	×	3	0.0
	21	1902.9	W 14	÷ 3.3	43	20-50	09	3	8	0	0	9	2	×	4	
13	00	1005.1	W 13	÷ 3.0	36	20-50	09	3	8	0	0	9	2	×	3	
	03	1008.2	W 14	÷ 2.9	34	20-50	09	3	8	0	0	9	2	×	4	
	06	1010.3	W 13	÷ 3.0	..	÷ 4.5	32	> 50	09	3	8	0	0	9	2	×	3	0.0
	09	1012.9	W 13	÷ 3.0	40	> 50	09	3	8	0	0	9	7	×	3	
	12	1014.5	W 11	÷ 2.3	36	> 50	09	3	8	0	0	9	7	×	3	
	15	1015.8	W 11	÷ 1.8	43	> 50	09	3	8	0	0	9	2	×	3	
	18	1016.3	W 7	÷ 1.6	÷ 1.4	..	43	> 50	02	2	8	0	0	9	2	×	3	0.0
	21	1017.0	WSW 5	÷ 2.1	39	> 50	02	2	8	0	0	9	4	7	3	
14	00	1017.6	0	÷ 3.0	39	> 50	02	2	8	0	0	9	0	7	3	

¹ 0900 Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1017.6	WSW 2	÷ 3.0	43	> 50	02	2	8	0	0	9	0	7	3	
	06	1017.5	SSE 2	÷ 5.3	..	÷ 6.2	47	> 50	02	2	8	0	0	9	0	7	9	0.0
	09	1017.7	SE 3	÷ 5.5	50	> 50	02	2	8	0	0	9	0	7	9	
	12	1017.8	SE 2	÷ 4.2	48	> 50	01	2	6	0	0	9	0	7	3	
	15	1017.0	SE'E 3	÷ 4.5	46	> 50	01	2	2	0	0	9	0	8	9	
	18	1017.0	SE'E 3	÷ 5.7	÷ 2.0	..	58	> 50	01	1	1	0	0	9	0	8	3	0.0
	21	1017.0	SE 4	÷ 7.0	62	> 50	01	0	1	0	0	9	0	8	3	
15	00	1017.7	0	÷ 8.0	62	> 50	00	0	0	0	0	9	0	0	4	
	03	1018.3	0	÷ 9.8	68	> 50	03	0	1	0	0	9	4	0	3	
	06	1018.9	0	÷ 10.0	..	÷ 10.0	67	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1019.9	0	÷ 9.4	70	> 50	03	0	1	0	0	9	0	4	3	
	12	1020.6	0	÷ 7.0	68	> 50	02	0	1	0	0	9	0	4	3	
	15	1020.1	0	÷ 6.9	60	> 50	02	0	1	0	0	9	0	4	9	
	18	1019.7	0	÷ 5.6	÷ 5.5	..	60	> 50	02	0	1	0	0	9	0	4	8	0.0
	21	1019.5	0	÷ 8.5	58	> 50	02	0	1	0	0	9	4	0	8	
16	00	1019.5	0	÷ 9.2	56	> 50	02	0	1	0	0	9	4	0	3	
	03	1019.8	W 3	÷ 8.2	56	> 50	02	0	1	0	0	9	4	0	4	
	06	1019.3	0	÷ 8.7	..	÷ 10.2	56	> 50	02	0	1	0	0	9	4	0	9	0.0
	09	1018.9	SE'E 4	÷ 8.0	56	> 50	02	0	1	0	0	9	4	0	8	
	12	1019.1	SE'E 2	÷ 7.5	54	> 50	02	0	1	0	0	9	4	1	4	
	15	1017.8	0	÷ 6.2	56	> 50	02	0	1	0	0	9	4	2	9	
	18	1017.5	0	÷ 5.6	÷ 5.5	..	54	> 50	02	0	1	0	0	9	4	2	6	0.0
	21	1017.9	0	÷ 6.2	56	> 50	02	0	1	0	0	9	4	0	4	
17	00	1018.1	0	÷ 5.8	60	> 50	03	1	4	0	0	9	3	0	3	
	03	1018.6	0	÷ 5.0	64	> 50	01	1	1	0	0	9	4	0	3	
	06	1018.6	0	÷ 6.4	..	÷ 9.4	66	> 50	02	0	1	0	0	9	4	2	3	0.0
	09	1018.7	E'S 3	÷ 5.6	66	> 50	02	0	1	0	0	9	4	2	3	
	12	1018.1	SE'E 5	÷ 6.0	62	> 50	03	0	1	0	0	9	5	0	9	
	15	1016.8	0	÷ 4.9	60	> 50	01	0	2	0	0	9	4	0	8	
	18	1016.1	0	÷ 4.5	÷ 4.5	..	58	> 50	03	0	2	0	0	9	4	4	6	0.0
	21	1015.6	0	÷ 5.3	63	> 50	03	0	2	0	0	9	5	4	8	
18	00	1015.0	S 1	÷ 6.6	66	> 50	02	0	2	0	0	9	5	0	8	
	03	1016.1	0	÷ 9.0	70	> 50	01	0	1	0	0	9	4	0	4	
	06	1013.1	SE 2	÷ 9.0	..	÷ 10.0	72	> 50	03	0	3	0	0	9	4	6	9	0.0
	09	1012.6	S 1	÷ 7.8	72	> 50	01	0	2	0	0	9	4	0	6	
	12	1011.8	S 1	÷ 5.9	72	> 50	02	0	2	0	0	9	4	1	8	
	15	1009.8	WSW 7	÷ 3.5	62	> 50	02	0	2	0	0	9	4	0	9	
	18	1008.7	W 6	÷ 3.2	÷ 3.0	..	60	> 50	02	0	1	0	0	9	4	1	8	0.0
	21	1007.5	SE'S 5	÷ 6.9	62	> 50	02	0	1	0	0	9	4	0	8	
19	00	1006.8	S 2	÷ 8.1	65	> 50	02	0	1	0	0	9	4	0	8	
	03	1005.7	0	÷ 9.6	70	> 50	02	0	1	0	0	9	7	0	8	
	06	1004.7	0	÷ 10.1	..	÷ 10.9	74	> 50	02	0	1	0	0	9	7	0	8	0.0
	09	1004.5	0	÷ 10.0	74	> 50	02	0	1	0	0	9	4	0	6	
	12	1003.9	0	÷ 7.5	75	> 50	02	0	1	0	0	9	4	1	9	
	15	1004.3	0	÷ 8.0	68	> 50	03	0	2	0	0	9	7	1	4	
	18	1004.4	W 8	÷ 4.2	÷ 4.2	..	50	> 50	03	1	7	0	0	9	7	×	3	0.0
	21	1007.9	W 8	÷ 3.8	50	> 50	03	2	8	0	0	9	2	×	4	
20	00	1009.5	W 10	÷ 4.6	46	> 50	03	2	8	0	0	9	2	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1011.8	W 8	÷ 7.0	60	> 50	01	1	3	0	0	9	4	1	4	
	06	1012.8	W 7	÷ 7.9	..	÷10.5	60	> 50	01	1	3	0	0	9	4	1	3	0.0
	09	1013.6	W 4	÷ 7.7	57	> 50	01	0	3	0	0	9	4	2	3	
	12	1013.8	W 3	÷ 7.0	55	> 50	01	0	2	0	0	9	4	9	1	
	15	1014.1	W 5	÷ 6.0	52	> 50	02	0	3	0	0	9	4	9	3	
	18	1013.8	WSW 5	÷ 5.9	÷ 3.2	..	50	> 50	01	0	1	0	0	9	4	1	9	0.0
	21	1013.7	SSW 1	÷ 8.5	56	> 50	02	0	1	0	0	9	4	0	6	
21	00	1013.4	0	÷ 9.1	60	> 50	02	0	1	0	0	9	4	0	8	
	03	1013.4	0	÷ 8.6	65	> 50	03	1	7	0	0	9	7	×	3	
	06	1013.2	0	÷10.0	..	÷10.1	70	> 50	01	1	4	0	0	9	7	0	9	0.0
	09	1013.6	S 2	÷ 8.0	69	> 50	01	0	1	0	0	9	4	0	4	
	12	1012.4	0	÷ 8.0	66	> 50	01	0	1	0	0	9	4	0	9	
	15	1011.8	0	÷ 7.8	62	> 50	03	1	3	0	0	9	4	9	6	
	18	1011.4	0	÷ 7.6	÷ 5.5	..	64	> 50	03	2	7	0	0	9	3	×	8	0.0
	21	1011.6	0	÷ 8.0	64	> 50	02	2	7	0	0	9	3	×	4	
22	00	1012.0	SE 1	÷ 8.1	64	> 50	02	2	8	0	0	9	3	×	3	
	03	1012.7	0	÷ 8.6	64	> 50	01	2	7	0	0	9	3	×	3	
	06	1014.2	SE'E 3	÷ 9.8	..	÷ 9.8	68	10—20	03	2	8	4	5	5	2	×	4	0.0
	09	1017.0	NW'W 8	÷ 6.8	67	> 50	02	2	7	0	0	9	7	2	4	
	12	1017.4	W 10	÷ 7.4	64	10—20	01	2	6	1	5	5	4	2	1	
	15	1018.0	W 15	÷ 7.2	51	4—10	02	2	7	0	0	9	7	×	3	
	18	1019.3	W 15	÷ 7.5	÷ 6.0	..	55	4—10	09	3	7	0	0	9	7	×	4	0.0
	21	1021.3	W 14	÷ 7.5	50	4—10	09	3	7	0	0	9	7	×	4	
23	00	1021.7	W 14	÷ 7.5	50	4—10	09	3	7	0	0	9	7	×	1	
	03	1021.5	W 11	÷ 7.8	56	> 50	02	2	7	0	0	9	7	×	9	
	06	1020.5	W 9	÷ 7.5	..	÷10.2	53	> 50	02	2	8	0	0	9	7	×	9	0.0
	09	1018.4	W 8	÷ 7.2	60	> 50	05	2	8	0	0	9	2	×	9	
	12	1017.7	SW 8	÷ 6.3	56	10—20	01	2	8	0	0	9	2	×	6	
	15	1016.1	W 10	÷ 5.8	76	10—20	05	2	8	0	0	9	2	×	9	
	18	1015.0	W 11	÷ 5.4	÷ 5.4	..	72	10—20	05	2	8	0	0	9	7	×	8	0.0
	21	1015.8	W 9	÷ 5.8	76	20—50	05	2	8	0	0	9	7	×	4	
24	00	1016.2	W 10	÷ 5.5	58	20—50	02	2	8	0	0	9	7	×	3	
	03	1017.1	W 10	÷ 5.3	56	> 50	02	2	8	0	0	9	7	×	4	
	06	1018.1	W 10	÷ 5.5	..	÷ 7.5	59	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1018.9	W 10	÷ 5.1	60	> 50	02	2	8	0	0	9	7	×	3	
	12	1020.1	W 14	÷ 4.7	56	> 50	02	2	8	0	0	9	7	×	3	
	15	1021.8	W 12	÷ 4.3	66	20—50	02	2	8	0	0	9	7	×	3	
	18	1022.3	W 9	÷ 4.8	÷ 4.1	..	68	> 50	02	2	8	0	0	9	7	×	1	0.0
	21	1023.0	W 5	÷ 5.5	60	> 50	01	2	6	0	0	9	7	×	3	
25	00	1022.7	W 5	÷ 5.8	60	> 50	02	2	7	0	0	9	7	×	9	
	03	1022.0	W 5	÷ 5.5	60	> 50	02	2	8	0	0	9	7	×	8	
	06	1018.9	W 9	÷ 4.7	..	÷ 6.2	58	> 50	02	2	8	0	0	9	7	×	9	0.0
	09	1016.2	W 8	÷ 5.2	62	> 50	01	2	4	0	0	9	7	×	8	
	12	1014.2	W 10	÷ 4.5	56	> 50	03	2	7	0	0	9	7	×	8	
	15	1010.8	W 5	÷ 4.5	58	> 50	03	2	8	0	0	9	7	×	8	
	18	1009.2	W 7	÷ 4.5	÷ 4.3	..	55	20—50	01	2	7	0	0	9	7	×	6	0.0
	21	1008.2	W 5	÷ 4.7	60	4—10	70	7	8	8	5	4	×	×	8	
26	00	1008.2	0	÷ 6.3	79	1—2	73	7	8	8	5	3	×	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1007.7	0	÷ 7.2	86	1-2	71	7	8	8	5	3	×	×	4	
	06	1007.5	0	÷ 8.0	..	÷ 8.0	84	1-2	73	7	8	8	×	×	×	×	9	×
	09	1007.9	0	÷ 10.1	81	2-4	71	7	8	8	0	3	2	×	8	
	12	1007.9	0	÷ 10.9	82	1-2	71	7	8	8	×	×	×	×	3	
	15	1007.7	E 4	÷ 13.4	82	1-2	71	7	8	8	×	×	×	×	9	
	18	1007.8	0	÷ 13.8	÷ 4.5	..	82	2-4	71	7	8	8	0	5	2	×	3	×
27	21	1007.6	W 6	÷ 9.6	70	1-2	71	7	8	8	×	×	×	×	9	
	00	1007.7	W 7	÷ 9.6	68	4-10	02	7	8	0	0	9	2	×	3	
	03	1007.8	W 8	÷ 9.9	72	4-10	02	3	8	0	0	9	2	×	3	
	06	1008.0	W 11	÷ 10.0	..	÷ 14.9	76	10-20	02	3	8	0	0	9	2	×	3	0.0
	09	1008.8	W 7	÷ 10.0	70	4-10	02	3	8	0	0	9	2	×	3	
	12	1009.6	W 13	÷ 10.8	76	0.5-1	36	3	8	9	0	9	2	×	3	
	15	1009.9	W 12	÷ 10.7	78	4-10	02	3	8	8	0	5	2	×	4	
	18	1011.3	W 11	÷ 10.5	÷ 9.5	..	76	4-10	02	3	8	8	0	5	2	×	1	0.0
	21	1012.9	W 12	÷ 10.5	72	4-10	02	3	8	8	0	4	2	×	4	
28	00	1014.1	W 13	÷ 10.8	80	1-2	02	3	8	8	×	×	×	×	3	
	03	1015.0	W 14	÷ 10.8	80	1-2	02	3	8	8	×	×	×	×	3	
	06	1014.6	W 12	÷ 10.9	..	÷ 11.2	78	4-10	02	2	8	0	0	9	2	×	9	0.0
	09	1016.8	W 12	÷ 10.8	81	4-10	02	2	8	0	0	9	7	×	4	
	12	1017.6	W 10	÷ 10.7	65	> 50	02	2	7	0	0	9	7	×	3	
	15	1018.8	W 8	÷ 10.7	60	20-50	02	2	7	0	0	9	7	×	3	
	18	1019.3	W 7	÷ 11.0	÷ 10.5	..	60	> 50	01	2	7	0	0	9	3	2	1	0.0
29	21	1019.4	W 8	÷ 11.4	60	> 50	01	2	6	0	0	9	3	2	3	
	00	1019.4	W 7	÷ 11.0	62	> 50	03	2	8	0	0	9	7	×	3	
	03	1018.5	W 6	÷ 10.6	60	> 50	02	2	8	0	0	9	7	×	9	
	06	1017.4	W 6	÷ 9.7	..	÷ 11.8	60	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1016.4	W 5	÷ 9.0	60	> 50	02	2	8	0	0	9	7	×	8	
	12	1015.8	W 6	÷ 8.4	58	> 50	02	2	8	0	0	9	2	×	8	
	15	1014.1	WSW 6	÷ 8.3	60	20-50	02	2	8	0	0	9	2	×	9	
	18	1013.2	WSW 5	÷ 9.2	÷ 8.0	..	64	> 50	01	2	7	0	0	9	2	×	6	0.0
	21	1012.3	WSW 6	÷ 10.3	68	> 50	03	2	8	0	0	9	1	×	8	
30	00	1012.0	WSW 5	÷ 10.8	68	> 50	02	2	8	0	0	9	1	×	6	
	03	1011.8	WSW 6	÷ 11.0	66	> 50	01	2	5	0	0	9	1	0	8	
	06	1011.9	W 7	÷ 12.1	..	÷ 12.2	65	> 50	03	2	6	0	0	9	7	0	3	0.0
	09	1012.0	W 6	÷ 13.0	62	> 50	02	2	5	0	0	9	7	0	3	
	12	1011.7	W 7	÷ 11.5	66	> 50	03	2	7	0	0	9	7	0	9	
	15	1010.0	WSW 6	÷ 12.2	60	> 50	01	2	5	0	0	9	1	0	9	
	18	1009.7	WSW 5	÷ 12.4	÷ 9.0	..	58	> 50	03	2	6	0	0	9	1	2	6	0.0
	21	1008.9	WSW 7	÷ 13.7	60	> 50	01	2	5	0	0	9	1	2	9	
Mean		1012.0	4.7	÷ 5.7	÷ 3.6	÷ 7.4	0.1

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1008.4	WSW 8	÷ 13.8	62	> 50	02	2	6	0	0	9	3	0	8	
	03	1007.9	WSW 6	÷ 13.1	61	> 50	02	2	6	0	0	9	3	0	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1007.7	WSW 6	÷14.3	..	÷14.3	60	> 50	01	1	2	0	0	9	3	0	6	0.0
	09	1007.3	WSW 5	÷14.1	60	> 50	02	1	2	0	0	9	3	0	8	
	12	1007.3	WSW 5	÷12.6	58	> 50	03	2	7	0	0	9	3	×	3	
	15	1007.2	WSW 3	÷12.0	56	> 50	02	2	7	0	0	9	3	×	3	
	18	1007.6	WSW 3	÷12.0	÷11.8	..	57	> 50	02	2	7	0	0	9	3	×	4	0.0
	21	1008.7	WSW 1	÷12.4	58	> 50	02	2	7	0	0	9	3	×	4	
2	00	1008.6	WSW 3	÷12.5	58	> 50	02	2	8	0	0	9	3	×	3	
	03	1009.3	WSW 2	÷12.5	58	> 50	02	2	8	0	0	9	3	×	4	
	06	1010.0	WSW 6	÷12.4	..	÷14.5	55	> 50	02	2	8	0	0	9	3	×	3	0.0
	09	1010.8	WSW 8	÷12.6	56	> 50	02	2	8	0	0	9	3	×	3	
	12	1011.1	WSW 7	÷12.6	52	> 50	02	2	7	0	0	9	3	×	1	
	15	1012.6	WSW 8	÷13.1	49	> 50	01	2	5	0	0	9	3	0	4	
	18	1012.9	WSW 8	÷13.3	÷12.0	..	49	> 50	03	2	6	0	0	9	3	0	1	0.0
	21	1014.9	WSW 5	÷13.2	50	> 50	03	2	7	0	0	9	3	0	4	
3	00	1015.8	WSW 6	÷13.7	50	> 50	02	2	7	0	0	9	7	×	1	
	03	1016.6	WSW 8	÷13.6	50	> 50	03	2	8	0	0	9	7	×	3	
	06	1017.2	WSW 5	÷13.5	..	14.1	50	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1019.5	WSW 7	÷13.8	50	> 50	02	2	8	0	0	9	7	×	4	
	12	1020.2	W 6	÷14.2	52	> 50	02	2	8	0	0	9	7	×	1	
	15	1021.2	W 8	÷14.9	50	20-50	01	2	7	0	0	9	7	2	3	
	18	1021.7	W 5	÷16.1	÷13.1	..	52	> 50	01	1	2	0	0	9	3	2	1	0.0
	21	1022.4	WSW 5	÷17.3	55	> 50	01	0	1	0	0	9	3	0	3	
4	00	1022.8	WSW 5	÷17.6	56	> 50	00	0	0	0	0	9	0	0	3	
	03	1023.1	WSW 5	÷17.9	57	> 50	02	0	1	0	0	9	4	0	3	
	06	1023.5	WSW 5	÷18.0	..	÷18.0	57	> 50	02	0	1	0	0	9	4	0	3	0.0
	09	1024.0	WSW 6	÷18.0	57	> 50	02	0	1	0	0	9	4	0	3	
	12	1022.8	WSW 6	÷18.4	56	> 50	02	0	1	0	0	9	4	0	9	
	15	1022.3	WSW 4	÷17.7	54	> 50	02	0	1	0	0	9	4	0	6	
	18	1022.1	WSW 5	÷17.6	÷16.0	..	54	> 50	03	2	7	0	0	9	3	×	6	0.0
	21	1021.8	WSW 4	÷17.1	57	> 50	03	2	7	0	0	9	7	×	8	
5	00	1021.7	W 1	÷16.0	60	> 50	03	2	8	0	0	9	7	×	6	
	03	1021.4	0	÷15.6	56	> 50	02	2	8	0	0	9	7	×	9	
	06	1021.0	E 1	÷15.5	..	÷18.6	59	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1021.5	E 1	÷15.7	62	20-50	02	2	8	8	6	4	×	×	4	
	12	1021.3	E 1	÷15.4	64	20-50	02	2	8	8	6	4	×	×	9	
	15	1020.9	0	÷15.2	68	20-50	02	2	8	8	6	4	×	×	8	
	18	1020.8	E 1	÷15.2	÷15.2	..	70	20-50	02	2	8	8	6	4	×	×	8	0.0
	21	1021.2	0	÷15.0	70	20-50	02	2	8	8	6	4	×	×	4	
6	00	1021.9	W 4	÷14.6	68	20-50	02	2	8	8	6	4	×	×	3	
	03	1022.6	W 5	÷14.6	65	20-50	02	2	8	8	6	4	×	×	3	
	06	1023.2	W 5	÷14.7	..	÷15.8	64	20-50	02	2	8	8	6	4	×	×	3	0.0
	09	1024.2	W 6	÷15.1	64	20-50	02	2	8	8	6	5	×	×	3	
	12	1024.4	W 6	÷15.8	64	> 50	01	2	7	0	0	9	3	×	1	
	15	1024.4	W 3	÷17.8	65	> 50	00	0	0	0	0	9	0	0	1	
	18	1024.2	W 3	÷18.8	÷14.6	..	66	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1023.7	W 3	÷19.5	66	> 50	00	0	0	0	0	9	0	0	8	
7	00	1023.5	W 3	÷19.7	66	> 50	00	0	0	0	0	9	0	0	8	
	03	1023.0	SW 5	÷20.4	66	> 50	00	0	0	0	0	9	0	0	8	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1023.3	SW 5	÷20.4	..	÷20.5	66	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1023.3	W 4	÷20.3	65	> 50	00	0	0	0	0	9	0	0	3	
	12	1023.3	W 5	÷20.1	64	> 50	00	0	0	0	0	9	0	0	3	
	15	1023.3	W 4	÷20.0	64	> 50	00	0	0	0	0	9	0	0	3	
	18	1023.9	W 2	÷20.0	÷18.9	..	63	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1024.8	W 1	÷21.0	62	> 50	00	0	0	0	0	9	0	0	3	
8	00	1025.1	W 3	÷21.0	63	> 50	00	0	0	0	0	9	0	0	3	
	03	1025.7	0	÷21.4	63	> 50	00	0	0	0	0	9	0	0	3	
	06	1026.0	0	÷21.5	..	÷21.5	62	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1026.9	0	÷21.5	63	> 50	03	0	1	0	0	9	0	2	4	
	12	1027.7	0	÷21.8	64	> 50	03	0	3	0	0	9	0	2	3	
	15	1027.9	0	÷22.0	66	> 50	01	0	1	0	0	9	0	2	1	
	18	1027.7	W 1	÷22.5	÷20.0	..	67	> 50	02	0	1	0	0	9	0	2	9	0.0
	21	1027.7	0	÷22.3	66	> 50	02	0	1	0	0	9	0	2	3	
9	00	1027.7	W 3	÷23.2	66	> 50	00	0	0	0	0	9	0	0	3	
	03	1027.0	W 2	÷23.0	67	> 50	00	0	0	0	0	9	0	0	9	
	06	1026.3	W 4	÷22.8	..	÷23.5	68	> 50	01	0	1	0	0	9	4	0	8	0.0
	09	1025.7	W 6	÷21.5	67	> 50	03	2	8	0	0	9	5	×	8	
	12	1025.5	SW 6	÷21.1	67	> 50	02	2	7	0	0	9	5	0	6	
	15	1025.4	SW 4	÷20.7	66	> 50	01	2	5	0	0	9	4	1	8	
	18	1025.2	SW 4	÷20.0	÷20.0	..	64	> 50	03	2	6	0	0	9	5	4	8	0.0
	21	1025.2	SW 5	÷19.8	64	> 50	02	2	8	0	0	9	7	×	3	
10	00	1025.1	SW 4	÷19.5	64	> 50	02	2	8	0	0	9	7	×	8	
	03	1024.8	SW 4	÷19.4	64	> 50	02	2	8	0	0	9	7	×	8	
	06	1024.6	WSW 3	÷19.2	..	÷23.0	64	> 50	01	2	8	0	0	9	3	×	8	0.0
	09	1024.3	WSW 3	÷19.0	64	> 50	02	2	8	0	0	9	3	×	8	
	12	1025.2	WSW 7	÷18.6	64	> 50	03	2	8	0	0	9	7	×	4	
	15	1025.3	W 6	÷18.6	64	20—50	02	2	8	0	0	9	7	×	1	
	18	1026.0	W 6	÷19.0	÷18.3	..	62	20—50	02	2	8	0	0	9	7	×	1	0.0
	21	1026.6	W 3	÷19.6	64	20—50	02	2	8	0	0	9	7	×	3	
11	00	1027.1	SW 3	÷19.7	65	> 50	01	2	8	0	0	9	3	×	3	
	03	1026.8	SE'E 4	÷21.5	65	> 50	01	2	8	0	0	9	3	×	9	
	06	1027.0	SE'E 4	÷21.4	..	÷21.5	66	> 50	02	2	8	0	0	9	3	×	4	0.0
	09	1026.4	SE'E 4	÷22.1	66	> 50	02	2	8	8	5	4	×	×	9	
	12	1026.3	SSE 4	÷21.8	66	> 50	77	2	8	8	5	4	×	×	8	
	15	1025.3	SSE 3	÷22.6	66	> 50	01	2	6	6	5	4	0	0	8	
	18	1024.2	SSE 4	÷23.5	÷18.9	..	66	> 50	03	2	6	6	5	5	0	0	8	trace
	21	1023.3	SSE 4	÷23.7	64	> 50	01	2	5	2	5	4	3	0	8	
12	00	1021.9	SSE 3	÷25.0	66	20—50	02	2	8	8	5	4	×	×	8	
	03	1020.8	WSW 4	÷23.0	69	2—4	71	7	8	8	7	4	2	×	8	
	06	1019.4	WSW 3	÷22.8	..	÷25.7	70	4—10	71	7	8	8	7	4	×	×	8	trace
	09	1018.8	0	÷21.9	70	2—4	71	7	8	8	7	4	×	×	6	
	12	1017.9	0	÷22.1	72	2—4	71	7	8	8	7	5	×	×	8	
	15	1016.4	0	÷21.9	72	2—4	71	7	8	8	7	5	×	×	9	
	18	1015.4	0	÷21.7	÷21.1	..	73	2—4	71	7	8	8	×	×	×	×	8	2.0
	21	1013.9	W 7	÷20.1	73	2—4	71	7	8	8	×	×	×	×	9	
13	00	1012.2	W 10	÷19.4	74	1—2	36	7	8	9	×	×	×	×	8	
	03	1010.0	W 13	÷19.0	74	0.5—1	37	3	9	9	×	×	×	×	9	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1009.6	W 11	÷18.5	..	÷22.8	78	0.5—1	36	7	9	9	×	×	×	×	8	4.3
	09	1009.6	W 12	÷18.5	80	0.2—0.5	73	7	9	9	×	×	×	×	3	
	12	1008.8	W 12	÷18.8	80	0.2—0.5	37	7	9	9	×	×	×	×	9	
	15	1006.8	W 13	÷18.5	80	0.2—0.5	73	7	9	9	×	×	×	×	9	
	18	1005.9	W 15	÷18.8	÷18.2	..	80	0.2—0.5	73	7	9	9	×	×	×	×	6	×
	21	1004.1	W 15	÷18.5	80	0.2—0.5	73	7	9	9	×	×	×	×	9	
14	00	1003.2	W 17	÷19.2	80	0.2—0.5	73	7	9	9	×	×	×	×	7	
	03	1000.7	W 21	÷19.4	80	0.2—0.5	73	7	9	9	×	×	×	×	7	
	06	999.1	W 15	÷19.6	..	÷19.7	80	0.2—0.5	37	3	9	9	×	×	×	×	8	×
	09	998.0	W 14	÷19.6	80	0.2—0.5	37	3	9	9	×	×	×	×	8	
	12	996.6	W 16	÷19.8	81	0.05—0.2	37	3	9	9	×	×	×	×	8	
	15	995.2	W 17	÷19.5	82	0.05—0.2	37	3	9	9	×	×	×	×	8	
	18	994.6	W 17	÷19.0	÷18.0	..	83	0.05—0.2	37	3	9	9	×	×	×	×	6	×
	21	994.8	W 16	÷18.0	82	0.05—0.2	37	3	9	9	×	×	×	×	4	
15	00	994.6	W 14	÷17.5	82	0.05—0.2	37	3	9	9	×	×	×	×	9	
	03	994.8	W 19	÷16.6	82	0.05—0.2	37	3	9	9	×	×	×	×	8	
	06	994.0	W 18	÷15.5	..	÷19.9	82	0.05—0.2	39	3	9	9	×	×	×	×	9	×
	09	994.6	W 17	÷14.5	82	0.05—0.2	39	3	9	9	×	×	×	×	4	
	12	996.7	W 12	÷13.8	84	0.2—0.5	39	3	9	9	×	×	×	×	4	
	15	999.4	W 10	÷14.8	80	> 50	02	2	8	8	6	5	×	×	3	
	18	1000.6	W 6	÷14.4	÷13.2	..	80	> 50	02	2	8	4	6	5	2	×	1	0.0
	21	1001.9	W 10	÷13.8	78	> 50	02	2	8	0	0	9	5	×	3	
16	00	1003.1	W 9	÷15.4	68	> 50	01	1	1	0	0	9	4	0	3	
	03	1004.7	W 6	÷16.0	68	> 50	00	0	0	0	0	9	0	0	3	
	06	1006.4	WSW 5	÷16.4	..	÷16.4	68	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1007.0	WSW 4	÷16.6	68	> 50	00	0	0	0	0	9	0	0	3	
	12	1007.3	WSW 5	÷17.0	68	> 50	00	0	0	0	0	9	0	0	3	
	15	1007.4	WSW 7	÷17.4	70	> 50	00	0	0	0	0	9	0	0	4	
	18	1007.8	WSW 6	÷16.6	÷13.4	..	70	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1007.5	WSW 8	÷17.3	70	> 50	00	0	0	0	0	9	0	0	9	
17	00	1007.4	WSW 5	÷17.3	70	> 50	00	0	0	0	0	9	0	0	6	
	03	1007.0	WSW 3	÷17.5	70	> 50	00	0	0	0	0	9	0	0	9	
	06	1007.0	WSW 5	÷17.5	..	÷17.5	70	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1006.6	WSW 2	÷18.5	62	> 50	03	2	8	0	0	9	1	×	8	
	12	1006.2	0	÷18.0	62	> 50	02	2	8	0	0	9	1	×	8	
	15	1005.9	0	÷17.5	63	> 50	01	2	4	0	0	9	4	0	8	
	18	1005.6	WSW 2	÷18.3	÷16.5	..	64	> 50	02	2	4	0	0	9	4	0	8	0.0
	21	1005.8	0	÷16.5	66	> 50	02	1	3	0	0	9	5	0	4	
18	00	1005.9	0	÷17.0	67	> 50	02	1	3	0	0	9	4	0	3	
	03	1005.6	0	÷16.0	70	> 50	03	2	8	0	0	9	2	×	9	
	06	1005.9	0	÷16.0	..	÷18.8	74	> 50	01	1	3	0	0	9	4	0	4	0.0
	09	1006.8	0	÷17.5	78	20—50	03	2	8	0	0	9	2	×	4	
	12	1007.1	W 7	÷14.3	80	20—50	02	2	8	0	0	9	2	×	1	
	15	1007.4	W 7	÷13.8	70	20—50	01	2	5	0	0	9	4	0	3	
	18	1007.7	W 5	÷15.5	÷13.6	..	72	> 50	01	0	2	0	0	9	4	0	3	0.0
	21	1007.9	W 4	÷18.0	74	> 50	00	0	0	0	0	9	0	0	3	
19	00	1007.7	WSW 1	÷19.7	74	> 50	00	0	0	0	0	9	0	0	9	
	03	1006.6	0	÷21.3	76	> 50	00	0	0	0	0	9	0	0	9	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1006.3	0	÷22.0	..	÷22.0	77	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1005.5	0	÷23.0	78	> 50	03	1	4	0	0	9	0	4	9	
	12	1005.1	0	÷23.2	79	> 50	02	2	5	0	0	9	5	2	8	
	15	1004.1	0	÷23.5	79	> 50	02	2	5	0	0	9	4	4	9	
	18	1004.1	WSW 3	÷23.2	÷15.5	..	79	> 50	03	2	8	0	0	9	5	4	3	0.0
	21	1003.5	WSW 2	÷21.7	78	> 50	02	2	8	0	0	9	5	5	9	
20	00	1003.5	WSW 2	÷21.0	77	> 50	02	2	8	0	0	9	5	5	3	
	03	1003.1	0	÷21.8	76	> 50	01	2	3	0	0	9	4	0	8	
	06	1003.1	0	÷22.0	..	÷23.7	76	> 50	02	2	3	0	0	9	4	0	3	0.0
	09	1004.1	0	÷23.0	76	> 50	01	1	1	0	0	9	4	0	4	
	12	1004.5	0	÷22.3	77	20-50	03	2	6	0	0	9	3	×	1	
	15	1005.0	0	÷23.0	80	> 50	01	1	2	0	0	9	4	2	3	
	18	1005.6	0	÷23.5	÷19.5	..	82	> 50	02	7	2	0	0	9	0	2	3	trace
	21	1005.9	0	÷23.5	82	> 50	02	0	1	0	0	9	0	2	3	
21	00	1006.3	0	÷24.3	83	> 50	00	0	0	0	0	9	0	0	3	
	03	1006.8	0	÷23.7	82	> 50	00	0	0	0	0	9	0	0	3	
	06	1007.7	0	÷24.3	..	÷24.5	80	> 50	02	0	1	0	0	9	4	0	3	0.0
	09	1008.3	0	÷24.2	79	> 50	02	0	1	0	0	9	0	2	3	
	12	1009.8	0	÷24.2	78	> 50	02	0	1	0	0	9	0	1	4	
	15	1011.3	WSW 3	÷24.0	77	> 50	02	0	1	0	0	9	4	0	3	
	18	1012.8	0	÷23.5	÷23.2	..	76	> 50	03	0	4	0	0	9	0	2	1	0.0
	21	1012.8	WSW 3	÷23.4	76	> 50	01	0	1	0	0	9	4	0	4	
22	00	1013.6	0	÷24.4	76	> 50	02	0	1	0	0	9	4	0	3	
	03	1014.4	0	÷24.2	76	> 50	00	0	0	0	0	9	0	0	3	
	06	1014.4	0	÷24.7	..	÷24.7	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1014.9	0	÷25.3	78	> 50	00	0	0	0	0	9	0	0	4	
	12	1015.0	0	÷24.7	79	> 50	00	0	0	0	0	9	0	0	3	
	15	1014.0	0	÷25.5	78	> 50	00	0	0	0	0	9	0	0	9	
	18	1014.2	0	÷25.4	÷22.7	..	76	> 50	00	0	0	0	0	9	0	0	5	0.0
	21	1013.9	0	÷25.0	76	> 50	00	0	0	0	0	9	0	0	0	
23	00	1014.0	W 5	÷21.5	70	> 50	00	0	0	0	0	9	0	0	4	
	03	1013.7	W 6	÷19.7	72	> 50	03	0	1	0	0	9	4	0	9	
	06	1013.7	W 9	÷18.6	..	÷25.7	70	> 50	03	1	3	0	0	9	4	5	3	0.0
	09	1014.7	W 9	÷16.8	69	> 50	03	2	6	0	0	9	4	6	4	
	12	1015.0	W 10	÷15.6	68	> 50	03	2	8	0	0	9	4	7	3	
	15	1015.8	W 8	÷14.4	66	> 50	02	2	8	0	0	9	4	7	3	
	18	1016.7	W 7	÷14.5	÷14.4	..	67	> 50	02	2	4	0	0	9	4	8	3	0.0
	21	1017.9	0	÷15.9	66	> 50	01	1	2	0	0	9	4	0	3	
24	00	1018.1	W 6	÷16.3	67	> 50	02	0	1	0	0	9	4	0	1	
	03	1018.8	0	÷17.8	68	> 50	00	0	0	0	0	9	0	0	3	
	06	1018.1	WSW 1	÷18.7	..	÷18.7	74	> 50	03	0	1	0	0	9	4	0	9	0.0
	09	1018.1	WSW 1	÷15.0	74	> 50	02	0	1	0	0	9	4	0	3	
	12	1018.8	WSW 2	÷15.5	76	> 50	02	0	1	0	0	9	4	0	4	
	15	1018.7	W'S 6	÷17.0	75	> 50	00	0	0	0	0	9	0	0	9	
	18	1018.9	W 8	÷15.5	÷14.5	..	74	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1019.8	W 7	÷15.6	72	> 50	00	0	0	0	0	9	0	0	4	
25	00	1020.3	W 8	÷15.5	72	> 50	00	0	0	0	0	9	0	0	3	
	03	1020.5	W 10	÷15.5	73	> 50	00	0	0	0	0	9	0	0	3	

1	2	3	4	5	6	6	8	9	10	11	12	13	14	15	16	17	18	19
	06	1021.4	W 7	÷17.0	..	÷19.0	74	> 50	02	0	1	0	0	9	4	0	4	0.0
	09	1022.0	0	÷22.0	79	> 50	02	0	1	0	0	9	4	0	3	
	12	1023.4	0	÷23.0	81	> 50	02	0	1	0	0	9	4	0	1	
	15	1024.8	E 6	÷23.0	82	> 50	02	0	1	0	0	9	0	2	3	
	18	1025.8	0	÷23.2	÷15.0	..	82	> 50	03	0	5	0	0	9	0	6	3	0.0
	21	1026.8	W 5	÷22.5	82	> 50	00	0	0	0	0	9	0	0	3	
26	00	1028.3	W 3	÷23.5	80	> 50	00	0	0	0	0	9	0	0	3	
	03	1027.0	W 4	÷20.4	78	> 50	00	0	0	0	0	9	0	0	9	
	06	1026.7	W 5	÷19.9	..	÷23.5	77	> 50	03	0	1	0	0	9	4	0	6	0.0
	09	1025.6	WSW 8	÷18.5	74	> 50	03	0	1	0	0	9	4	0	9	
	12	1024.3	WSW 10	÷18.1	74	> 50	02	0	1	0	0	9	4	0	8	
	15	1023.5	WSW 7	÷18.5	73	> 50	02	0	1	0	0	9	4	0	6	
	18	1022.8	W 5	÷17.3	÷15.4	..	72	> 50	03	0	2	0	0	9	4	0	8	0.0
	21	1022.0	W 5	÷17.2	74	> 50	01	0	1	0	0	9	4	0	8	
27	00	1021.1	W 6	÷16.6	74	> 50	00	0	0	0	0	9	0	0	8	
	03	1020.8	W 4	÷16.0	73	> 50	00	0	0	0	0	9	0	0	6	
	06	1020.8	W 6	÷16.5	..	÷20.1	72	> 50	03	0	2	0	0	9	0	5	3	0.0
	09	1021.5	W 4	÷14.6	71	> 50	03	2	8	0	0	9	2	×	4	
	12	1021.5	W 5	÷15.3	72	> 50	02	2	8	0	0	9	2	×	3	
	15	1021.5	W 2	÷14.0	73	> 50	02	2	8	0	0	9	2	×	3	
	18	1020.8	0	÷14.3	÷14.0	..	74	> 50	02	2	8	0	0	9	2	×	3	0.0
	21	1021.1	0	÷14.5	74	> 50	00	0	0	0	0	9	0	0	9	
28	00	1019.6	0	÷16.8	76	> 50	00	0	0	0	0	9	0	0	9	
	03	1017.9	W 4	÷16.4	76	> 50	00	0	0	0	0	9	0	0	8	
	06	1016.3	W 5	÷16.4	..	÷16.9	78	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1014.6	W 2	÷18.3	78	> 50	00	0	0	0	0	9	0	0	8	
	12	1013.0	0	÷18.3	78	> 50	00	0	0	0	0	9	0	0	8	
	15	1010.9	W 3	÷18.7	78	> 50	00	0	0	0	0	9	0	0	9	
	18	1009.6	0	÷19.0	÷14.4	..	78	> 50	03	0	1	0	0	9	4	0	6	0.0
	21	1008.2	W 4	÷18.7	77	> 50	02	0	1	0	0	9	4	0	8	
29	00	1008.3	0	÷19.1	78	> 50	00	0	0	0	0	9	0	0	4	
	03	1008.6	0	÷19.5	78	> 50	00	0	0	0	0	9	0	0	4	
	06	1009.5	0	÷19.3	..	÷19.5	78	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1010.6	0	÷21.5	81	> 50	00	0	0	0	0	9	0	0	3	
	12	1011.8	0	÷21.0	82	> 50	00	0	0	0	0	9	0	0	3	
	15	1012.8	0	÷22.2	82	> 50	00	0	0	0	0	9	0	0	3	
	18	1013.2	0	÷23.5	÷18.3	..	84	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1013.4	0	÷24.8	84	> 50	02	0	1	0	0	9	4	0	3	
30	00	1013.4	0	÷24.6	86	> 50	03	0	3	0	0	9	0	5	3	
	03	1014.4	SE/E 3	÷24.0	85	> 50	03	2	6	0	0	9	0	6	4	
	06	1015.1	0	÷24.8	..	÷24.8	84	> 50	01	0	1	0	0	9	4	0	3	0.0
	09	1015.5	W 3	÷24.5	86	> 50	00	0	0	0	0	9	0	0	1	
	12	1016.2	0	÷23.5	85	> 50	03	0	1	0	0	9	4	0	4	
	15	1017.6	0	÷25.6	84	> 50	03	0	2	0	0	9	5	0	4	
	18	1018.9	E 2	÷25.6	÷23.5	..	84	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1020.3	0	÷25.6	84	> 50	00	0	0	0	0	9	0	0	3	
31	00	1021.5	0	÷26.1	85	> 50	00	0	0	0	0	9	0	0	3	
	03	1022.8	E 2	÷24.0	85	10—20	03	1	8	8	5	4	×	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1023.2	0	÷23.8	..	÷26.2	85	10—20	02	2	8	8	5	4	×	×	1	0.0
	09	1024.0	0	÷23.5	85	10—20	02	2	8	8	5	4	×	×	3	
	12	1023.0	0	÷23.2	88	10—20	02	2	8	8	6	4	×	×	8	
	15	1022.8	0	÷22.8	88	20—50	02	2	8	8	6	4	×	×	8	
	18	1021.5	0	÷21.4	÷21.0	..	88	20—50	02	2	8	8	6	4	×	×	8	0.0
	21	1020.6	SE'E 3	÷21.0	88	20—50	02 ¹	2	8	8	6	4	×	×	8	
Mean		1015.3	4.2	÷19.0	÷17.0	÷20.2	71	6.3

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1019.9	S'E 4	÷21.0	88	10—20	02	2	8	8	6	4	×	×	8	
	03	1018.8	0	÷20.2	88	10—20	78	7	8	8	6	4	×	×	8	
	06	1017.3	0	÷20.4	..	÷23.8	89	10—20	02	7	8	8	6	4	×	×	8	trace
	09	1016.7	E 3	÷20.3	89	10—20	70	7	8	8	6	4	×	×	6	
	12	1016.2	0	÷20.7	88	10—20	02	7	8	8	6	5	×	×	8	
	15	1015.0	0	÷21.3	89	10—20	02	2	8	8	0	7	7	×	9	
	18	1014.3	0	÷22.0	÷20.1	..	87	10—20	02	2	8	8	0	7	7	×	6	trace
	21	1013.7	0	÷22.0	87	20—50	02	2	8	8	0	8	7	×	8	
2	00	1012.5	W 6	÷20.7	83	20—50	02	2	8	8	0	8	7	×	9	
	03	1011.2	W 8	÷21.0	80	20—50	02	2	8	8	0	8	7	×	8	
	06	1010.0	W 9	÷21.0	..	÷22.3	80	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1008.8	W 8	÷21.2	78	> 50	02	2	8	0	0	9	7	×	8	
	12	1007.9	W 6	÷21.0	77	> 50	02	2	8	8	6	4	×	×	8	
	15	1006.4	W 4	÷21.0	77	> 50	02	2	8	8	6	4	×	×	8	
	18	1005.5	W 5	÷21.0	÷20.5	..	77	10—20	77	7	8	8	6	4	×	×	8	trace
	21	1004.5	W 2	÷21.0	78	10—20	77	7	8	8	6	4	×	×	8	
3	00	1003.8	0	÷21.0	80	10—20	77	7	8	8	6	4	×	×	8	
	03	1002.8	0	÷21.0	80	10—20	77	7	8	8	6	4	×	×	8	
	06	1001.4	0	÷21.5	..	÷21.7	82	10—20	02	2	8	8	6	5	×	×	9	trace
	09	1002.0	W 1	÷21.2	82	20—50	02	2	8	8	6	6	×	×	4	
	12	1002.2	W 5	÷21.0	82	20—50	02	2	8	8	0	7	7	×	3	
	15	1003.2	W 9	÷20.7	77	20—50	02	2	8	0	0	9	7	×	4	
	18	1003.4	W 12	÷19.8	÷19.8	..	75	20—50	02	2	8	0	0	9	7	×	1	0.0
	21	1004.1	W 10	÷19.2	74	20—50	02	2	8	0	0	9	7	×	4	
4	00	1004.7	W 13	÷19.0	75	20—50	02	2	8	0	0	9	7	×	3	
	03	1005.3	W 12	÷19.3	80	2—4	02	2	8	8	6	5	×	×	3	
	06	1006.2	W 15	÷19.5	..	÷21.5	74	10—20	02	2	8	8	6	5	×	×	3	trace
	09	1007.2	W 10	÷20.0	70	> 50	00	2	0	0	0	9	0	0	3	
	12	1007.4	W 12	÷19.4	69	> 50	01	0	2	0	0	9	5	0	1	
	15	1007.6	W 9	÷18.7	70	> 50	03	2	5	0	0	9	5	0	3	
	18	1007.6	W 14	÷17.5	÷17.5	..	70	> 50	03	2	7	0	0	9	5	0	3	0.0
	21	1007.9	W 14	÷15.7	70	> 50	02	2	7	0	0	9	5	0	4	
5	00	1008.1	W 10	÷16.5	70	> 50	02	2	7	0	0	9	3	0	3	
	03	1008.4	W 10	÷16.5	70	> 50	02	2	7	0	0	9	3	0	3	
	06	1008.8	W 12	÷16.2	..	÷20.5	70	20—50	02	2	8	0	0	9	3	×	3	0.0

¹ Hoarfrost the whole 24 hours.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1010.5	W 11	÷16.4	69	20—50	02	2	8	0	0	9	3	×	4	
	12	1011.5	W 13	÷16.1	70	20—50	02	2	8	0	0	9	3	×	3	
	15	1012.7	W 13	÷15.5	69	20—50	02	2	8	0	0	9	3	×	3	
	18	1013.7	W 10	÷15.3	÷15.3	..	68	4—10	02	2	8	0	0	9	3	×	3	0.0
	21	1015.0	W 12	÷15.8	72	10—20	02	2	8	0	0	9	3	×	3	
6	00	1015.2	W 9	÷16.0	69	> 50	02	2	8	0	0	9	3	×	1	
	03	1015.2	W 7	÷16.2	72	10—20	02	2	8	0	0	9	3	×	3	
	06	1014.8	SW'W 3	÷17.0	..	÷17.1	71	> 50	02	2	7	0	0	9	3	×	9	0.0
	09	1014.9	SW'W 2	÷17.6	72	10—20	00	1	0	0	0	9	0	0	3	
	12	1015.0	W 5	÷19.0	72	> 50	00	0	0	0	0	9	0	0	3	
	15	1015.5	SW'W 3	÷20.0	74	> 50	00	0	0	0	0	9	0	0	3	
	18	1015.9	SW'W 1	÷21.0	÷15.0	..	74	> 50	03	0	1	0	0	9	5	0	3	0.0
	21	1017.0	WSW 1	÷20.2	74	> 50	03	2	8	0	0	9	3	0	4	
7	00	1017.5	0	÷19.8	74	> 50	02	2	8	0	0	9	7	×	1	
	03	1018.0	0	÷18.2	75	20—50	77	7	8	8	5	9	×	×	3	
	06	1017.8	0	÷19.0	..	÷21.0	75	10—20	02	2	8	0	0	9	3	×	9	trace
	09	1018.2	E 2	÷18.5	84	4—10	03	2	8	8	5	9	×	×	4	
	12	1017.9	E 3	÷18.2	88	4—10	02	2	8	8	5	6	×	×	9	
	15	1017.0	E 5	÷17.9	88	4—10	02	3	8	8	5	5	×	×	9	
	18	1016.3	E 6	÷17.6	÷17.3	..	88	10—20	02	2	8	8	5	6	×	×	8	0.0
	21	1016.4	E 6	÷17.6	88	4—10	70	7	8	8	5	4	×	×	4	
8	00	1015.5	E 3	÷18.7	90	2—4	02	7	8	8	5	3	×	×	9	
	03	1014.5	E 4	÷19.0	80	2—4	02	2	8	8	5	2	×	×	8	
	06	1014.3	E 2	÷19.5	..	÷19.5	92	1—2	77	7	8	8	6	2	×	×	6	trace
	09	1014.4	0	÷19.1	92	1—2	77	7	8	8	6	2	×	×	4	
	12	1014.4	W 4	÷19.6	92	1—2	77 ¹	7	8	8	6	2	×	×	3	
	15	1014.1	W 4	÷20.2	92	20—50	02	2	6	6	6	2	0	0	9	
	18	1013.5	W 5	÷20.4	÷17.6	..	92	20—50	02	2	6	6	6	2	0	0	8	trace
	21	1013.0	W 5	÷21.5	88	> 50	01	0	1	1	6	2	0	0	8	
9	00	1013.3	W 5	÷22.0	86	> 50	03	0	2	0	0	9	0	5	4	
	03	1012.3	W 3	÷21.6	82	> 50	03	0	4	0	0	9	5	0	9	
	06	1011.8	0	÷21.5	..	÷22.3	78	> 50	03	2	8	0	0	9	3	0	6	0.0
	09	1011.7	W 3	÷21.5	74	> 50	01	0	1	0	0	9	4	0	6	
	12	1011.7	0	÷22.5	74	> 50	02	0	1	0	0	9	4	0	3	
	15	1012.3	0	÷22.6	76	> 50	00	0	0	0	0	9	0	0	4	
	18	1012.4	W 1	÷22.0	÷20.5	..	76	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1013.4	0	÷23.6	73	> 50	00	0	0	0	0	9	0	0	4	
10	00	1013.8	0	÷23.2	74	> 50	00	0	0	0	0	9	0	0	1	
	03	1014.6	0	÷24.5	74	> 50	00	0	0	0	0	9	0	0	4	
	06	1014.8	0	÷25.4	..	÷25.5	74	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1015.0	0	÷24.6	76	> 50	00	0	0	0	0	9	0	0	3	
	12	1015.4	0	÷24.3	76	> 50	02	0	1	0	0	9	0	1	3	
	15	1016.2	E 3	÷24.7	76	> 50	00	0	0	0	0	9	0	0	3	
	18	1016.2	E 5	÷25.3	÷22.0	..	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1017.7	0	÷25.9	76	> 50	00	0	0	0	0	9	0	0	3	
11	00	1018.5	0	÷26.4	77	> 50	00	0	0	0	0	9	0	0	3	
	03	1019.3	0	÷26.5	77	> 50	00	0	0	0	0	9	0	0	3	
	06	1019.6	0	÷25.5	..	÷26.5	78	> 50	00	0	0	0	0	9	0	0	1	0.0

¹ 0000—1200 Hoarfrost.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1020.8	WSW 6	÷21.2	72	> 50	00	0	0	0	0	9	0	0	4	
	12	1021.5	0	÷22.0	70	> 50	00	0	0	0	0	9	0	0	3	
	15	1021.6	WSW 2	÷23.4	72	> 50	03	0	1	0	0	9	4	0	1	
	18	1021.4	WSW 2	÷24.0	÷20.2	..	76	20—50	02	0	1	0	0	9	4	0	9	0.0
	21	1022.0	WSW 1	÷24.7	78	> 50	00	0	0	0	0	9	0	0	4	
12	00	1021.8	0	÷24.9	79	> 50	03	0	1	0	0	9	4	0	9	
	03	1021.4	WSW 7	÷21.5	71	> 50	00	0	0	0	0	9	0	0	9	
	06	1021.6	WSW 6	÷22.0	..	÷25.9	74	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1022.5	W 7	÷22.6	74	> 50	00	0	0	0	0	9	0	0	3	
	12	1022.9	W 7	÷22.4	74	> 50	02	0	2	0	0	9	4	0	3	
	15	1023.3	W 6	÷23.0	73	> 50	02	2	5	0	0	9	4	5	3	
	18	1023.6	W 4	÷23.2	÷21.0	..	73	> 50	02	2	4	0	0	9	0	5	3	0.0
	21	1025.3	E 2	÷26.7	78	> 50	01	0	2	0	0	9	0	2	4	
13	00	1025.7	0	÷26.7	80	4—10	77	7	4	0	0	9	0	6	1	
	03	1026.0	0	÷26.5	78	4—10	40	7	5	0	0	9	0	6	3	
	06	1025.7	[0	÷26.7	..	÷26.7	78	4—10	71	7	5	0	0	9	0	6	9	trace
	09	1025.9	0	÷26.6	79	10—20	71	7	5	0	0	9	0	6	4	
	12	1025.1	W 6	÷24.1	75	> 50	02	7	4	0	0	9	4	6	9	
	15	1024.3	W 9	÷24.0	73	4—10	03	2	8	0	0	9	4	×	8	
	18	1024.2	W 8	÷23.4	÷23.1	..	71	10—20	01	2	7	0	0	9	4	2	6	0.0
	21	1023.8	W 8	÷23.5	70	20—50	01	2	4	0	0	9	0	2	9	
14	00	1023.9	W 6	÷24.2	72	> 50	01	0	1	0	0	9	0	2	4	
	03	1023.4	W 4	÷24.0	72	> 50	02	0	1	0	0	9	0	2	9	
	06	1023.2	W 7	÷24.7	..	÷26.7	70	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1023.6	W 5	÷24.8	72	> 50	03	0	3	0	0	9	5	0	4	
	12	1023.2	0	÷26.7	73	> 50	02	0	3	0	0	9	4	5	9	
	15	1021.4	W 4	÷24.2	76	> 50	03	2	8	0	0	9	1	×	9	
	18	1020.4	W 7	÷23.0	÷23.0	..	75	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1019.6	W 8	÷23.2	73	> 50	00	0	0	0	0	9	0	0	8	
15	00	1019.3	W 10	÷22.5	74	> 50	00	0	0	0	0	9	0	0	8	
	03	1018.3	W 10	÷22.0	72	> 50	02	2	8	0	0	9	1	×	9	
	06	1017.3	W 13	÷21.3	..	÷27.2	82	2—4	36	3	8	0	0	9	1	×	8	0.0
	09	1017.7	W 13	÷21.3	88	2—4	36	3	8	0	0	9	1	×	4	
	12	1018.2	W 12	÷21.2	88	4—10	36	3	8	0	0	9	1	×	3	
	15	1019.0	W 11	÷21.5	88	10—20	01	3	3	0	0	9	4	0	4	
	18	1019.0	W 10	÷21.5	÷21.1	..	88	20—50	01	0	1	0	0	9	4	0	3	0.0
	21	1019.1	W 12	÷21.8	86	> 50	00	0	0	0	0	9	0	0	3	
16	00	1019.3	W 7	÷22.6	83	> 50	00	0	0	0	0	9	0	0	3	
	03	1017.9	W 10	÷22.8	77	> 50	00	0	0	0	0	9	0	0	9	
	06	1016.5	W 9	÷24.0	..	÷24.0	74	> 50	02	0	2	0	0	9	5	0	8	0.0
	09	1016.3	0	÷25.6	74	> 50	02	0	2	0	0	9	5	0	6	
	12	1015.0	W 5	÷26.6	75	> 50	02	0	2	0	0	9	5	0	9	
	15	1014.1	W 2	÷27.0	76	> 50	03	0	4	0	0	9	0	6	8	
	18	1014.0	W 4	÷27.3	÷21.0	..	76	> 50	02	0	2	0	0	9	0	5	6	0.0
	21	1014.9	W 8	÷26.0	76	> 50	03	2	8	0	0	9	1	×	4	
17	00	1015.5	W 5	÷25.4	74	> 50	02	2	8	0	0	9	1	×	3	
	03	1017.2	E 5	÷27.3	78	> 50	00	0	0	0	0	9	0	0	4	
	06	1018.5	E 2	÷28.7	..	÷29.7	80	> 50	00	0	0	0	0	9	0	0	3	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1021.4	E 1	÷28.9	81	> 50	00	0	0	0	0	9	0	0	4	
	12	1022.4	E 3	÷29.7	78	> 50	00	0	0	0	0	9	0	0	1	
	15	1022.9	0	÷29.4	78	> 50	00	0	0	0	0	9	0	0	1	
	18	1023.9	0	÷29.7	÷24.7	..	78	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1025.1	0	÷30.2	78	> 50	00	0	0	0	0	9	0	0	3	
18	00	1025.0	0	÷31.0	79	> 50	00	0	0	0	0	9	0	0	1	
	03	1026.3	0	÷31.7	79	> 50	00	0	0	0	0	9	0	0	3	
	06	1027.0	0	÷31.0	..	÷32.0	80	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1028.0	0	÷31.8	80	> 50	00	0	0	0	0	9	0	0	3	
	12	1028.6	W 2	÷31.6	79	> 50	03	0	1	0	0	9	5	0	3	
	15	1029.0	0	÷32.1	80	> 50	00	0	0	0	0	9	0	0	3	
	18	1028.8	W 1	÷32.2	÷29.7	..	80	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1028.8	W 3	÷32.0	80	> 50	00	0	0	0	0	9	0	0	3	
19	00	1028.2	W 2	÷32.3	80	> 50	00	0	0	0	0	9	0	0	9	
	03	1027.6	W 4	÷32.2	80	> 50	00	0	0	0	0	9	0	0	8	
	06	1026.1	0	÷32.8	..	÷32.8	80	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1025.8	0	÷33.2	74	> 50	00	0	0	0	0	9	0	0	6	
	12	1024.6	0	÷33.1	74	> 50	00	0	0	0	0	9	0	0	9	
	15	1022.7	0	÷33.2	80	> 50	00	0	0	0	0	9	0	0	9	
	18	1022.1	0	÷34.0	÷31.8	..	82	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1020.9	0	÷34.5	88	> 50	00	0	0	0	0	9	0	0	9	
20	00	1020.6	0	÷33.7	92	> 50	00	0	0	0	0	9	0	0	6	
	03	1019.2	0	÷33.6	95	> 50	00	0	0	0	0	9	0	0	9	
	06	1018.2	0	÷33.3	..	÷34.7	93	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1018.1	W 4	÷32.5	92	> 50	00	0	0	0	0	9	0	0	6	
	12	1018.1	W 6	÷31.5	89	> 50	00	0	0	0	0	9	0	0	3	
	15	1019.6	W 7	÷30.5	86	> 50	00	0	0	0	0	9	0	0	4	
	18	1021.2	W 7	÷30.6	÷30.5	..	84	> 50	03	0	1	0	0	9	5	0	3	0.0
	21	1024.2	W 6	÷29.2	80	> 50	00	0	0	0	0	9	0	0	4	
21	00	1025.5	W 6	÷29.1	69	> 50	00	0	0	0	0	9	0	0	1	
	03	1027.1	W 5	÷29.3	68	> 50	00	0	0	0	0	9	0	0	3	
	06	1027.6	W 3	÷29.2	..	÷33.5	68	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1028.4	W 5	÷26.8	76	> 50	03	2	7	0	0	9	7	×	3	
	12	1029.1	W 5	÷28.7	73	> 50	01	0	1	0	0	9	4	0	3	
	15	1029.8	0	÷29.1	75	> 50	02	0	1	0	0	9	4	0	3	
	18	1030.3	W 2	÷30.2	÷26.0	..	76	> 50	02	0	1	0	0	9	4	0	3	0.0
	21	1030.6	0	÷30.8	78	> 50	00	0	0	0	0	9	0	0	3	
22	00	1030.3	W 2	÷31.4	80	> 50	00	0	0	0	0	9	0	0	9	
	03	1029.9	W 3	÷30.7	81	> 50	00	0	0	0	0	9	0	0	8	
	06	1030.4	W 5	÷29.8	..	÷31.4	80	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1031.0	W 2	÷31.0	80	> 50	00	0	0	0	0	9	0	0	3	
	12	1031.9	W 4	÷31.2	80	> 50	00	0	0	0	0	9	0	0	1	
	15	1032.8	W 5	÷30.2	80	> 50	03	2	8	8	6	4	×	×	3	
	18	1033.4	W 5	÷30.5	÷29.8	..	80	> 50	02	2	8	8	6	4	×	×	1	0.0
	21	1034.3	W 1	÷30.1	80	> 50	02	2	8	8	6	4	×	×	3	
23	00	1035.3	W 5	÷30.5	80	> 50	00	0	0	0	0	9	0	0	3	
	03	1036.9	0	÷32.0	80	> 50	00	0	0	0	0	9	0	0	4	
	06	1037.3	0	÷31.4	..	÷32.0	80	> 50	00	0	0	0	0	9	0	0	1	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	09	1038.7	0	÷32.3	80	> 50	00	0	0	0	0	9	0	0	4	
	12	1039.5	0	÷32.7	82	> 50	00	0	0	0	0	9	0	0	1	
	15	1039.5	W 1	÷32.0	82	> 50	03	0	1	0	0	9	4	0	3	
	18	1040.3	W 1	÷31.8	÷30.4	..	82	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1040.7	0	÷31.6	82	> 50	00	0	0	0	0	9	0	0	1	
24	00	1040.6	0	÷31.9	82	> 50	00	0	0	0	0	9	0	0	9	
	03	1040.5	0	÷32.0	82	> 50	00	0	0	0	0	9	0	0	8	
	06	1040.1	0	÷31.6	..	÷32.5	82	> 50	03	2	8	8	6	4	×	×	8	0.0
	09	1039.7	W 2	÷31.0	82	> 50	02	2	8	8	6	4	×	×	8	
	12	1038.1	W 5	÷31.0	83	> 50	01	2	4	4	6	4	0	0	9	
	15	1036.4	0	÷30.4	85	> 50	02	2	8	8	6	4	×	×	8	
	18	1034.5	0	÷30.0	÷29.0	..	88	> 50	02	2	8	8	6	4	×	×	8	0.0
	21	1031.6	0	÷29.4	89	10-20	78	7	8	8	6	4	×	×	9	
25	00	1029.3	0	÷29.1	90	10-20	78	7	8	8	6	4	×	×	8	
	03	1024.6	E 4	÷28.8	90	4-10	78	7	8	8	6	2	×	×	9	
	06	1022.6	E 1	÷27.7	..	÷32.0	92	20-50	01	7	3	0	0	9	4	0	6	trace
	09	1020.9	E 1	÷28.6	91	20-50	01	0	2	0	0	9	4	0	8	
	12	1018.8	SW 1	÷28.2	91	> 50	03	0	4	0	0	9	4	0	8	
	15	1014.7	W 3	÷28.2	91	> 50	01	0	1	0	0	9	4	0	9	
	18	1012.2	WSW 2	÷29.2	÷27.7	..	92	> 50	02	0	1	0	0	9	4	0	6	0.0
	21	1009.6	0	÷28.3	90	> 50	03	2	7	0	0	9	1	×	8	
26	00	1008.8	W 3	÷27.6	89	> 50	00	0	0	0	0	9	0	6	6	
	03	1007.7	W 2	÷27.2	88	> 50	03	0	1	0	0	9	4	0	8	
	06	1007.7	W 2	÷26.5	..	÷27.9	86	> 50	02	0	1	0	0	9	4	0	3	0.0
	09	1009.2	W 4	÷24.9	83	> 50	00	0	0	0	0	9	0	0	4	
	12	1010.6	0	÷26.4	86	> 50	00	0	0	0	0	9	0	0	3	
	15	1012.1	0	÷27.0	88	> 50	00	0	0	0	0	9	0	0	3	
	18	1013.5	E 1	÷25.4	÷24.2	..	92	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1014.0	W 3	÷25.5	94	> 50	00	0	0	0	0	9	0	0	1	
27	00	1015.5	W 3	÷22.0	94	> 50	00	0	0	0	0	9	0	0	4	
	03	1017.0	0	÷23.0	93	> 50	00	0	0	0	0	9	0	0	3	
	06	1017.0	0	÷23.0	..	÷27.4	92	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1017.4	0	÷20.2	91	> 50	00	0	0	0	0	9	0	0	4	
	12	1015.8	WSW 2	÷19.4	88	> 50	00	0	0	0	0	9	0	0	9	
	15	1013.6	0	÷19.3	89	> 50	03	2	8	0	0	9	2	×	9	
	18	1010.4	0	÷21.0	÷17.3	..	92	> 50	01	0	1	0	0	9	4	0	9	0.0
	21	1005.8	0	÷23.1	95	> 50	00	0	0	0	0	9	0	0	9	
28	00	1001.0	WSW 2	÷23.4	98	> 50	00	0	0	0	0	9	0	0	8	
	03	995.0	0	÷22.9	100	4-10	03	2	8	8	5	4	×	×	9	
	06	992.1	E 5	÷22.0	..	÷23.7	94	4-10	02 ¹	2	8	8	5	4	×	×	6	trace
	09	988.6	E 4	÷22.0	90	4-10	77	7	8	8	6	4	×	×	8	
	12	989.2	W 6	÷21.0	90	20-50	02	2	8	8	6	4	×	×	4	
	15	991.2	W 9	÷17.3	88	10-20	71	7	8	8	6	4	×	×	8	
	18	993.4	W 11	÷16.6	÷15.4	..	88	4-10	71	7	8	8	6	4	×	×	8	0.0
	21	998.4	W 15	÷17.2	90	0.5-1	39	3	9	9	×	×	×	×	4	
29	00	1002.6	W 12	÷17.3	90	0.5-1	38	3	9	9	×	×	×	×	4	
	03	1006.2	W 13	÷16.0	88	20-50	02	2	8	8	6	4	×	×	4	
	06	1010.4	W 8	÷16.4	..	÷22.0	88	20-50	02	2	8	8	6	4	×	×	3	0.0

¹ 0300-0600 Hoarfrost.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
30	09	1012.4	W 9	÷15.2	86	20—50	02	2	8	0	0	9	2	×	1	0.0
	12	1015.4	W 7	÷15.0	87	20—50	02	2	8	0	0	9	2	×	4	
	15	1018.3	E 3	÷18.3	80	> 50	00	0	0	0	0	9	0	0	3	
	18	1020.0	0	÷20.2	÷14.4	..	82	> 50	03	0	1	0	0	9	4	0	1	
	21	1021.9	SE'E 1	÷19.5	80	> 50	01	0	1	0	0	9	0	2	3	
	00	1022.6	0	÷20.3	79	> 50	00	0	0	0	0	9	0	0	1	
	03	1023.3	0	÷21.9	78	> 50	00	0	0	0	0	9	0	0	3	
	06	1023.5	0	÷22.2	..	÷22.3	78	> 50	00	0	0	0	0	9	0	0	1	
	09	1023.6	0	÷23.0	78	> 50	00	0	0	0	0	9	0	0	3	
	12	1022.7	0	÷23.5	78	> 50	00	0	0	0	0	9	0	0	9	
	15	1020.2	0	÷24.8	78	> 50	00	0	0	0	0	9	0	0	8	
	18	1018.7	0	÷25.8	÷19.1	..	78	> 50	00	0	0	0	0	9	0	0	8	
21	1018.5	0	÷25.8	78	> 50	00	0	0	0	0	9	0	0	6		
Mean	1018.2		3.8	÷24.3	÷14.4	÷44.1	79

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1017.7	W 4	÷25.0	77	> 50	03	0	1	0	0	9	5	0	9	0.0
	03	1017.1	W 6	÷23.5	75	> 50	02	0	2	0	0	9	5	0	8	
	06	1017.1	W 7	÷18.1	..	÷29.3	70	> 50	03	2	8	0	0	9	7	×	3	
2	09	1018.3	W 8	÷17.3	64	> 50	02	2	8	0	0	9	7	×	4	0.0
	12	1018.5	W 7	÷17.7	62	> 50	02	2	8	0	0	9	7	×	1	
	15	1017.6	W 5	÷19.0	62	> 50	01	0	4	0	0	9	2	0	9	
	18	1016.3	0	÷19.3	÷16.7	..	63	> 50	00	0	0	0	0	9	0	0	9	
	21	1013.9	0	÷24.8	68	> 50	00	0	0	0	0	9	0	0	9	
	00	1011.3	0	÷24.5	70	> 50	00	0	0	0	0	9	0	0	8	
	03	1007.3	0	÷24.3	70	> 50	00	0	0	0	0	9	0	0	9	
	06	1004.4	SE'E 4	÷26.5	..	÷26.7	70	> 50	00	0	0	0	0	9	0	0	8	
	09	1001.2	SE'E 3	÷27.2	71	> 50	00	0	0	0	0	9	0	0	8	
	12	998.0	0	÷28.5	73	> 50	00 ¹	0	0	0	0	9	0	0	8	
	15	996.0	0	÷29.2	74	> 50	00	0	0	0	0	9	0	0	6	
	18	994.8	0	÷29.5	÷19.0	..	74	> 50	03	0	4	0	0	9	0	6	8	
21	994.8	0	÷29.5	74	> 50	02 ²	2	8	0	0	9	0	7	3		
3	00	995.5	W 10	÷26.5	72	20—50	02	2	8	8	6	4	×	×	4	trace
	03	996.7	W 10	÷21.5	64	4—10	71	7	8	8	6	2	×	×	3	
	06	997.8	W 13	÷21.2	..	÷29.5	74	1—2	36	7	×	9	×	×	×	×	3	
4	09	1000.0	W 13	÷20.9	78	1—2	36	3	9	9	×	×	×	×	4	trace
	12	1000.7	W 13	÷21.2	80	2—4	36	3	8	0	0	9	×	×	1	
	15	1001.0	W 15	÷21.2	80	0.2—0.5	39	3	9	9	×	×	×	×	1	
	18	1001.5	W 15	÷21.4	÷19.4	..	80	0.05—0.2	39	3	9	9	×	×	×	×	3	
	21	1001.4	W 16	÷21.3	80	0.2—0.5	39	3	9	9	×	×	×	×	9	
	00	1002.1	W 15	÷21.0	80	0.05—0.2	39	3	9	9	×	×	×	×	4	
	03	1001.9	W 15	÷21.4	80	0.05—0.2	39	3	9	9	×	×	×	×	9	
	06	1002.4	W 15	÷21.0	..	÷21.5	80	0.2—0.5	39	3	9	9	×	×	×	×	4	
	09	1003.8	W 17	÷21.0	80	0.05—0.2	39	3	9	9	×	×	×	×	3	

¹ 1130 2 Paraselenae. ² 1900 Lunar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1004.6	W 13	÷20.5	79	0.2—0.5	39	3	9	9	×	×	×	×	3	
	15	1005.8	W 13	÷20.5	79	0.2—0.5	39	3	9	9	×	×	×	×	3	
	18	1006.7	W 12	÷20.5	÷20.5	..	79	20—50	02 ¹	3	8	0	0	9	0	7	3	0.0
	21	1007.9	W 12	÷20.2	79	10—20	02 ¹	3	8	0	0	9	0	7	3	
5	00	1008.9	W 12	÷20.5	79	10—20	02 ¹	2	8	0	0	9	0	7	3	
	03	1010.0	W 12	÷20.5	79	4—10	02 ¹	2	8	0	0	9	0	7	3	
	06	1011.2	W 11	÷21.0	..	÷21.2	79	2—4	36 ¹	3	8	0	0	9	0	7	3	0.0
	09	1012.6	W 12	÷20.6	79	2—4	36 ¹	3	8	0	0	9	0	7	3	
	12	1013.3	W 13	÷20.6	79	20—50	02 ¹	2	8	0	0	9	0	9	1	
	15	1014.1	W 13	÷21.0	79	> 50	02 ¹	2	8	0	0	9	0	7	3	
	18	1015.1	W 14	÷21.1	÷20.0	..	79	> 50	02 ¹	2	8	0	0	9	0	7	3	0.0
	21	1016.0	W 13	÷20.8	79	> 50	02	2	8	0	0	9	0	9	3	
6	00	1016.0	W 15	÷20.7	79	> 50	02	2	8	0	0	9	0	9	3	
	03	1016.6	W 13	÷21.3	80	> 50	02	2	8	0	0	9	0	7	4	
	06	1017.3	W 12	÷20.8	..	÷21.7	80	> 50	02 ¹	2	8	0	0	9	0	7	3	0.0
	09	1017.9	W 13	÷21.0	80	> 50	02 ¹	2	8	0	0	9	0	7	3	
	12	1018.0	W 12	÷21.4	80	> 50	02 ¹	2	8	0	0	9	0	7	1	
	15	1017.7	W 11	÷21.2	80	> 50	02 ¹	2	8	0	0	9	0	7	9	
	18	1017.7	W 14	÷21.0	÷20.5	..	80	> 50	02 ¹	2	8	0	0	9	0	7	3	0.0
	21	1017.5	W 12	÷21.4	80	> 50	02 ¹	2	8	0	0	9	0	7	9	
7	00	1018.0	W 12	÷22.0	80	> 50	03	0	3	0	0	9	0	5	4	
	03	1018.9	W 12	÷21.5	80	> 50	02 ¹	0	8	0	0	9	0	2	3	
	06	1018.2	W 10	÷21.9	..	÷22.0	80	> 50	01	2	4	0	0	9	0	2	9	0.0
	09	1018.4	W 10	÷22.2	80	> 50	01	0	3	0	0	9	0	2	4	
	12	1018.3	W 12	÷22.7	80	> 50	01	0	1	0	0	9	4	2	9	
	15	1018.1	W 11	÷23.2	80	> 50	02	0	1	0	0	9	4	0	9	
	18	1018.0	W 10	÷23.1	÷21.1	..	80	> 50	02	0	1	0	0	9	4	0	8	0.0
	21	1019.0	W 7	÷23.5	70	> 50	00	0	0	0	0	9	0	0	4	
8	00	1019.4	W 12	÷23.3	70	> 50	00	0	0	0	0	9	0	0	1	
	03	1019.7	W 8	÷24.3	60	> 50	00	0	0	0	0	9	0	0	3	
	06	1019.9	W 6	÷24.2	..	÷24.4	62	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1020.0	W 7	÷24.5	62	> 50	00	0	0	0	0	9	0	0	3	
	12	1020.0	W 2	÷25.0	62	> 50	00	0	0	0	0	9	0	0	3	
	15	1019.6	W 4	÷25.7	62	> 50	00	0	0	0	0	9	0	0	9	
	18	1019.6	0	÷27.1	÷22.9	..	63	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1019.3	W 2	÷28.2	66	> 50	00	0	0	0	0	9	0	0	9	
9	00	1018.7	0	÷29.2	68	> 50	00	0	0	0	0	9	0	0	8	
	03	1017.6	0	÷29.6	70	> 50	00	0	0	0	0	9	0	0	9	
	06	1016.6	WSW 2	÷29.3	..	÷31.2	72	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1015.9	0	÷29.3	72	> 50	03	0	1	0	0	9	0	1	8	
	12	1015.5	0	÷29.7	74	> 50	02	0	1	0	0	9	0	1	6	
	15	1014.8	W 1	÷30.3	75	> 50	00	0	0	0	0	9	0	0	9	
	18	1014.6	W 2	÷29.6	÷27.0	..	76	> 50	03	2	5	0	0	9	0	2	6	0.0
	21	1014.9	W 2	÷28.8	78	> 50	00	0	0	0	0	9	0	0	4	
10	00	1014.7	W 1	÷29.2	78	> 50	00	0	0	0	0	9	0	0	9	
	03	1015.4	W 4	÷25.7	80	> 50	03	2	8	0	0	9	3	×	4	
	06	1015.9	0	÷25.0	..	÷30.6	80	> 50	77	7	8	4	6	5	2	×	3	trace
	09	1017.3	E 6	÷27.0	88	> 50	77	7	8	4	6	5	2	×	4	

¹ Lunar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1016.6	E 6	÷25.8	85	> 50	77	7	8	4	6	5	2	×	9	
	15	1015.6	0	÷26.2	85	> 50	02	2	8	0	0	9	7	×	8	
	18	1015.2	0	÷26.0	÷24.7	..	86	> 50	02	2	8	0	0	9	7	×	6	trace
	21	1014.1	0	÷28.2	88	> 50	01	2	1	0	0	9	4	0	9	
11	00	1014.0	0	÷29.4	91	> 50	00	0	0	0	0	9	0	0	6	
	03	1012.2	WSW 3	÷20.2	92	> 50	02	0	3	0	0	9	0	2	9	
	06	1011.5	0	÷30.8	..	÷31.1	90	> 50	02	0	4	0	0	9	0	2	6	0.0
	09	1010.4	0	÷30.9	91	> 50	02	2	8	0	0	9	0	7	8	
	12	1009.9	0	÷29.8	91	> 50	02	2	8	0	0	9	0	7	6	
	15	1009.1	0	÷28.9	91	> 50	02	2	8	0	0	9	3	7	8	
	18	1009.8	WSW 3	÷28.3	÷26.0	..	91	> 50	02	2	8	0	0	9	3	×	4	0.0
	21	1011.0	0	÷27.0	90	> 50	02	2	8	0	0	9	3	×	4	
12	00	1011.8	0	÷26.3	90	> 50	02	2	8	0	0	9	7	×	3	
	03	1013.0	W 5	÷24.7	85	> 50	02	2	8	0	0	9	7	×	3	
	06	1013.8	0	÷24.8	..	÷31.0	83	> 50	02	2	8	0	0	9	1	×	3	0.0
	09	1015.5	W 4	÷25.5	84	> 50	01	2	1	0	0	9	0	5	4	
	12	1016.6	W 1	÷26.7	86	> 50	00	0	0	0	0	9	0	0	1	
	15	1017.1	WSW 4	÷26.2	86	> 50	03	2	8	0	0	9	7	×	3	
	18	1017.5	WSW 4	÷24.7	÷24.2	..	86	20—50	71	7	8	8	7	5	×	×	3	trace
	21	1018.2	W 5	÷24.0	89	20—50	71	7	8	8	7	5	×	×	3	
13	00	1018.9	W 2	÷24.0	90	20—50	71	7	8	8	7	5	×	×	3	
	03	1018.9	0	÷23.5	90	20—50	71	7	8	8	7	5	×	×	3	
	06	1018.8	0	÷23.8	..	÷27.1	90	20—50	02	2	8	0	0	9	2	×	3	trace
	09	1018.6	0	÷24.7	90	> 50	01	2	5	0	0	9	3	0	9	
	12	1018.4	0	÷23.5	92	20—50	03	2	8	0	0	9	3	×	8	
	15	1016.8	WSW 4	÷23.8	92	20—50	02	2	8	0	0	9	7	×	9	
	18	1015.5	W 3	÷22.2	÷22.2	..	92	20—50	02	2	8	0	0	9	2	×	8	trace
	21	1014.0	W 5	÷22.1	92	20—50	02	2	8	0	0	9	2	×	8	
14	00	1012.8	W 5	÷21.7	92	4—10	70	7	8	0	0	9	7	×	4	
	03	1010.5	W 5	÷20.2	96	4—10	70	7	8	0	0	9	7	×	9	
	06	1010.5	W 5	÷20.5	..	÷24.9	96	1—2	71	7	8	8	7	4	×	×	8	trace
	09	1009.4	W 3	÷19.6	96	4—10	71	7	8	8	7	4	×	×	6	
	12	1009.0	0	÷21.4	93	> 50	00	0	0	0	0	9	0	0	3	
	15	1009.0	W 3	÷22.9	94	> 50	00	0	0	0	0	9	0	0	9	
	18	1008.5	W 3	÷24.2	÷19.1	..	92	> 50	00	0	0	0	0	9	0	0	8	trace
	21	1007.4	W 4	÷23.0	86	> 50	00	0	0	0	0	9	0	0	8	
15	00	1005.9	W 6	÷23.0	84	> 50	00	0	0	0	0	9	0	0	9	
	03	1004.3	W 7	÷21.5	84	20—50	02	2	8	8	6	4	×	×	8	
	06	1003.8	W 7	÷19.0	..	÷25.4	86	10—20	71	7	8	8	7	4	×	×	8	trace
	09	1001.2	W 6	÷18.8	92	0.05—0.2	73	7	8	8	7	4	×	×	9	
	12	1000.1	W 7	÷18.3	92	0.2—0.5	73	7	8	8	7	4	×	×	8	
	15	999.3	W 7	÷19.0	92	> 50	01	7	1	0	0	9	4	×	8	
	18	999.8	W 1	÷18.6	÷17.2	..	90	20—50	71	7	8	8	7	4	×	×	4	trace
	21	1000.8	W 3	÷18.4	92	10—20	71	7	8	8	7	4	×	×	3	
16	00	1002.0	0	÷18.0	91	4—10	71	7	8	8	7	4	×	×	4	
	03	1003.1	0	÷19.0	94	1—2	71	7	8	8	7	4	×	×	3	
	06	1003.3	W 2	÷17.1	..	÷19.4	93	1—2	71	7	8	8	7	4	×	×	1	trace
	09	1003.4	W 6	÷15.9	92	1—2	71	7	8	8	7	4	×	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1002.4	W 7	÷15.4	88	1—2	71	7	8	8	7	4	×	×	9	
	15	1000.8	W 7	÷14.3	88	1—2	71	7	8	8	7	4	×	×	8	
	18	999.7	W 6	÷13.2	÷13.0	..	90	1—2	36	7	8	8	7	4	×	×	8	trace
	21	1001.5	E 2	÷13.8	90	1—2	71	7	8	8	7	4	×	×	4	
17	00	1002.3	E 8	÷12.5	90	1—2	71	7	8	8	7	4	×	×	1	
	03	1003.3	E 3	÷13.3	86	2—4	71	7	8	8	7	4	×	×	3	
	06	1004.3	0	÷20.1	..	÷20.4	88	4—10	01	7	1	1	7	4	0	0	3	0.1
	09	1005.9	0	÷22.6	86	4—10	02	0	1	1	7	4	0	0	4	
	12	1007.0	W 3	÷20.4	85	4—10	03	2	8	8	7	5	×	×	3	
	15	1007.8	W 7	÷17.3	85	10—20	02	2	8	8	7	6	×	×	3	
	18	1008.6	W 7	÷16.6	÷12.4	..	81	10—20	71	7	8	8	7	4	×	×	3	trace
	21	1009.1	W 7	÷15.6	81	10—20	71	7	8	8	7	4	×	×	3	
18	00	1008.8	W 10	÷14.8	81	10—20	71	7	8	8	7	4	×	×	9	
	03	1008.4	W 11	÷14.9	82	10—20	71	7	8	8	7	4	×	×	8	
	06	1008.7	W 10	÷15.0	..	÷22.9	84	10—20	71	7	8	8	7	4	×	×	4	trace
	09	1009.1	W 12	÷15.3	84	10—20	02	7	8	8	7	4	×	×	3	
	12	1011.2	W 12	÷15.8	85	1—2	71	7	8	8	7	4	×	×	4	
	15	1012.0	W 11	÷16.0	84	10—20	71	7	8	8	7	4	×	×	1	
	18	1011.4	W 13	÷16.7	÷14.0	..	82	1—2	71	7	8	8	7	4	×	×	9	trace
	21	1011.0	W 14	÷16.2	84	1—2	71	7	8	8	7	4	×	×	6	
19	00	1010.0	W 13	÷16.5	84	1—2	71	7	8	8	7	4	×	×	9	
	03	1009.4	W 12	÷17.0	84	1—2	71	7	8	8	7	4	×	×	6	
	06	1008.7	W 13	÷17.5	..	÷17.5	82	4—10	36	7	4	4	7	4	0	0	8	trace
	09	1008.8	W 11	÷18.5	80	10—20	36	3	0	0	0	9	0	0	4	
	12	1008.7	W 12	÷18.7	78	10—20	36	3	0	0	0	9	0	0	9	
	15	1009.3	W 9	÷19.0	74	20—50	00	0	0	0	0	9	0	0	4	
	18	1010.3	W 9	÷19.0	÷15.9	..	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1012.1	W 5	÷19.0	72	> 50	02	0	2	0	0	9	5	0	3	
20	00	1013.9	0	÷22.8	71	> 50	00	0	0	0	0	9	0	0	3	
	03	1015.9	SE'E 5	÷23.5	72	> 50	00	0	0	0	0	9	0	0	3	
	06	1017.0	0	÷26.0	..	÷26.0	72	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1018.8	0	÷26.8	74	> 50	00	0	0	0	0	9	0	0	3	
	12	1019.7	0	÷27.4	74	> 50	00	0	0	0	0	9	0	0	1	
	15	1020.1	W 4	÷25.2	74	> 50	02	2	8	0	0	9	2	×	3	
	18	1019.3	W 8	÷24.0	÷19.0	..	72	> 50	02	2	8	0	0	9	2	×	9	0.0
	21	1019.6	W 7	÷22.3	72	> 50	02	2	8	0	0	9	2	×	4	
21	00	1018.7	W 11	÷19.6	74	> 50	02	2	8	0	0	9	2	×	9	
	03	1017.5	W 11	÷18.0	68	> 50	36	3	8	0	0	9	2	×	9	
	06	1017.4	W 10	÷17.7	..	÷29.2	66	> 50	02	2	8	0	0	9	2	×	6	0.0
	09	1016.8	W 13	÷18.0	66	10—20	01	2	7	0	0	9	2	×	9	
	12	1015.9	W 15	÷17.7	60	20—50	02	2	8	0	0	9	2	×	8	
	15	1015.5	W 14	÷17.3	57	20—50	02	2	8	0	0	9	2	×	6	
	18	1015.0	W 10	÷16.8	÷17.1	..	57	> 50	02	2	8	0	0	9	2	×	8	0.0
	21	1015.4	W 13	÷16.8	70	20—50	02	2	8	0	0	9	2	×	4	
22	00	1015.4	W 12	÷16.5	75	20—50	02	2	8	0	0	9	2	×	3	
	03	1015.4	W 12	÷16.8	76	20—50	02	2	8	8	6	4	×	×	3	
	06	1015.6	W 12	÷17.0	..	÷18.1	74	20—50	02	2	8	8	6	4	×	×	4	0.0
	09	1016.3	W 12	÷17.0	72	20—50	02	2	8	8	6	4	×	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1016.8	W 6	÷17.8	70	20—50	02	2	8	8	6	4	×	×	3	
	15	1016.6	W 2	÷19.0	70	> 50	01	2	2	0	0	9	4	0	9	
	18	1016.3	0	÷20.3	÷16.5	..	71	> 50	03	2	4	4	6	5	×	×	8	0.0
	21	1015.4	W 2	÷21.2	72	> 50	03	2	8	8	6	5	×	×	9	
23	00	1014.7	W 3	÷21.3	76	> 50	02	2	8	8	6	4	×	×	8	
	03	1013.8	0	÷20.6	76	> 50	02	2	8	8	6	3	×	×	8	
	06	1012.7	W 4	÷20.4	..	÷21.5	78	20—50	02	2	8	8	6	3	×	×	8	0.0
	09	1012.6	W 8	÷23.0	81	> 50	01	0	1	1	6	4	0	0	6	
	12	1011.9	W 5	÷24.3	78	> 50	00	0	0	0	0	9	0	0	9	
	15	1011.8	W 3	÷24.2	74	> 50	00	0	0	0	0	9	0	0	6	
	18	1011.8	W 4	÷24.5	÷20.1	..	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1012.0	0	÷25.7	72	> 50	00	0	0	0	0	9	0	0	4	
24	00	1012.1	0	÷25.5	72	> 50	00	0	0	0	0	9	0	0	3	
	03	1013.1	0	÷27.6	72	> 50	00	0	0	0	0	9	0	0	4	
	06	1013.4	0	÷28.7	..	÷29.1	74	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1014.3	0	÷28.8	75	> 50	00	0	0	0	0	9	0	0	4	
	12	1014.6	0	÷29.6	76	> 50	00	0	0	0	0	9	0	0	1	
	15	1014.0	0	÷30.5	76	> 50	00	0	0	0	0	9	0	0	9	
	18	1013.2	0	÷31.0	÷24.5	..	76	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1011.8	0	÷31.6	77	> 50	00	0	0	0	0	9	0	0	9	
25	00	1010.7	0	÷32.2	77	> 50	00	0	0	0	0	9	0	0	8	
	03	1009.2	0	÷31.3	76	> 50	00	0	0	0	0	9	0	0	8	
	06	1008.2	0	÷30.0	..	÷33.2	75	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1007.6	W 5	÷28.0	72	> 50	00	0	0	0	0	9	0	0	8	
	12	1008.2	0	÷28.4	72	> 50	00	0	0	0	0	9	0	0	4	
	15	1009.8	E 4	÷30.5	74	> 50	00	0	0	0	0	9	0	0	3	
	18	1010.5	E 6	÷30.5	÷28.0	..	75	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1011.2	0	÷32.0	78	> 50	00	0	0	0	0	9	0	0	4	
26	00	1011.0	W 4	÷31.5	78	> 50	00	0	0	0	0	9	0	0	9	
	03	1010.1	W 6	÷30.5	76	> 50	00	0	0	0	0	9	0	0	3	
	06	1010.4	W 8	÷29.0	..	÷33.7	74	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1012.0	W 2	÷29.3	74	> 50	00	0	0	0	0	9	0	0	4	
	12	1012.2	W 5	÷29.1	72	> 50	00	0	0	0	0	9	0	0	1	
	15	1012.7	0	÷28.4	72	> 50	00	0	0	0	0	9	0	0	4	
	18	1014.0	0	÷31.2	÷27.2	..	75	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1014.8	0	÷31.1	76	> 50	02	0	1	0	0	9	4	0	3	
27	00	1015.0	W 2	÷30.4	76	> 50	02	0	1	0	0	9	4	0	1	
	03	1015.3	0	÷29.3	75	> 50	00	0	0	0	0	9	0	0	3	
	06	1015.7	0	÷30.5	..	÷31.3	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1016.9	0	÷30.2	76	> 50	00	0	0	0	0	9	0	0	4	
	12	1017.4	0	÷29.0	76	> 50	00	0	0	0	0	9	0	0	1	
	15	1018.0	0	÷30.0	77	> 50	00	0	0	0	0	9	0	0	3	
	18	1018.3	0	÷31.0	÷27.0	..	77	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1019.2	0	÷30.5	78	> 50	03	2	8	0	0	9	3	×	4	
28	00	1019.6	0	÷28.0	78	> 50	02	2	8	0	0	9	7	×	3	
	03	1020.4	0	÷26.2	77	> 50	02	2	8	0	0	9	7	×	3	
	06	1020.3	W 6	÷25.7	..	÷31.5	76	> 50	02	2	8	0	0	9	7	×	9	0.0
	09	1021.3	W 4	÷24.5	75	20—50	02	2	8	0	0	9	7	×	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	12	1022.1	W 2	÷24.3	75	10—20	70	7	8	0	0	9	7	×	3	
	15	1022.4	W 3	÷24.5	76	4—10	71	7	8	0	0	9	7	×	1	
	18	1022.8	W 4	÷24.7	÷24.1	..	77	4—10	71	7	8	8	7	4	×	×	3	trace
	21	1023.0	W 4	÷25.0	78	4—10	02	7	8	0	0	9	3	×	3	
29	00	1022.7	W 3	÷25.5	76	10—20	02	2	8	0	0	9	3	×	9	
	03	1022.8	W 4	÷24.8	76	10—20	02	2	8	0	0	9	3	×	4	
	06	1022.3	W 4	÷23.8	..	÷25.8	76	10—20	02	2	8	0	0	9	7	×	8	trace
	09	1022.4	W 3	÷22.5	76	10—20	02	2	8	0	0	9	7	×	4	
	12	1022.1	W 1	÷22.4	74	20—50	02 ¹	2	8	0	0	9	7	×	9	
	15	1021.6	W 8	÷21.5	72	> 50	02	2	3	0	0	9	4	0	8	
	18	1021.5	W 9	÷21.0	÷20.9	..	72	> 50	02	2	4	0	0	9	5	0	6	0.0
	21	1021.9	W 7	÷21.0	72	> 50	02	2	4	0	0	9	5	0	4	
30	00	1022.6	W 8	÷22.0	66	> 50	00	0	0	0	0	9	0	0	3	
	03	1023.8	W 4	÷23.5	65	> 50	00	0	0	0	0	9	0	0	4	
	06	1024.8	0	÷24.5	..	÷24.5	66	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1027.0	0	÷25.6	70	> 50	00	0	0	0	0	9	0	0	4	
	12	1028.5	0	÷27.0	70	> 50	00	0	0	0	0	9	0	0	3	
	15	1030.3	0	÷28.8	72	> 50	00	0	0	0	0	9	0	0	3	
	18	1031.8	0	÷30.0	÷20.4	..	74	> 50	02	0	1	0	0	9	4	0	3	0.0
	21	1033.8	0	÷29.3	74	> 50	03 ²	2	8	0	0	9	0	7	3	
31	00	1034.5	W 5	÷28.1	72	> 50	01	0	2	0	0	9	0	7	1	
	03	1035.5	W 2	÷26.5	72	20—50	03	2	8	0	0	9	7	×	3	
	06	1035.5	W 4	÷26.0	..	÷31.2	72	20—50	02	2	8	0	0	9	7	×	3	0.0
	09	1034.8	W 6	÷25.1	72	2—4	71	7	8	8	7	4	×	×	9	
	12	1034.3	W 7	÷24.8	74	2—4	71	7	8	8	7	4	×	×	8	
	15	1032.4	W 8	÷23.0	77	2—4	71	7	8	8	7	4	×	×	9	
	18	1030.5	W 6	÷22.4	÷22.4	..	78	2—4	71	7	8	8	7	4	×	×	8	trace
	21	1029.2	W 6	÷22.5	77	> 50	02	2	3	0	0	9	4	0	8	
Mean		1013.7		5.4	÷23.4	÷20.7	÷26.0	78	0.2

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1027.9	W 7	÷25.0	67	> 50	00	0	0	0	0	9	0	0	8	
	03	1026.4	W 2	÷28.0	64	> 50	00	0	0	0	0	9	0	0	8	
	06	1025.4	0	÷29.9	..	÷30.0	67	> 50	03	2	8	0	0	9	0	9	8	0.0
	09	1024.2	0	÷29.5	72	> 50	02	2	8	0	0	9	2	×	8	
	12	1023.9	WSW 2	÷29.3	72	20—50	02	2	8	0	0	9	2	×	6	
	15	1025.4	W 8	÷28.0	71	10—20	02	2	8	0	0	9	2	×	4	
	18	1027.9	W 14	÷25.8	÷22.1	..	75	2—4	38	3	8	0	0	9	2	×	4	0.0
	21	1030.3	W 7	÷26.8	70	4—10	36	3	2	0	0	9	4	0	3	
2	00	1030.7	W 8	÷27.5	67	> 50	36	3	0	0	0	9	0	0	1	
	03	1030.5	W 3	÷29.9	65	> 50	00	0	0	0	0	9	0	0	9	
	06	1029.2	0	÷31.5	..	÷31.9	62	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1027.9	W 3	÷32.4	70	> 50	00	0	0	0	0	9	0	0	8	
	12	1027.7	W 4	÷32.6	70	> 50	00	0	0	0	0	9	0	0	6	

¹ Corona. ² Lunar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1027.3	W 1	÷33.2	73	> 50	00	0	0	0	0	9	0	0	8	
	18	1027.4	W 4	÷33.2	÷25.8	..	72	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1027.1	0	÷33.2	70	> 50	02	0	3	0	0	9	5	0	9	
3	00	1027.4	W 4	÷32.6	70	> 50	00	0	0	0	0	9	0	0	4	
	03	1027.2	0	÷33.3	71	> 50	00	0	0	0	0	9	0	0	9	
	06	1025.9	W 5	÷32.5	..	÷34.8	71	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1026.2	W 3	÷32.2	69	> 50	02	0	1	0	0	9	0	1	4	
	12	1025.3	W 5	÷32.0	68	> 50	03	1	4	0	0	9	0	2	7	
	15	1024.7	0	÷31.8	70	> 50	03	2	8	0	0	9	0	2	8	
	18	1023.7	0	÷33.6	÷31.6	..	72	> 50	02 ¹	2	8	0	0	9	0	7	9	0.0
	21	1022.3	0	÷34.0	74	> 50	01	0	2	0	0	9	0	2	9	
4	00	1020.5	0	÷33.0	76	> 50	02	0	1	0	0	9	0	2	9	
	03	1018.5	0	÷33.2	76	> 50	03	0	3	0	0	9	4	2	9	
	06	1016.8	0	÷33.6	..	÷34.9	76	> 50	03 ¹	2	8	0	0	9	0	7	8	0.0
	09	1014.6	0	÷33.2	76	> 50	02 ¹	2	8	0	0	9	0	7	9	
	12	1013.1	0	÷32.6	76	> 50	01	0	1	0	0	9	5	0	8	
	15	1010.9	0	÷32.6	76	> 50	00	0	0	0	0	9	0	0	8	
	18	1010.2	W 2	÷30.5	÷30.2	..	74	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1009.5	W 5	÷27.8	73	> 50	00	0	0	0	0	9	0	0	8	
5	00	1009.9	W 4	÷29.2	73	> 50	03	0	3	0	0	9	5	0	4	
	03	1010.1	0	÷29.1	73	> 50	00	0	0	0	0	9	0	0	3	
	06	1009.7	W 1	÷25.9	..	÷34.0	74	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1009.2	NW W4	÷29.4	73	> 50	03	2	6	0	0	9	0	7	8	
	12	1007.7	W 4	÷26.6	74	> 50	02	2	7	0	0	9	0	7	9	
	15	1006.6	W 4	÷26.5	74	> 50	00	0	0	0	0	9	0	0	8	
	18	1006.7	W 3	÷32.7	÷23.2	..	75	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1006.5	0	÷32.2	75	> 50	02	0	1	0	0	9	4	0	9	
6	00	1007.0	W 2	÷31.1	76	> 50	02	0	1	0	0	9	4	0	4	
	03	1007.2	0	÷31.3	76	> 50	00	0	0	0	0	9	0	0	3	
	06	1007.7	0	÷32.5	..	÷32.7	76	> 50	03	0	3	0	0	9	5	0	3	0.0
	09	1009.3	0	÷33.6	76	> 50	03 ¹	0	3	0	0	9	0	5	4	
	12	1010.5	W 1	÷32.8	76	> 50	02 ¹	2	8	0	0	9	0	7	3	
	15	1013.0	W 2	÷31.8	76	> 50	01	0	3	0	0	9	0	2	4	
	18	1014.6	0	÷31.2	÷29.0	..	73	> 50	03	2	5	0	0	9	5	0	1	0.0
	21	1015.6	0	÷31.5	74	> 50	02	2	5	0	0	9	5	0	3	
7	00	1016.0	0	÷33.8	74	> 50	02	2	4	0	0	9	5	0	1	
	03	1015.7	0	÷33.0	75	> 50	01	0	2	0	0	9	0	2	9	
	06	1013.6	0	÷32.8	..	÷33.8	75	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1011.8	W 5	÷32.5	75	> 50	03	2	5	0	0	9	0	6	8	
	12	1009.8	W 7	÷30.5	74	> 50	03	2	8	0	0	9	0	7	8	
	15	1009.2	W 5	÷29.3	73	> 50	01	0	2	0	0	9	0	2	6	
	18	1008.6	W 6	÷29.1	÷29.1	..	72	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1009.9	W 1	÷30.5	72	> 50	00	0	0	0	0	9	0	0	4	
8	00	1010.8	W 3	÷29.3	72	> 50	03	0	4	0	0	9	0	9	3	
	03	1011.6	W 6	÷27.8	71	> 50	02	2	4	0	0	9	0	9	3	
	06	1013.0	0	÷29.0	..	÷33.6	71	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1015.6	W 2	÷27.5	71	> 50	03	0	1	0	0	9	5	0	4	
	12	1016.3	W 4	÷29.4	72	> 50	02	0	2	0	0	9	5	0	1	

¹ Lunar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1017.0	0	÷28.5	72	> 50	03	0	8	0	0	9	5	0	3	
	18	1015.9	0	÷29.0	÷25.1	..	73	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1015.0	0	÷28.2	75	> 50	03	2	8	0	0	9	1	×	8	
9	00	1013.7	W 5	÷29.5	75	> 50	02	2	8	0	0	9	7	×	8	
	03	1012.3	W 6	÷26.0	74	> 50	02	2	8	0	0	9	7	×	8	
	06	1009.7	W 4	÷25.8	..	÷30.2	72	> 50	02	2	8	0	0	9	3	×	9	0.0
	09	1007.7	W 3	÷27.0	71	> 50	01	0	2	0	0	9	4	0	8	
	12	1006.3	W 3	÷24.5	72	> 50	03	2	8	0	0	9	3	×	6	
	15	1004.7	W 7	÷25.5	71	> 50	01	0	1	0	0	9	4	0	8	
	18	1003.6	W 7	÷24.7	÷24.3	..	72	> 50	02	0	1	0	0	9	4	0	8	0.0
	21	1004.5	W 4	÷25.6	72	> 50	00	0	0	0	0	9	0	0	4	
10	00	1003.9	W 2	÷27.7	72	> 50	00	0	0	0	0	9	0	0	9	
	03	1005.4	W 6	÷24.1	71	> 50	00	0	0	0	0	9	0	0	4	
	06	1007.0	W 7	÷25.0	..	÷27.6	71	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1009.6	ESE 3	÷24.7	72	> 50	00	0	0	0	0	9	0	0	4	
	12	1011.2	0	÷27.5	74	> 50	03	0	2	0	0	9	5	0	1	
	15	1011.1	E'N 7	÷28.0	76	20—50	03	2	8	8	6	5	×	×	9	
	18	1010.4	E 6	÷27.7	÷23.7	..	76	20—50	02	2	8	8	6	5	×	×	8	0.0
	21	1008.2	E 6	÷27.5	76	20—50	02	2	8	8	6	5	×	×	9	
11	00	1006.4	0	÷28.3	77	> 50	00	0	0	0	0	9	0	0	8	
	03	1004.5	W 5	÷29.5	78	> 50	00	0	0	0	0	9	0	0	8	
	06	1003.4	W 2	÷28.5	..	÷30.0	77	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1002.4	W 10	÷26.1	76	> 50	00	0	0	0	0	9	0	0	8	
	12	1003.1	W 10	÷23.2	75	> 50	00	0	0	0	0	9	0	0	4	
	15	1004.1	W 10	÷22.0	74	> 50	03	0	2	0	0	9	4	0	3	
	18	1005.7	E 5	÷27.7	÷20.9	..	74	> 50	02	0	2	0	0	9	4	0	4	0.0
	21	1007.7	E 5	÷29.3	75	> 50	00	0	0	0	0	9	0	0	3	
12	00	1008.0	E 3	÷29.6	76	> 50	00	0	0	0	0	9	0	0	1	
	03	1008.4	0	÷32.0	76	> 50	00	0	0	0	0	9	0	0	3	
	06	1008.8	0	÷32.0	..	÷32.0	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1010.3	0	÷32.6	77	> 50	00	0	0	0	0	9	0	0	4	
	12	1011.6	W 4	÷30.2	78	> 50	00	0	0	0	0	9	0	0	3	
	15	1013.0	W 9	÷18.0	69	> 50	02	2	8	8	6	5	×	×	3	
	18	1014.7	W 7	÷17.0	÷15.2	..	68	> 50	02	2	8	8	6	5	×	×	3	0.0
	21	1015.2	W 8	÷17.9	66	> 50	01	2	3	3	6	5	0	0	1	
13	00	1015.9	E 7	÷16.5	70	> 50	02	0	1	0	0	9	5	0	3	
	03	1015.8	E 3	÷28.9	72	> 50	00	0	0	0	0	9	0	0	9	
	06	1015.5	0	÷28.2	..	÷33.1	77	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1015.3	0	÷29.5	77	> 50	00	0	0	0	0	9	0	0	8	
	12	1015.4	0	÷29.1	78	> 50	00	0	0	0	0	9	0	0	4	
	15	1016.4	W 7	÷29.6	74	> 50	03	0	1	0	0	9	4	0	4	
	18	1018.6	0	÷24.5	÷17.0	..	68	> 50	03	2	7	0	0	9	2	×	4	0.0
	21	1020.4	W 8	÷22.3	64	20—50	02	2	8	0	0	9	2	×	3	
14	00	1021.6	W 7	÷22.4	70	10—20	71	7	8	8	7	5	×	×	3	
	03	1022.7	E 5	÷26.3	70	> 50	01	7	1	0	0	9	4	0	3	
	06	1024.0	E 2	÷27.5	..	÷30.1	73	> 50	02	0	1	0	0	9	4	0	3	
	09	1022.3	E 5	÷27.0	69	> 50	00	0	0	0	0	9	0	0	9	trace
	12	1021.6	0	÷29.0	69	> 50	00	0	0	0	0	9	0	0	6	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	15	1020.7	0	÷31.7	73	> 50	00	0	0	0	0	9	0	0	8	
	18	1020.5	0	÷32.8	÷21.6	..	74	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1020.1	0	÷32.5	75	20-50	78	0	8	8	6	5	×	×	8	
15	00	1019.8	W 3	÷32.2	76	10-20	71	7	8	8	7	4	×	×	8	
	03	1019.7	W 1	÷32.6	76	10-20	71	7	8	8	7	4	×	×	8	
	06	1019.9	0	÷32.1	..	÷33.2	75	10-20	02	7	8	8	7	5	×	×	4	trace
	09	1020.5	W 3	÷33.6	74	> 50	00	0	0	0	0	9	0	0	4	
	12	1021.0	0	÷34.7	73	> 50	00	0	0	0	0	9	0	0	3	
	15	1022.0	0	÷35.4	72	> 50	00	0	0	0	0	9	0	0	4	
	18	1023.0	0	÷34.8	÷32.0	..	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1023.7	0	÷35.2	72	> 50	00	0	0	0	0	9	0	0	3	
16	00	1023.6	W 3	÷34.8	71	> 50	00	0	0	0	0	9	0	0	9	
	03	1023.0	0	÷36.0	71	> 50	00	0	0	0	0	9	0	0	9	
	06	1021.0	0	÷35.0	..	÷36.9	72	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1018.7	0	÷35.2	72	> 50	00	0	0	0	0	9	0	0	8	
	12	1016.3	0	÷36.4	73	> 50	00	0	0	0	0	9	0	0	8	
	15	1013.1	0	÷37.6	73	> 50	00	0	0	0	0	9	0	0	9	
	18	1011.0	0	÷37.0	÷34.8	..	73	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1009.2	0	÷36.1	74	> 50	00	0	0	0	0	9	0	0	6	
17	00	1007.4	0	÷36.1	74	> 50	00	0	0	0	0	9	0	0	8	
	03	1005.6	W 4	÷36.3	74	> 50	00	0	0	0	0	9	0	0	8	
	06	1005.2	W 10	÷34.1	..	÷37.7	74	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1005.7	E 2	÷32.5	72	> 50	03	2	8	0	0	9	4	×	4	
	12	1004.8	W 11	÷23.7	77	10-20	03	2	8	8	7	5	×	×	9	
	15	1006.4	W 10	÷22.5	82	10-20	02	2	8	8	6	5	×	×	3	
	18	1007.2	W 9	÷23.5	÷21.4	..	82	20-50	02	2	8	8	6	5	×	×	1	0.0
	21	1007.7	W 9	÷23.3	80	10-20	02	2	8	8	6	5	×	×	3	
18	00	1008.3	W 5	÷24.5	81	20-50	01	0	2	2	6	5	0	0	3	
	03	1008.7	W 13	÷24.6	68	> 50	00	0	0	0	0	9	0	0	3	
	06	1009.1	W 12	÷25.0	..	÷34.0	67	> 50	02	0	1	0	0	9	4	0	3	0.0
	09	1009.7	W 12	÷25.7	69	> 50	00	0	0	0	0	9	0	0	3	
	12	1011.1	W 10	÷26.8	66	> 50	00	0	0	0	0	9	0	0	1	
	15	1011.0	W 10	÷27.3	64	> 50	00	0	0	0	0	9	0	0	9	
	18	1011.6	W 9	÷28.2	÷23.0	..	62	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1013.5	W 10	÷28.5	62	> 50	00	0	0	0	0	9	0	0	4	
19	00	1014.2	W 9	÷28.0	61	> 50	00	0	0	0	0	9	0	0	1	
	03	1016.0	0	÷30.0	62	> 50	00	0	0	0	0	9	0	0	4	
	06	1016.5	0	÷32.1	..	÷32.1	63	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1016.5	0	÷33.2	65	> 50	00	0	0	0	0	9	0	0	3	
	12	1015.2	SSE 3	÷31.8	64	> 50	00	0	0	0	0	9	0	0	9	
	15	1013.1	0	÷33.0	69	> 50	00	0	0	0	0	9	0	0	9	
	18	1010.6	0	÷35.5	÷27.6	..	70	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1006.1	0	÷35.2	72	> 50	03	2	4	0	0	9	0	7	9	
20	00	1000.8	SE'E 3	÷34.1	73	> 50	03	2	8	0	0	9	2	×	9	
	03	995.4	W 3	÷32.9	73	4-10	02	2	8	0	0	9	2	×	8	
	06	992.9	W 6	÷33.6	..	÷35.4	73	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	991.3	W 6	÷32.3	72	> 50	00	0	0	0	0	9	0	0	6	
	12	990.2	W 12 ¹	÷29.0	76	10-20	02	0	2	0	0	9	4	0	6	

¹ 0930 the wind suddenly grew to 10-12 m/sec.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
21	15	992.1	W 15	÷29.4	78	0.2—0.5	39	3	9	9	×	×	×	×	4	
	18	995.3	W 10	÷29.4	÷27.4	..	78	> 50	00	3	0	0	0	9	0	0	4	0.0
	21	995.5	W 14	÷29.4	78	> 50	02	2	8	8	4	6	×	×	4	
	00	1002.1	W 14	÷28.8	78	> 50	00	0	0	0	0	9	0	0	1	
	03	1005.6	W 8	÷28.5	75	20—50	03	2	8	0	0	9	2	×	3	
	06	1006.8	W 9	÷28.7	..	÷33.5	73	20—50	02	2	7	0	0	9	2	×	1	0.0
	09	1007.5	W 6	÷29.0	72	20—50	02	2	8	0	0	9	2	×	3	
	12	1006.9	W 2	÷31.3	72	> 50	00	0	0	0	0	9	0	0	9	
	15	1005.0	E 5	÷31.9	73	> 50	00	0	0	0	0	9	0	0	9	
22	18	1003.0	0	÷33.7	÷28.3	..	73	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1000.8	0	÷34.4	74	> 50	00	0	0	0	0	9	0	0	8	
	00	999.7	W 3	÷34.5	75	> 50	00	0	0	0	0	9	0	0	6	
	03	999.0	W 5	÷32.4	75	20—50	03	2	8	0	0	9	2	×	6	
	06	998.8	W 6	÷33.4	..	÷35.2	75	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	999.5	W 6	÷32.0	75	20—50	02	0	3	0	0	9	5	0	4	
	12	1000.5	W 6	÷31.8	74	20—50	02	0	3	0	0	9	5	0	3	
	15	1001.7	W 4	÷32.0	73	20—50	03	0	4	0	0	9	5	0	3	
	18	1002.3	W 4	÷32.0	÷28.0	..	73	20—50	02	0	4	0	0	9	5	0	3	0.0
23	21	1002.7	W 4	÷32.3	74	> 50	00	0	0	0	0	9	0	0	3	
	00	1001.4	W 4	÷32.6	74	> 50	00	0	0	0	0	9	0	0	9	
	03	1001.9	0	÷35.0	74	> 50	00	0	0	0	0	9	0	0	4	
	06	1000.3	0	÷35.8	..	÷35.8	75	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	999.3	0	÷36.2	75	> 50	00	0	0	0	0	9	0	0	8	
	12	997.6	W 12	÷36.0	70	> 50	03	0	1	0	0	9	4	0	9	
	15	997.9	W 10	÷34.1	74	> 50	03	2	7	0	0	9	7	×	4	
	18	998.3	W 14	÷32.9	÷31.1	..	74	> 50	02	2	8	0	0	9	7	×	4	0.0
	21	1000.3	W 13	÷33.2	72	> 50	01	0	1	0	0	9	4	0	4	
24	00	1001.6	W 11	÷33.4	72	> 50	02	0	2	0	0	9	4	0	1	
	03	1002.8	W 10	÷32.5	72	> 50	00	0	0	0	0	9	0	0	3	
	06	1004.1	W 6	÷32.6	..	÷38.0	71	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1005.7	W 4	÷32.9	71	> 50	00	0	0	0	0	9	0	0	3	
	12	1007.0	0	÷34.7	72	> 50	00	0	0	0	0	9	0	0	3	
	15	1008.1	0	÷35.6	73	> 50	00	0	0	0	0	9	0	0	3	
	18	1008.9	0	÷37.6	÷32.0	..	74	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1009.4	W 4	÷37.4	74	> 50	00	0	0	0	0	9	0	0	3	
	00	1010.3	0	÷37.3	74	> 50	00	0	0	0	0	9	0	0	3	
25	03	1011.5	W 4	÷36.7	74	> 50	03	0	1	0	0	9	5	0	3	
	06	1012.5	0	÷36.0	..	÷37.9	74	20—50	03	2	8	0	0	9	0	7	3	0.0
	09	1014.3	W 3	÷35.2	74	20—50	02	2	8	0	0	9	0	7	4	
	12	1016.2	0	÷34.6	74	> 50	01	0	0	0	0	9	0	0	3	
	15	1017.4	0	÷36.5	74	> 50	00	0	0	0	0	9	0	0	3	
	18	1017.7	0	÷37.9	÷33.0	..	74	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1017.3	0	÷38.4	74	> 50	00	0	0	0	0	9	0	0	9	
	00	1015.5	0	÷38.8	74	> 50	03	0	3	0	0	9	0	6	9	
	03	1012.2	0	÷36.3	74	1—2	73	7	8	8	7	4	×	×	9	
26	06	1009.9	W 6	÷35.4	..	÷39.2	74	1—2	73	7	8	8	7	4	×	×	6	trace
	09	1009.2	W 8	÷33.7	74	1—2	02	7	8	8	6	4	×	×	6	
	12	1009.3	W 15	÷28.4	×	0—0.05	73	7	9	9	×	×	×	×	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
27	15	1013.2	W 13	÷29.0	×	0.2—0.5	39	3	0	0	0	9	0	0	4	0.4	
	18	1015.9	W 10	÷30.0	÷27.4	..	×	4—10	00	3	0	0	0	9	0	0	3		
	21	1018.2	W 6	÷30.5	×	> 50	00	0	0	0	0	9	0	0	3		
	00	1017.5	W 5	÷30.2	×	> 50	03	0	3	0	0	9	5	0	9		
	03	1017.3	S 6	÷32.4	×	> 50	00	0	0	0	0	9	0	0	8		
	06	1015.7	E 6	÷34.8	..	÷35.5	×	> 50	00	0	0	0	0	9	0	0	9		0.0
09	1014.3	E 7	÷34.4	×	> 50	00	0	0	0	0	9	0	0	8			
12	1014.3	0	÷35.0	×	> 50	00	0	0	0	0	9	0	0	3			
15	1010.7	E 4	÷35.2	×	> 50	00	0	0	0	0	9	0	0	9			
18	1008.5	W 3	÷36.5	÷30.0	..	×	> 50	00	0	0	0	0	9	0	0	8	0.0		
21	1004.4	0	÷36.4	×	> 50	02	2	6	0	0	9	0	6	9			
28	00	1002.0	W 4	÷35.4	70	20—50	03	2	8	0	0	9	2	×		6	
03	996.5	0	÷34.0	74	1—2	73	7	8	8	7	×	×	×	9			
06	992.0	0	÷32.1	..	÷37.2	78	4—10	02	7	8	0	0	9	7	×	6		0.1	
09	988.9	W 11	÷30.0	82	2—4	02	2	8	8	6	6	×	×	6			
12	991.3	W 14	÷29.7	87	0.2—0.5	39	3	9	9	×	×	×	×	4			
15	993.7	W 8	÷28.3	92	2—4	02	3	8	8	6	5	×	×	4			
18	996.9	W 6	÷29.4	÷27.3	..	92	> 50	02	0	3	0	0	9	5	0	4	0.0		
21	1003.1	0	÷31.0	92	> 50	00	0	0	0	0	9	0	0	4			
29	00	1006.7	0	÷32.6	92	> 50	00	0	0	0	0	9	0	0		1	
03	1009.5	0	÷32.9	94	> 50	00	0	0	0	0	9	0	0	3			
06	1011.1	0	÷32.5	..	÷35.2	94	> 50	00	0	0	0	0	9	0	0	1		0.0	
09	1013.3	0	÷34.0	94	> 50	03	2	8	0	0	9	3	×	4			
12	1013.7	0	÷33.7	96	> 50	01	0	1	0	0	9	4	0	9			
15	1009.7	E 2	÷33.7	96	> 50	01	0	1	0	0	9	4	0	9			
18	1007.5	W 3	÷34.2	÷29.0	..	96	> 50	03	0	4	0	0	9	0	2	6	0.0		
21	1004.6	W 10	÷31.5	×	> 50	02	0	3	0	0	9	4	0	8			
30	00	1002.8	W 11	÷28.5	×	> 50	01	0	1	0	0	9	4	0		8	
03	1002.1	W 5	÷25.7	×	> 50	03	2	8	0	0	9	7	×	6			
06	1000.8	0	÷27.5	..	÷34.9	×	> 50	02 ¹	0	2	0	0	9	4	0	9		0.0	
09	1001.5	E 6	÷27.5	×	20—50	02	2	8	0	0	9	7	×	1			
12	1003.5	E 3	÷27.5	×	2—4	71 ²	2	8	8	7	3	×	×	4			
15	1006.8	0	÷27.0	×	> 50	00	2	0	0	0	9	0	0	4			
18	1009.3	0	÷29.9	÷25.2	..	×	> 50	00	0	0	0	0	9	0	0	1	trace		
21	1011.0	W 3	÷29.5	×	> 50	00	0	0	0	0	9	0	0	1			
31	00	1011.6	0	÷30.0	×	> 50	03	0	1	0	0	9	5	0		9	
03	1007.7	0	÷29.5	×	> 50	00	0	0	0	0	9	0	0	9			
06	1005.9	W 6	÷24.2	..	÷30.4	×	> 50	00	0	0	0	0	9	0	0	6		0.0	
09	1004.8	W 3	÷26.6	×	> 50	02	0	1	0	0	9	0	2	6			
12	1003.0	W 4	÷27.9	×	> 50	02	0	1	0	0	9	4	0	8			
15	1001.9	W 3	÷26.7	×	> 50	03	2	8	0	0	9	4	6	8			
18	1000.9	W 3	÷26.7	÷22.3	..	×	> 50	01	0	1	0	0	9	4	0	8	0.0		
21	998.2	SSW 2	÷29.0	×	> 50	02	0	1	0	0	9	4	0	9			
Mean	1010.9	3.8	÷30.6	÷26.6	÷33.8	74	0.5

¹ Lunar halo. ² 1100—1245 light snow.

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	998.9	W 6	÷26.4	78	> 50	02	0	1	0	0	9	4	0	4	
	03	999.2	W 7	÷24.0	78	> 50	02	0	1	0	0	9	4	0	3	
	06	999.5	W 8	÷23.3	..	÷29.0	78	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1000.5	W 2	÷26.6	78	> 50	02	0	2	0	0	9	4	2	4	
	12	1002.7	W 3	÷25.8	81	> 50	00	0	0	0	0	9	0	0	4	
	15	1005.5	0	÷28.6	82	> 50	00	0	0	0	0	9	0	0	1	
	18	1007.4	0	÷29.8	÷23.1	..	83	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1009.1	W 7	÷27.3	82	> 50	00	0	0	0	0	9	0	0	3	
2	00	1010.5	0	÷28.5	82	> 50	00	0	0	0	0	9	0	0	1	
	03	1011.2	0	÷31.0	85	> 50	03	0	2	0	0	9	0	5	3	
	06	1011.9	0	÷32.6	..	÷33.8	86	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1011.9	0	÷32.7	88	> 50	00	0	0	0	0	9	0	0	3	
	12	1011.5	WSW 4	÷29.9	88	> 50	00	0	0	0	0	9	0	0	9	
	15	1011.1	0	÷31.5	89	> 50	00	0	0	0	0	9	0	0	8	
	18	1010.6	0	÷30.9	÷26.9	..	89	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1010.1	0	÷31.2	88	> 50	03	2	4	0	0	9	0	6	8	
3	00	1010.1	0	÷31.7	89	> 50	03 ¹	2	8	0	0	9	0	7	3	
	03	1010.1	0	÷32.1	89	20-50	03	2	8	0	0	9	7	×	3	
	06	1009.3	0	÷31.5	..	÷33.2	89	20-50	02	2	8	0	0	9	7	×	9	0.0
	09	1009.9	0	÷30.3	89	20-50	02	2	8	0	0	9	7	×	4	
	12	1009.3	0	÷30.0	89	20-50	02	2	8	0	0	9	1	×	9	
	15	1009.0	0	÷31.2	88	20-50	02	2	8	0	0	9	1	×	8	
	18	1008.3	0	÷31.7	÷29.8	..	88	20-50	02	2	8	0	0	9	1	×	9	0.0
	21	1006.7	0	÷29.4	88	20-50	02	2	8	0	0	9	2	×	8	
4	00	1004.9	0	÷27.2	88	> 50	02	2	8	0	0	9	2	×	8	
	03	1002.5	0	÷27.5	88	> 50	01	2	3	0	0	9	4	0	8	
	06	1000.1	0	÷26.7	..	÷32.0	88	> 50	03	2	8	0	0	9	7	×	8	0.0
	09	998.4	0	÷29.9	86	> 50	01	0	1	0	0	9	4	0	8	
	12	995.2	W 5	÷28.3	88	> 50	02	0	1	0	0	9	4	0	9	
	15	993.6	W 9	÷24.0	87	> 50	03	2	7	7	6	4	×	×	6	
	18	993.6	W 8	÷20.2	÷19.8	..	84	20-50	02	2	7	7	6	4	×	×	3	0.0
	21	994.5	W 7	÷20.1	75	> 50	00	0	0	0	0	9	0	0	4	
5	00	995.0	W 7	÷17.6	72	> 50	00	0	0	0	0	9	0	0	3	
	03	995.9	W 8	÷17.9	71	> 50	00	0	0	0	0	9	0	0	3	
	06	996.3	W 12	÷17.4	..	÷30.5	72	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	998.2	W 13	÷17.8	72	> 50	00	0	0	0	0	9	0	0	4	
	12	1000.8	W 16	÷20.5	80	20-50	00	0	0	0	0	9	0	0	1	
	15	1001.7	W 16	÷20.6	80	10-20	00	0	0	0	0	9	0	0	1	
	18	1004.3	W 9	÷21.4	÷14.4	..	76	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1007.0	W 8	÷22.0	75	> 50	02	0	1	0	0	9	4	0	3	
6	00	1008.9	W 5	÷21.5	75	20-50	03	2	6	0	0	9	5	0	1	
	03	1011.4	W 5	÷22.0	76	20-50	02	2	8	0	0	9	7	×	3	
	06	1012.3	0	÷22.6	..	÷22.6	76	20-50	02	2	8	0	0	9	7	×	1	0.0
	09	1013.1	W 2	÷23.1	76	20-50	02	2	8	0	0	9	7	×	3	
	12	1012.6	E 5	÷23.1	90	20-50	02	2	8	0	0	9	7	×	9	
	15	1011.3	E 3	÷23.8	90	10-20	03	2	8	8	6	5	×	×	9	

¹ Lunar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
7	18	1010.8	E 2	÷24.6	÷21.0	..	90	2—4	71	7	8	8	7	4	×	×	6	trace
	21	1011.5	0	÷25.7	90	1—2	71	7	8	8	7	4	×	×	4	
	00	1012.8	W 5	÷27.5	90	2—4	71	7	8	8	7	5	×	×	4	
	03	1014.5	W 7	÷26.3	88	2—4	02	7	8	8	7	5	×	×	4	
	06	1016.0	W 10	÷25.0	..	÷28.0	87	2—4	02	2	8	8	6	5	×	×	3	trace
	09	1019.4	W 10	÷24.6	85	2—4	02	2	8	8	6	5	×	×	4	
8	12	1021.6	W 9	÷25.4	82	2—4	02	2	3	0	0	9	4	0	3	
	15	1023.7	W 4	÷27.0	78	4—10	02	2	4	0	0	9	4	0	3	
	18	1024.6	0	÷28.6	÷22.3	..	81	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1025.9	0	÷30.5	82	> 50	00	0	0	0	0	9	0	0	3	
	00	1025.9	0	÷31.5	82	> 50	00	0	0	0	0	9	0	0	3	
	03	1025.9	0	÷32.6	83	> 50	00	0	0	0	0	9	0	0	3	
	06	1025.0	0	÷34.0	..	÷34.0	84	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1024.7	W 3	÷35.2	84	> 50	00	0	0	0	0	9	0	0	8	
	12	1024.2	0	÷35.6	85	> 50	00	0	0	0	0	9	0	0	8	
	15	1024.8	W 1	÷35.8	85	> 50	00	0	0	0	0	9	0	0	4	
9	18	1024.9	W 4	÷34.6	÷24.1	..	85	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1026.1	0	÷34.4	82	> 50	00	0	0	0	0	9	0	0	4	
	00	1026.9	W 3	÷33.0	82	> 50	00	0	0	0	0	9	0	0	3	
	03	1027.9	W 2	÷32.7	80	> 50	00	0	0	0	0	9	0	0	3	
	06	1028.6	0	÷33.0	..	÷36.1	80	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1029.2	0	÷33.5	82	> 50	00	0	0	0	0	9	0	0	3	
	12	1029.4	0	÷34.6	82	> 50	00	0	0	0	0	9	0	0	1	
	15	1029.1	0	÷35.0	84	> 50	00	0	0	0	0	9	0	0	9	
	18	1028.6	0	÷35.2	÷32.2	..	84	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1027.9	0	÷36.0	84	> 50	00	0	0	0	0	9	0	0	8	
10	00	1027.4	0	÷35.9	84	> 50	00	0	0	0	0	9	0	0	8	
	03	1026.8	0	÷36.0	84	> 50	00	0	0	0	0	9	0	0	8	
	06	1026.2	0	÷36.1	..	÷36.2	84	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1027.0	0	÷35.8	84	> 50	00	0	0	0	0	9	0	0	4	
	12	1027.2	W'S 4	÷33.5	84	> 50	00	0	0	0	0	9	0	0	3	
	15	1027.8	0	÷34.0	84	> 50	03	2	8	0	0	9	0	7	3	
	18	1028.4	W 2	÷33.5	÷32.3	..	83	> 50	02	2	8	0	0	9	0	7	3	0.0
	21	1029.3	0	÷33.5	82	> 50	01	0	1	0	0	9	4	0	3	
	00	1029.8	WSW 4	÷31.9	82	> 50	00	0	0	0	0	9	0	0	3	
	03	1030.2	W 7	÷32.2	81	> 50	00	0	0	0	0	9	0	0	3	
11	06	1029.5	W 6	÷32.8	..	÷36.4	81	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1029.7	W 7	÷32.6	81	> 50	03	0	2	0	0	9	0	5	4	
	12	1029.8	W 6	÷32.4	81	> 50	02	0	3	0	0	9	0	4	3	
	15	1029.8	W 8	÷30.3	80	20—50	03	2	7	7	6	5	0	0	3	
	18	1029.4	W 10	÷29.5	÷28.9	..	82	2—4	02	2	8	8	6	5	×	×	9	0.0
	21	1029.9	W 9	÷29.5	78	2—4	02	2	8	8	6	5	×	×	4	
	00	1030.2	W 9	÷29.8	78	10—20	00	0	0	0	0	9	0	0	3	
	03	1031.1	W 8	÷30.0	75	20—50	00	0	0	0	0	9	0	0	4	
	06	1031.4	W 5	÷30.7	..	÷32.8	76	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1032.2	W 4	÷30.5	77	> 50	02	0	1	0	0	9	4	0	3	
12	12	1032.8	W 1	÷33.4	76	> 50	02	0	1	0	0	9	4	0	3	
	15	1032.6	0	÷34.6	80	> 50	02	0	1	0	0	9	4	0	9	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
13	18	1032.0	0	÷35.4	÷28.2	..	80	> 50	00	0	0	0	0	9	0	0	8	0.0	
	21	1031.6	0	÷36.0	80	> 50	00	0	0	0	0	9	0	0	8		
	00	1030.9	0	÷36.3	81	> 50	00	0	0	0	0	9	0	0	8		
	03	1029.8	WSW 3	÷35.8	82	> 50	00	0	0	0	0	9	0	0	8		
	06	1028.7	0	÷36.3	..	÷37.4	80	> 50	00	0	0	0	0	9	0	0	8	0.0	
	09	1028.2	0	÷35.5	83	> 50	00	0	0	0	0	9	0	0	6		
	12	1027.5	0	÷36.6	82	> 50	00	0	0	0	0	9	0	0	8		
	15	1026.7	0	÷35.2	82	> 50	00	0	0	0	0	9	0	0	8		
	18	1025.9	0	÷35.3	÷28.0	82	> 50	00	0	0	0	9	0	0	8	0.0	
14	21	1025.4	W 5	÷34.8	82	> 50	00	0	0	0	0	9	0	0	8		
	00	1024.6	W 3	÷34.1	82	> 50	00	0	0	0	0	9	0	0	8		
	03	1022.9	0	÷36.8	82	> 50	00	0	0	0	0	9	0	0	9		
	06	1021.4	W 3	÷36.9	..	÷37.3	83	> 50	00	0	0	0	0	9	0	0	8	0.0	
	09	1019.4	0	÷35.8	84	> 50	00	0	0	0	0	9	0	0	8		
	12	1017.3	0	÷36.3	84	> 50	00	0	0	0	0	9	0	0	8		
	15	1014.4	W 3	÷38.3	83	> 50	00	0	0	0	0	9	0	0	9		
	18	1012.6	W 2	÷37.4	÷34.1	84	> 50	00	0	0	0	9	0	0	8	0.0	
	21	1010.5	W 2	÷36.4	84	> 50	00	0	0	0	0	9	0	0	8		
15	00	1008.1	W 6	÷37.0	83	> 50	00	0	0	0	0	9	0	0	8		
	03	1006.8	W 4	÷33.3	83	> 50	03	2	8	0	0	9	2	×	6		
	06	1006.5	W 4	÷32.0	..	÷38.4	82	10—20	71	7	8	8	7	5	×	×	6	trace	
	09	1007.3	E 2	÷33.3	84	10—20	02	7	8	8	6	5	×	×	4		
	12	1008.5	0	÷31.8	86	10—20	02	2	8	8	6	4	×	×	4		
	15	1010.1	W 13	÷28.4	76	20—50	00	2	0	0	0	9	0	0	3		
	18	1011.5	W 9	÷28.0	÷31.0	75	20—50	00	0	0	0	9	0	0	3	trace	
	21	1013.2	W 11	÷29.8	74	> 50	02	0	2	0	0	9	4	0	3		
	00	1014.0	W 11	÷30.2	73	20—50	02	0	2	0	0	9	4	0	1		
16	03	1016.1	W 11	÷30.6	74	10—20	03	2	8	8	6	5	×	×	4		
	06	1015.8	W 12	÷31.0	..	÷33.0	78	2—4	36	3	8	8	6	5	×	×	9	0.0	
	09	1016.4	W 10	÷31.3	78	1—2	36	3	8	8	6	4	×	×	4		
	12	1017.3	W 12	÷31.7	83	0.5—1	37	3	8	8	6	4	×	×	4		
	15	1017.5	W 12	÷32.0	84	1—2	36	3	8	8	6	4	×	×	1		
	18	1017.3	W 15	÷32.2	÷28.0	85	0.5—1	37	3	8	8	6	4	×	×	9	0.0
	21	1017.1	W 15	÷31.8	85	0.5—1	37	3	8	9	×	×	×	×	8		
	00	1016.9	W 15	÷31.7	85	0.5—1	37	3	8	9	×	×	×	×	8		
	03	1016.5	W 17	÷31.7	87	< 0.05	37	3	9	9	×	×	×	×	8		
17	06	1016.3	W 15	÷32.8	..	÷33.1	88	< 0.05	39	3	9	9	×	×	×	×	8	0.0	
	09	1015.9	W 13	÷31.6	88	< 0.05	39	3	9	9	×	×	×	×	8		
	12	1015.9	W 13	÷31.6	88	< 0.05	39	3	9	9	×	×	×	×	3		
	15	1015.3	W 12	÷31.5	88	< 0.05	39	3	9	9	×	×	×	×	9		
	18	1015.1	W 10	÷31.5	÷31.5	88	< 0.05	39	3	9	9	×	×	×	×	6	0.0
	21	1014.5	W 13	÷31.5	88	< 0.05	39	3	9	9	×	×	×	×	9		
	00	1013.7	W 18	÷31.0	88	< 0.05	39	3	9	9	×	×	×	×	8		
	03	1013.1	W 18	÷31.8	88	< 0.05	39	3	9	9	×	×	×	×	8		
	06	1012.8	W 15	÷30.5	..	÷33.0	88	< 0.05	39	3	9	9	×	×	×	×	8	0.0	
18	09	1012.4	W 15	÷30.1	88	1—2	02	3	8	8	6	6	×	×	8		
	12	1012.8	W 15	÷30.0	88	0.5—1	36	3	8	8	6	4	×	×	4		
	15	1013.2	W 9	÷30.3	87	10—20	02	2	8	4	6	4	7	×	3	0.1	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
19	18	1013.4	W 10	÷29.5	÷29.2	..	84	20—50	01	0	2	0	0	9	4	0	3	
	21	1013.6	W 10	÷29.9	82	> 50	00	0	0	0	0	9	0	0	3	
	00	1013.4	WSW 7	÷30.4	79	> 50	00	0	0	0	0	9	0	0	9	
	03	1012.9	WSW 12	÷31.0	79	> 50	00	0	0	0	0	9	0	0	9	
	06	1012.7	W 8	÷31.0	..	÷31.0	79	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1011.7	W 5	÷33.5	×	> 50	00	0	0	0	0	9	0	0	9	
	12	1011.5	W 6	÷34.0	×	> 50	00	0	0	0	0	9	0	0	6	
	15	1010.1	W 6	÷34.4	×	20—50	03	2	4	2	6	3	4	0	9	
	18	1009.8	W 6	÷34.4	÷28.3	..	×	> 50	03	0	3	0	0	9	5	0	6	0.0
	21	1009.5	W 6	÷35.6	×	> 50	02	0	3	0	0	9	5	0	8	
20	00	1008.9	W 7	÷34.6	×	> 50	00	0	0	0	0	9	0	0	8	
	03	1008.5	W 7	÷34.8	×	> 50	00	0	0	0	0	9	0	0	8	
	06	1007.8	W 6	÷34.9	..	÷35.2	×	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1008.0	W 7	÷35.3	×	> 50	02	0	1	0	0	9	0	2	4	
	12	1008.4	W 8	÷35.7	×	> 50	02	0	1	0	0	9	0	2	3	
	15	1008.8	W 7	÷36.2	×	> 50	02	0	1	0	0	9	0	2	3	
	18	1009.8	W 3	÷37.5	÷34.4	..	×	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1010.6	W 5	÷37.3	×	> 50	00	0	0	0	0	9	0	0	3	
	00	1011.1	W 5	÷37.6	70	> 50	00	0	0	0	0	9	0	0	3	
	03	1011.3	W 5	÷37.2	71	> 50	00	0	0	0	0	9	0	0	3	
21	06	1011.3	0	÷38.4	..	÷38.4	73	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1010.2	0	÷39.0	75	> 50	00	0	0	0	0	9	0	0	9	
	12	1008.0	W 4	÷38.4	76	> 50	03	0	3	0	0	9	0	0	9	
	15	1006.2	W 2	÷38.2	78	20—50	03	0	8	8	6	4	×	×	6	
	18	1005.7	0	÷35.8	÷37.0	..	81	10—20	02	2	8	8	6	4	×	×	8	0.0
	21	1006.0	W 7	÷24.3	87	10—20	02	2	8	8	6	4	×	×	4	
	00	1007.1	W 6	÷25.2	92	10—20	02	2	8	8	6	4	×	×	4	
	03	1008.4	W 7	÷24.9	93	10—20	02	2	8	8	6	4	×	×	3	
	06	1010.2	0	÷27.4	..	÷39.8	93	> 50	02	2	8	0	0	9	1	×	3	0.0
	09	1011.5	WSW 2	÷24.5	94	> 50	02	2	8	0	0	9	7	×	3	
22	12	1011.9	W 6	÷23.8	94	> 50	02	2	8	0	0	9	7	×	1	
	15	1012.3	W 7	÷23.7	88	> 50	01	0	4	0	0	9	4	0	3	
	18	1012.4	0	÷24.0	÷20.2	..	80	> 50	01	0	1	0	0	9	0	8	3	0.0
	21	1013.3	0	÷23.3	92	> 50	02	0	1	0	0	9	0	8	4	
	00	1013.9	SW 4	÷22.1	90	> 50	03	2	8	0	0	9	1	×	3	
	03	1014.7	W 7	÷22.1	92	> 50	02	2	8	0	0	9	1	×	3	
	06	1016.0	W 7	÷24.0	..	÷32.1	90	20—50	02	2	8	8	6	4	×	×	4	0.0
	09	1017.3	W 8	÷24.7	88	20—50	02	2	4	0	0	9	5	0	3	
	12	1016.8	W 6	÷25.1	86	> 50	00	0	0	0	0	9	0	0	9	
	15	1016.1	0	÷27.5	86	> 50	00	0	0	0	0	9	0	0	8	
24	18	1015.5	0	÷30.5	÷20.2	..	88	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1014.3	0	÷31.6	92	> 50	00	0	0	0	0	9	0	0	9	
	00	1013.2	0	÷33.5	92	> 50	00	0	0	0	0	9	0	0	8	
	03	1012.0	W 3	÷32.5	93	> 50	00	0	0	0	0	9	0	0	8	
	06	1011.9	0	÷32.8	..	÷33.8	92	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1011.8	0	÷32.1	92	> 50	00	0	0	0	0	9	0	0	8	
	12	1011.9	0	÷32.1	92	> 50	02	0	1	0	0	9	4	0	4	
	15	1011.7	0	÷32.2	92	> 50	02	0	1	0	0	9	4	0	9	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
25	18	1011.5	WSW 10	÷28.1	÷26.4	..	90	> 50	02	0	1	0	0	9	4	0	8	0.0	
	21	1011.9	W 12	÷30.4	90	20—50	00	0	0	0	0	9	0	0	4		
	00	1012.1	W 12	÷31.5	88	20—50	00	0	0	0	0	9	0	0	3		
26	03	1013.8	W 9	÷32.7	86	> 50	00	0	0	0	0	9	0	0	4		
	06	1012.8	W 8	÷33.6	..	÷33.6	86	> 50	00	0	0	0	0	9	0	0	9	0.0	
	09	1012.8	S 1	÷36.4	85	> 50	00	0	0	0	0	9	0	0	3		
	12	1012.4	ESE 4	÷37.5	86	> 50	00	0	0	0	0	9	0	0	9		
	15	1010.2	0	÷38.5	86	> 50	00	0	0	0	0	9	0	0	9		
	18	1009.2	0	÷39.9	÷28.0	88	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1008.8	0	÷40.2	91	> 50	00	0	0	0	0	9	0	0	8	
	00	1008.9	0	÷41.5	92	> 50	00	0	0	0	0	9	0	0	4	
	03	1008.9	0	÷41.1	92	> 50	00	0	0	0	0	9	0	0	3	
	06	1008.0	0	÷40.5	..	÷42.2	..	92	> 50	00	0	0	0	0	9	0	0	9	0.0
27	09	1007.9	0	÷41.3	92	> 50	00	0	0	0	0	9	0	0	6		
	12	1008.0	0	÷39.6	90	> 50	00	0	0	0	0	9	0	0	4		
	15	1008.9	0	÷40.1	89	> 50	00	0	1	0	0	9	0	8	4		
	18	1008.9	0	÷40.6	÷39.4	89	> 50	00	0	1	0	0	9	0	8	3	0.0
	21	1009.4	W 1	÷41.0	90	> 50	00	0	0	0	0	9	0	0	4	
	00	1009.4	0	÷41.1	90	> 50	00	0	0	0	0	9	0	0	3	
	03	1009.4	0	÷42.0	90	> 50	00	0	0	0	0	9	0	0	3	
	06	1009.4	0	÷42.9	..	÷43.0	..	91	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1009.8	0	÷43.0	91	> 50	00	0	0	0	0	9	0	0	4	
	12	1011.2	0	÷43.0	91	> 50	03	0	3	0	0	9	5	0	3	
28	15	1011.8	0	÷42.8	90	> 50	02	0	1	0	0	9	0	1	1		
	18	1012.1	0	÷42.9	÷40.5	..	90	> 50	00	0	0	0	0	9	0	0	4	0.0	
	21	1012.8	0	÷42.7	90	> 50	00	0	0	0	0	9	0	0	1	
	00	1013.2	0	÷43.1	89	> 50	00	0	0	0	0	9	0	0	3	
	03	1014.2	W 4	÷42.1	89	> 50	00	0	0	0	0	9	0	0	4	
	06	1013.1	W 6	÷40.6	..	÷44.1	..	89	> 50	02	0	1	0	0	9	4	0	8	0.0
	09	1015.0	W 6	÷39.0	87	> 50	03	2	8	0	0	9	7	×	4	
	12	1016.1	W 6	÷38.7	86	> 50	01	2	7	0	0	9	7	×	3	
	15	1017.0	W 4	÷39.5	85	> 50	01	0	1	0	0	9	4	0	3	
	18	1017.5	0	÷42.2	÷39.0	86	> 50	02	0	1	0	0	9	4	0	1	0.0
21	1018.5	SSW 2	÷43.2	88	> 50	00	0	0	0	0	9	0	0	4		
Mean		1014.6	4.4	÷32.0	÷28.5	÷34.5	88	0.2	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
1	00	1018.7	0	÷42.8	88	> 50	00	0	0	0	0	9	0	0	1		
	03	1018.1	W 2	÷42.0	88	> 50	00	0	0	0	0	9	0	0	9		
	06	1017.8	0	÷42.7	..	÷43.4	..	88	> 50	00	0	0	0	0	9	0	0	6	0.0
	09	1017.3	0	÷42.5	88	> 50	03	0	4	0	0	9	5	0	8	
	12	1016.6	0	÷43.3	88	> 50	02	2	4	0	0	9	5	0	8	
	15	1014.6	W 4	÷42.5	89	> 50	03	2	4	0	0	9	5	5	9	
	18	1012.4	W 5	÷39.8	÷39.8	86	> 50	02	2	8	0	0	9	2	×	8	0.0

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
2	21	1010.3	W 9	÷35.3	×	10—20	02	2	8	0	0	9	2	×	8	
	00	1007.2	W 14	÷32.6	×	0.2—0.5	39 ¹	3	9	9	×	×	×	×	9	
3	03	1006.1	W 15	÷31.3	×	0.2—0.5	39	3	9	9	×	×	×	×	6	
	06	1003.9	W 19	÷31.5	..	÷43.5	×	0.05—0.2	39	3	9	9	×	×	×	×	8	×
	09	1004.3	W 14	÷32.7	×	0.2—0.5	39	3	9	9	×	×	×	×	4	
	12	1004.4	W 18	÷32.5	×	0.5—1	38	3	9	9	×	×	×	×	3	
	15	1005.2	W 14	÷32.2	×	2—4	36	3	0	0	0	9	0	0	4	
	18	1005.3	W 13	÷31.5	÷31.5	..	×	10—20	03	3	5	0	0	9	3	×	1	×
	21	1004.0	W 15	÷29.5	×	2—4	36	3	9	9	×	×	×	×	9	
	00	1003.6	W 12	÷28.4	×	4—10	36	3	9	9	×	×	×	×	8	
	03	1002.2	W 12	÷27.2	×	10—20	02	2	8	0	0	9	3	×	9	
	06	1002.2	W 10	÷26.6	..	÷33.5	×	10—20	02	2	8	8	6	3	×	×	3	×
4	09	1001.6	W 10	÷26.1	×	10—20	02	2	8	8	6	3	×	×	9	
	12	1000.7	W 11	÷26.4	×	10—20	02	2	8	8	6	3	×	×	8	
	15	999.4	W 10	÷26.3	×	20—50	02	2	8	8	6	5	×	×	8	
	18	999.1	W 10	÷26.3	÷26.0	..	×	10—20	02	2	8	8	6	3	×	×	6	×
	21	997.2	W 12	÷25.8	×	10—20	02	2	8	8	6	3	×	×	9	
	00	995.3	W 15	÷25.5	×	10—20	02	2	8	8	6	3	×	×	8	
	03	992.9	W 17	÷25.5	×	0.2—0.5	39	3	9	9	×	×	×	×	8	
	06	990.2	W 16	÷25.6	÷	÷26.6	×	0.2—0.5	39	3	9	9	×	×	×	×	8	×
	09	989.4	W 15	÷26.3	×	< 0.05	39	3	9	9	×	×	×	×	6	
	12	989.6	W 15	÷26.1	×	< 0.05	39	3	9	9	×	×	×	×	4	
5	15	990.0	W 21	÷26.3	×	< 0.05	39	3	9	9	×	×	×	×	3	
	18	988.8	W 20	÷27.2	÷25.5	..	×	< 0.05	39	3	9	9	×	×	×	×	9	trace
	21	989.4	W 19	÷28.2	×	< 0.05	39	3	9	9	×	×	×	×	4	
	00	989.7	W 16	÷26.7	×	< 0.05	39	3	9	9	×	×	×	×	3	
	03	991.0	W 17	÷26.1	×	< 0.05	39	3	9	9	×	×	×	×	4	
	06	991.8	W 20	÷26.2	..	÷28.3	×	< 0.05	39	3	9	9	×	×	×	×	3	×
	09	993.3	W 18	÷25.5	×	< 0.05	39	3	9	9	×	×	×	×	3	
	12	994.3	W 16	÷25.6	×	< 0.05	39	3	9	9	×	×	×	×	3	
	15	994.8	W 15	÷25.5	×	< 0.05	39	3	9	9	×	×	×	×	2	
	18	995.3	W 15	÷25.0	÷25.0	..	×	< 0.05	39	3	9	9	×	×	×	×	3	×
6	21	996.5	W 14	÷25.2	×	< 0.05	39 ²	3	9	9	×	×	×	×	4	
	00	997.7	W 15	÷25.3	×	0.05—0.2	73	7	9	9	×	×	×	×	3	
	03	1000.0	W 17	÷25.5	×	< 0.05	73	7	9	9	×	×	×	×	1	
	06	1001.9	W 15	÷26.4	..	÷26.5	×	< 0.05	39	3	9	9	×	×	×	×	3	—
	09	1004.3	W 16	÷26.7	×	< 0.05	39	3	9	9	×	×	×	×	3	
	12	1007.1	W 17	÷27.7	×	< 0.05	39	3	9	9	×	×	×	×	3	
	15	1010.1	W 13	÷26.7	×	0.05—0.2	38	3	9	9	×	×	×	×	3	
	18	1012.4	W 15	÷26.3	÷24.8	..	×	0.2—0.5	36	3	8	8	6	4	×	×	3	1.7 ³
	21	1015.7	W 16	÷25.6	×	< 0.05	39	3	9	9	×	×	×	×	3	
	7	00	1018.5	W 15	÷25.4	×	10—20	02	2	8	8	6	4	×	×	3
03		1022.0	W 12	÷25.7	×	20—50	02	2	8	8	6	5	×	×	3	
06		1023.8	W 10	÷25.8	..	÷27.9	×	20—50	02	2	6	6	6	5	0	0	1	0.0
09		1025.9	W 11	÷26.0	×	> 50	00	0	0	0	0	9	0	0	3	
12		1026.7	W 5	÷27.7	×	> 50	03	0	3	0	0	9	5	0	1	
15		1028.3	W 4	÷28.1	×	> 50	03	0	5	0	0	9	0	5	4	

¹ Possibly snow fall too. ² 3—5 March possibly snow fall. ³ for 24 hours.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1028.3	W 2	÷29.3	÷25.2	..	×	> 50	03	0	3	0	0	9	5	0	3	0.0
	21	1027.6	0	÷30.0	×	> 50	00	0	0	0	0	9	0	0	9	
8	00	1028.3	0	÷31.6	×	> 50	00	0	0	0	0	9	0	0	4	
	03	1029.0	W 5	÷32.2	×	> 50	00	0	0	0	0	9	0	0	3	
	06	1028.1	W 4	÷31.1	..	÷34.2	×	> 50	02	0	1	0	0	9	0	8	9	0.0
	09	1027.0	W 5	÷31.0	×	> 50	02	0	1	0	0	9	0	8	8	
	12	1026.9	W 6	÷30.9	×	> 50	02	0	1	0	0	9	0	2	6	
	15	1028.4	W 3	÷30.9	×	> 50	03	2	8	0	0	9	0	7	4	
	18	1028.4	0	÷30.8	÷29.3	..	×	> 50	01	0	1	0	0	9	0	2	3	0.0
	21	1027.8	0	÷30.5	×	> 50	00	0	0	0	0	9	0	0	9	
9	00	1028.1	E 5	÷31.3	×	> 50	00	0	0	0	0	9	0	0	4	
	03	1027.8	0	÷32.3	×	> 50	00	0	0	0	0	9	0	0	9	
	06	1026.5	0	÷34.0	..	÷34.0	×	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1024.5	W 4	÷35.6	×	> 50	00	0	0	0	0	9	0	0	8	
	12	1022.6	0	÷35.3	×	> 50	00	0	0	0	0	9	0	0	8	
	15	1020.2	0	÷34.9	×	> 50	00	0	0	0	0	9	0	0	8	
	18	1018.6	W 3	÷34.6	÷30.5	..	58	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1017.6	W 5	÷33.2	59	> 50	00	0	0	0	0	9	0	0	8	
10	00	1016.7	0	÷33.6	59	> 50	00	0	0	0	0	9	0	0	8	
	03	1015.0	0	÷35.0	59	> 50	00	0	0	0	0	9	0	0	9	
	06	1013.3	0	÷34.8	..	÷36.1	59	> 50	03	2	8	0	0	9	2	×	8	0.0
	09	1012.6	W 3	÷33.1	59	> 50	01	0	1	0	0	9	4	0	6	
	12	1016.0	0	÷33.3	60	> 50	03	2	8	0	0	9	2	×	4	
	15	1019.4	W 16	÷25.0	62	10—20	03	2	8	0	0	9	7	×	3	
	18	1024.4	W 13	÷23.2	÷20.2	..	63	20—50	02	2	8	0	0	9	7	×	4	0.0
	21	1029.1	W 7	÷21.5	63	20—50	02	2	8	0	0	9	7	×	3	
11	00	1031.3	W 6	÷23.3	63	> 50	02	2	8	0	0	9	7	×	1	
	03	1033.0	0	÷30.0	63	> 50	01	0	1	0	0	9	4	0	3	
	06	1035.4	0	÷33.0	..	÷34.9	64	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1036.0	W 3	÷33.4	64	> 50	03	0	2	0	0	9	5	4	1	
	12	1037.7	0	÷34.4	65	> 50	02	0	2	0	0	9	0	4	1	
	15	1038.0	W 7	÷26.9	66	> 50	00	0	0	0	0	9	0	0	1	
	18	1038.6	WSW 1	÷27.0	÷19.4	..	65	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1039.5	0	÷31.0	64	> 50	00	0	0	0	0	9	0	0	3	
12	00	1040.5	0	÷32.0	64	> 50	00	0	0	0	0	9	0	0	3	
	03	1040.8	0	÷34.5	64	> 50	00	0	0	0	0	9	0	0	1	
	06	1040.3	W 2	÷34.7	..	÷35.6	64	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1040.5	0	÷34.7	64	> 50	00	0	0	0	0	9	0	0	4	
	12	1040.5	0	÷34.1	65	> 50	00	0	0	0	0	9	0	0	3	
	15	1040.5	0	÷36.0	65	> 50	00	0	0	0	0	9	0	0	3	
	18	1041.2	0	÷35.1	÷31.0	..	65	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1040.5	NW'W1	÷34.9	66	> 50	00	0	0	0	0	9	0	0	9	
13	00	1042.0	0	÷34.7	66	> 50	00	0	0	0	0	9	0	0	4	
	03	1042.2	W 3	÷35.2	66	> 50	00	0	0	0	0	9	0	0	1	
	06	1042.2	0	÷35.0	..	÷36.3	66	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1042.0	W 1	÷35.6	68	> 50	00	0	0	0	0	9	0	0	9	
	12	1041.5	0	÷35.3	68	> 50	00	0	0	0	0	9	0	0	8	
	15	1039.9	W 2	÷33.9	68	> 50	00	0	0	0	0	9	0	0	9	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
14	18	1038.8	W 3	÷33.2	÷33.2	..	68	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1039.9	W 6	÷33.1	68	> 50	00	0	0	0	0	9	0	0	8	
	00	1037.8	WNW 3	÷33.8	68	> 50	00	0	0	0	0	9	0	0	6	
	03	1038.1	W 5	÷31.3	68	> 50	00	0	0	0	0	9	0	0	4	
	06	1038.2	W 4	÷30.7	..	÷36.2	69	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1038.2	W 5	÷31.5	68	> 50	00	0	0	0	0	9	0	0	3	
	12	1037.6	WSW 3	÷30.6	68	> 50	00	0	0	0	0	9	0	0	9	
	15	1037.3	W 1	÷31.9	68	> 50	00	0	0	0	0	9	0	0	8	
15	18	1037.6	W 1	÷34.0	÷30.2	..	67	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1038.1	W 1	÷34.6	67	> 50	00	0	0	0	0	9	0	0	4	
	00	1038.1	0	÷33.6	68	> 50	00	0	0	0	0	9	0	0	3	
	03	1037.6	0	÷32.3	68	> 50	00	0	0	0	0	9	0	0	9	
	06	1036.8	W 6	÷28.6	..	÷35.1	68	> 50	03	0	3	0	0	9	3	0	8	0.0
	09	1035.5	W 5	÷29.4	68	> 50	03	2	8	0	0	9	3	7	8	
	12	1034.6	W 6	÷27.5	68	> 50	02	2	8	0	0	9	4	7	8	
	15	1032.1	W 6	÷26.7	68	> 50	01	2	6	0	0	9	4	7	9	
16	18	1031.0	W 6	÷26.8	÷25.1	..	67	> 50	01	2	4	0	0	9	4	9	6	0.0
	21	1029.8	W 5	÷27.6	67	> 50	01	0	1	0	0	9	4	0	8	
	00	1029.6	0	÷30.4	67	> 50	02	0	1	0	0	9	4	0	6	
	03	1029.0	0	÷31.6	67	> 50	00	0	0	0	0	9	0	0	8	
	06	1027.5	0	÷32.6	..	÷32.6	68	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1026.7	0	÷33.9	68	> 50	00	0	0	0	0	9	0	0	6	
	12	1025.8	0	÷33.5	68	> 50	00	0	0	0	0	9	0	0	8	
	15	1022.2	W 5	÷29.7	69	> 50	00	0	0	0	0	9	0	0	9	
17	18	1020.9	W 3	÷30.8	÷26.9	..	69	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1019.4	W 5	÷31.6	69	> 50	00	0	0	0	0	9	0	0	8	
	00	1018.1	0	÷31.2	69	> 50	00	0	0	0	0	9	0	0	8	
	03	1017.0	0	÷30.6	69	> 50	00	0	0	0	0	9	0	0	8	
	06	1015.5	0	÷32.2	..	÷34.3	69	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1015.8	0	÷33.5	69	> 50	02	0	1	0	0	9	4	9	4	
	12	1016.1	SW 1	÷34.0	70	> 50	02	0	1	0	0	9	0	1	3	
	15	1016.0	0	÷33.0	70	> 50	02	0	1	0	0	9	0	1	9	
18	18	1015.5	0	÷34.1	÷27.3	..	70	> 50	02	0	1	0	0	9	0	1	9	0.0
	21	1015.7	0	÷34.4	70	> 50	02	0	1	0	0	9	4	0	8	
	00	1013.9	0	÷35.2	70	> 50	00	0	0	0	0	9	0	0	9	
	03	1012.3	0	÷36.1	70	> 50	00	0	0	0	0	9	0	0	8	
	06	1010.9	0	÷33.8	..	÷37.1	70	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1009.6	0	÷34.7	70	> 50	00	0	0	0	0	9	0	0	8	
	12	1007.1	0	÷33.7	70	> 50	03	0	2	0	0	9	0	5	9	
	15	1003.7	0	÷30.9	70	> 50	03	2	6	0	0	9	0	6	8	
19	18	1000.5	0	÷29.0	÷29.0	..	71	20—50	02	2	8	3	6	3	2	×	8	0.0
	21	996.9	0	÷27.2	71	4—10	71	7	8	8	7	2	×	×	8	
	00	993.9	W 3	÷25.5	71	4—10	71	7	8	8	7	2	×	×	8	
	03	989.9	SSW 4	÷24.0	71	> 50	02	2	6	3	6	3	5	0	9	
	06	987.3	0	÷24.3	..	÷29.0	72	4—10	70	7	8	8	7	5	×	×	6	—
	09	987.4	W 10	÷26.8	73	10—20	01	0	4	0	0	9	4	9	4	
	12	990.7	W 12	÷26.4	79	4—10	36	3	7	0	0	9	7	×	4	
	15	992.7	W 9	÷27.9	79	20—50	02	2	6	0	0	9	7	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
20	18	993.4	W 4	÷26.8	÷23.8	..	75	> 50	02	2	6	0	0	9	4	×	1	0.3 ¹	
	21	993.6	W 5	÷27.0	72	> 50	02	2	7	0	0	9	7	×	3		
	00	993.9	WSW 5	÷26.3	70	20-50	02	2	8	0	0	9	7	×	3		
	03	994.9	NE 5	÷24.4	71	20-50	03	2	7	7	5	5	×	×	3		
	06	994.9	0	÷25.0	..	÷27.9	×	20-50	02	2	8	8	6	5	×	×	3		0.0
	09	996.6	0	÷26.0	×	10-20	77	2	8	8	6	3	×	×	4		
21	12	997.7	W 4	÷23.0	×	20-50	02	2	8	8	6	3	×	×	3	trace	
	15	1000.0	W 6	÷19.6	×	> 50	02	2	7	0	0	9	4	0	4		
	18	1001.6	WSW 9	÷20.2	÷17.8	..	×	> 50	02	2	3	0	0	9	4	0	3		
	21	1002.2	WSW 7	÷21.1	×	> 50	02	0	3	0	0	9	4	0	1		
	00	1002.2	WSW 4	÷22.2	×	> 50	02	0	2	0	0	9	5	0	3		
	03	1001.6	WSW 2	÷23.7	×	> 50	03	0	5	0	0	9	5	4	9		
22	06	1001.3	0	÷25.4	..	÷26.3	×	> 05	01	0	2	0	0	9	0	8	8	0.0	
	09	1000.6	0	÷27.1	×	> 50	03	2	6	0	0	9	4	9	9		
	12	1000.9	W 1	÷25.2	×	> 50	03	2	8	0	0	9	1	×	4		
	15	1000.4	0	÷26.6	×	> 50	01	0	1	0	0	9	0	9	9		
	18	1000.0	W 3	÷33.5	÷19.4	..	×	> 50	02	0	1	0	0	9	4	9	9		
	21	1000.4	0	÷27.8	×	> 50	02	0	1	0	0	9	4	0	4		
23	00	1000.9	0	÷27.0	×	> 50	02	0	1	0	0	9	4	0	3	0.0	
	03	1001.2	W 4	÷23.5	×	> 50	02	0	1	0	0	9	4	0	3		
	06	1001.2	0	÷24.8	..	÷33.5	×	> 50	00	0	0	0	0	9	0	0	3		
	09	1001.8	0	÷25.5	×	> 50	00	0	0	0	0	9	0	0	3		
	12	1001.8	W 3	÷26.1	×	> 50	00	0	0	0	0	9	0	0	3		
	15	1001.2	0	÷26.2	×	> 50	00	0	0	0	0	9	0	0	9		
24	18	1000.3	W 3	÷26.1	÷23.2	..	70	> 50	00	0	0	0	0	9	0	0	8	0.0	
	21	1000.6	0	÷27.5	73	> 50	00	0	0	0	0	9	0	0	4		
	00	1001.5	0	÷30.5	75	> 50	00	0	0	0	0	9	0	0	4		
	03	1003.3	0	÷29.0	77	> 50	00	0	0	0	0	9	0	0	4		
	06	1004.6	0	÷28.5	..	÷31.2	78	> 50	03	0	1	0	0	9	4	0	3		
	09	1007.1	0	÷27.6	79	> 50	02	0	1	0	0	9	4	0	4		
25	12	1009.1	W 3	÷26.6	79	> 50	03	2	4	0	0	9	0	8	3	0.0	
	15	1011.7	0	÷27.2	80	> 50	02	2	3	0	0	9	0	8	3		
	18	1012.3	0	÷29.3	÷25.9	..	80	> 50	02	0	3	0	0	9	0	8	1		
	21	1013.8	0	÷30.4	80	> 50	01	0	1	0	0	9	0	1	4		
	00	1015.4	0	÷31.6	80	> 50	02	0	1	0	0	9	0	1	3		
	03	1016.1	SSW 1	÷33.0	81	> 50	02	0	1	0	0	9	0	1	1		
26	06	1017.9	WSW 2	÷34.5	..	÷35.0	82	> 50	00	0	0	0	0	9	0	0	1	0.0	
	09	1017.9	WSW 2	÷34.8	82	> 50	00	0	0	0	0	9	0	0	3		
	12	1017.9	0	÷34.0	82	> 50	00	0	0	0	0	9	0	0	3		
	15	1018.2	SW'W 3	÷32.0	82	> 50	00	0	0	0	0	9	0	0	4		
	18	1017.9	SW 3	÷32.8	÷29.5	..	82	> 50	00	0	0	0	0	9	0	0	7		
	21	1018.1	0	÷35.1	82	> 50	02	0	1	0	0	9	0	2	4		
27	00	1018.1	0	÷34.8	82	> 50	00	0	0	0	0	9	0	0	3	0.0	
	03	1017.8	0	÷35.3	82	> 50	00	0	0	0	0	9	0	0	9		
	06	1017.2	W 3	÷33.1	..	÷36.1	82	> 50	03	0	3	0	0	9	0	5	8		
	09	1017.4	W 2	÷32.2	82	> 50	02	2	4	0	0	9	0	8	4		
	12	1017.9	W 1	÷30.7	82	> 50	01	0	1	0	0	9	0	1	3		
	15	1017.3	W 7	÷27.5	80	> 50	00	0	0	0	0	9	0	0	9		

¹ For the 24 hours.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
26	18	1016.9	W 10	÷26.0	÷26.0	..	80	> 50	00	0	0	0	0	9	0	0	8	0.0	
	21	1017.5	W 9	÷24.8	80	> 50	00	0	0	0	0	9	0	0	4		
	00	1017.9	W 7	÷25.6	78	> 50	00	0	0	0	0	9	0	0	3		
	03	1018.2	W 12	÷25.0	79	> 50	02	0	1	0	0	9	0	1	3		
	06	1017.9	W 14	÷24.5	..	÷33.0	79	> 50	00	0	0	0	0	9	0	0	9	0.0	
	09	1018.2	W 15	÷24.8	78	> 50	03	0	5	0	0	9	0	6	4		
	12	1017.6	W 14	÷23.6	82	> 50	02	2	5	0	0	9	5	5	9		
	15	1017.8	W 15	÷23.3	82	> 50	02	2	7	0	0	9	7	×	1		
	18	1017.6	W 15	÷22.5	÷21.1	82	> 50	02	2	8	0	0	9	2	×	9	0.0
27	21	1017.6	W 15	÷22.5	84	10—20	02	2	8	8	6	2	×	×	3		
	00	1017.9	W 15	÷22.5	88	1—2	02	2	8	8	6	2	×	×	4		
	03	1018.4	W 15	÷22.5	92	1—2	02	2	8	8	6	2	×	×	3		
	06	1018.1	W 13	÷22.5	..	÷24.9	92	1—2	02	2	8	0	0	9	7	×	9	0.0	
	09	1018.5	W 14	÷22.3	92	0.5—1	02	2	8	0	0	9	7	×	4		
	12	1019.2	W 16	÷21.4	92	1—2	02	2	8	0	0	9	7	×	4		
	15	1019.6	W 15	÷21.3	92	1—2	02	2	8	0	0	9	7	×	3		
	18	1020.1	W 15	÷20.3	÷19.5	92	2—4	02	2	8	8	6	4	×	×	3	0.0
	21	1020.1	W 4	÷19.3	92	10—20	02	2	8	0	0	9	7	×	3		
28	00	1020.6	W 7	÷20.4	92	20—50	02	2	8	0	0	9	2	×	4		
	03	1021.3	W 5	÷21.3	×	20—50	02	2	8	0	0	9	2	×	3		
	06	1021.3	W 5	÷21.5	..	÷22.5	×	> 50	02	2	8	0	0	9	2	×	3	0.0	
	09	1021.0	W 5	÷22.1	×	> 50	02	2	8	0	0	9	2	×	9		
	12	1020.6	W 5	÷20.8	×	> 50	02	2	8	0	0	9	0	7	3		
	15	1020.3	W 5	÷21.2	×	> 50	02	2	6	0	0	9	5	2	3		
	18	1019.6	W 5	÷21.6	÷18.7	..	×	> 50	01	2	3	0	0	9	4	2	9	0.0	
	21	1018.6	W 2	÷23.7	×	> 50	00	0	0	0	0	9	0	0	8		
	00	1017.4	0	÷25.3	×	> 50	00	0	0	0	0	9	0	0	3		
29	03	1016.1	0	÷26.5	×	> 50	00	0	0	0	0	9	0	0	3		
	06	1015.4	0	÷28.3	..	÷28.5	×	> 50	02	1	1	0	0	9	0	1	9	0.0	
	09	1014.9	0	÷28.1	68	> 50	03	2	8	0	0	9	1	×	8		
	12	1014.4	0	÷27.7	68	> 50	02	2	8	0	0	9	1	×	8		
	15	1014.0	E 3	÷26.5	70	> 50	01	2	6	0	0	9	4	2	8		
	18	1014.0	E 4	÷27.5	÷21.7	..	71	> 50	02	2	6	0	0	9	4	2	3	0.0	
	21	1013.8	E 5	÷26.8	73	> 50	01	2	4	0	0	9	4	2	9		
	00	1013.2	E 4	÷27.8	83	> 50	01	0	2	0	0	9	4	0	9		
	03	1013.4	E 1	÷29.5	75	> 50	03	2	4	0	0	9	4	2	4		
30	06	1013.4	W 4	÷28.2	..	÷29.7	75	> 50	02	2	4	0	0	9	4	0	3	0.0	
	09	1013.5	WSW 3	÷28.5	76	> 50	02	2	4	0	0	9	4	2	3		
	12	1013.5	WSW 4	÷27.3	76	> 50	03	2	7	0	0	9	3	×	3		
	15	1013.2	W 2	÷25.5	75	> 50	02	2	7	0	0	9	3	×	9		
	18	1013.7	SE'E 2	÷25.7	÷25.1	..	75	20—50	02	2	8	0	0	9	3	×	4	0.0	
	21	1013.3	E 1	÷26.3	76	20—50	02	2	8	0	0	9	3	×	9		
	00	1012.7	0	÷27.3	77	20—50	01	2	6	0	0	9	4	0	8		
	03	1012.2	0	÷27.5	77	10—20	70	7	8	0	0	9	2	×	8		
	06	1011.8	W 2	÷28.3	..	÷28.5	78	10—20	70	7	8	0	0	9	2	×	8	trace	
31	09	1010.1	0	÷27.5	78	10—20	70	7	8	0	0	9	3	×	8		
	12	1010.7	0	÷27.5	78	10—20	02	2	8	0	0	9	3	×	8		
	15	1010.6	0	÷26.0	77	10—20	02	2	8	0	0	9	3	×	6		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1010.4	0	÷25.8	÷25.8	..	78	4—10	70	7	8	0	0	9	3	×	8	trace
	21	1010.1	W 2	÷25.8	78	2—4	71	7	8	0	0	9	3	×	8	
Mean		1015.3	5.3	÷29.0	÷25.7	÷32.2	74	×

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1009.6	0	÷26.4	78	4—10	71	7	8	0	0	9	3	×	8	
	03	1009.1	0	÷26.7	79	4—10	71	7	8	8	6	5	×	×	8	
	06	1008.8	W 1	÷26.2	..	÷28.9	79	4—10	71	7	8	8	6	5	×	×	8	trace
	09	1009.9	E 2	÷25.8	79	4—10	71	7	8	8	6	5	×	×	9	
	12	1008.0	E 4	÷26.5	80	4—10	71	7	8	8	6	5	×	×	4	
	15	1007.7	E 4	÷26.7	80	4—10	71	7	8	8	6	5	×	×	9	
	18	1008.2	0	÷28.1	÷25.6	..	81	10—20	01	2	6	0	0	9	3	8	4	0.4
	21	1009.7	W 2	÷27.3	80	4—10	71	7	8	8	6	5	×	×	4	
2	00	1010.4	W 4	÷26.6	80	4—10	71	7	8	8	6	5	×	×	3	
	03	1012.0	W 7	÷25.2	80	4—10	71	7	8	8	6	5	×	×	4	
	06	1014.6	W 6	÷25.3	..	÷28.5	79	4—10	71	7	8	8	6	5	×	×	3	0.2
	09	1016.5	W 8	÷25.0	79	4—10	71	7	8	8	6	5	×	×	3	
	12	1017.0	W 6	÷22.7	78	10—20	01	2	8	0	0	9	1	×	1	
	15	1018.2	W 2	÷22.3	75	> 50	01	0	2	0	0	9	0	2	3	
	18	1019.5	E 4	÷25.9	÷22.3	..	75	> 50	01	0	1	0	0	9	0	1	3	0.1
	21	1021.0	0	÷29.4	75	> 50	02	0	1	0	0	9	4	0	3	
3	00	1021.5	0	÷29.8	78	> 50	02	0	1	0	0	9	4	0	1	
	03	1022.1	0	÷31.3	78	> 50	00	0	0	0	0	9	0	0	3	
	06	1022.5	0	÷32.0	..	÷32.7	78	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1022.7	0	÷30.8	78	> 50	00	0	0	0	0	9	0	0	1	
	12	1022.6	W 2	÷30.7	80	> 50	00	0	0	0	0	9	0	0	9	
	15	1023.0	0	÷29.0	80	> 50	00	0	0	0	0	9	0	0	4	
	18	1023.8	0	÷28.1	÷26.0	..	77	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1022.5	0	÷29.7	75	> 50	00	0	0	0	0	9	0	0	9	
4	00	1022.9	0	÷31.6	75	> 50	02	0	1	0	0	9	0	1	4	
	03	1024.2	W 1	÷32.2	76	> 50	02	0	1	0	0	9	0	1	4	
	06	1024.7	0	÷32.6	..	÷32.8	76	> 50	02	0	1	0	0	9	0	1	1	0.0
	09	1025.2	W 2	÷32.5	76	> 50	02	0	1	0	0	9	0	0	3	
	12	1026.0	0	÷31.5	76	> 50	02	0	1	0	0	9	0	1	3	
	15	1026.7	W 5	÷28.4	75	10—20	05 ¹	0	0	0	0	9	0	0	3	
	18	1026.8	W 4	÷29.8	÷28.0	..	75	10—20	05 ¹	0	0	0	0	9	0	0	1	0.0
	21	1027.8	0	÷29.8	75	> 50	02	0	1	0	0	9	0	1	4	
5	00	1028.2	0	÷32.7	75	> 50	02	0	1	0	0	9	0	1	3	
	03	1028.1	0	÷33.2	77	> 50	02	0	1	0	0	9	0	1	9	
	06	1028.3	0	÷34.0	..	÷34.2	78	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1028.2	0	÷33.6	78	> 50	00	0	0	0	0	9	0	0	9	
	12	1028.5	0	÷33.5	77	> 50	00	0	0	0	0	9	0	0	4	
	15	1028.1	0	÷32.8	76	> 50	00	0	0	0	0	9	0	0	9	
	18	1027.5	0	÷33.0	÷28.2	..	76	> 50	00	0	0	0	0	9	0	0	8	0.0

¹ Solar halo and parhelia.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	21	1027.2	0	÷34.4	77	> 50	00	0	0	0	0	9	0	0	8	
6	00	1027.1	0	÷35.2	78	> 50	00	0	0	0	0	9	0	0	8	
	03	1025.4	0	÷35.6	78	> 50	03	0	1	0	0	9	0	5	9	
	06	1024.5	0	÷35.9	..	÷36.3	78	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1023.3	0	÷35.2	78	> 50	00	0	0	0	0	9	0	0	8	
	12	1022.5	0	÷31.8	78	> 50	00	0	0	0	0	9	0	0	8	
	15	1020.8	0	÷32.9	75	> 50	00	0	0	0	0	9	0	0	9	
	18	1018.1	0	÷33.1	÷30.4	..	74	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1017.0	0	÷35.5	75	> 50	00	0	0	0	0	9	0	0	6	
7	00	1015.2	W 3	÷34.7	76	> 50	00	0	0	0	0	9	0	0	8	
	03	1013.7	W 4	÷35.2	76	> 50	00	0	0	0	0	9	0	0	8	
	06	1012.6	0	÷35.0	..	÷37.6	76	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1012.2	0	÷33.2	74	> 50	00	0	0	0	0	9	0	0	6	
	12	1012.1	0	÷31.0	74	> 50	00	0	0	0	0	9	0	0	8	
	15	1011.8	0	÷29.4	73	> 50	00	0	0	0	0	9	0	0	8	
	18	1012.1	W 2	÷27.6	÷27.1	..	71	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1013.2	0	÷29.5	70	> 50	00	0	0	0	0	9	0	0	4	
8	00	1014.6	0	÷31.2	69	> 50	00	0	0	0	0	9	0	0	3	
	03	1016.2	0	÷34.1	70	> 50	00	0	0	0	0	9	0	0	3	
	06	1016.4	0	÷34.6	..	÷34.8	70	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1017.4	0	÷34.7	72	> 50	02	0	1	0	0	9	0	1	4	
	12	1018.3	0	÷33.9	72	> 50	00	0	0	0	0	9	0	0	3	
	15	1019.4	0	÷32.0	71	> 50	00	0	0	0	0	9	0	0	3	
	18	1020.8	0	÷32.1	÷27.4	..	71	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1022.3	0	÷31.8	72	> 50	00	0	0	0	0	9	0	0	3	
9	00	1023.4	0	÷33.2	72	> 50	02	0	1	0	0	9	0	1	3	
	03	1025.2	W 2	÷33.3	73	> 50	03	0	2	0	0	9	0	6	4	
	06	1026.4	W 1	÷33.0	..	÷34.7	72	> 50	03	0	3	0	0	9	0	5	1	0.0
	09	1027.4	0	÷31.8	72	> 50	03	2	6	0	0	9	0	6	3	
	12	1028.5	0	÷31.8	72	> 50	02	2	6	0	0	9	0	6	3	
	15	1029.1	0	÷30.6	70	> 50	02	2	4	0	0	9	0	6	1	
	18	1029.3	0	÷30.6	÷29.7	..	70	> 50	02	2	8	0	0	9	0	7	3	0.0
	21	1029.3	0	÷31.0	72	> 50	02 ¹	2	8	0	0	9	0	7	3	
10	00	1029.7	0	÷30.6	72	> 50	02	2	8	0	0	9	1	×	4	
	03	1031.1	W 4	÷29.1	73	20—50	02	2	8	0	0	9	2	×	4	
	06	1031.8	0	÷28.0	..	÷33.0	72	> 50	01	2	7	0	0	9	3	×	3	0.0
	09	1032.4	W 4	÷25.7	72	> 50	02	2	7	0	0	9	7	×	3	
	12	1032.6	W 4	÷24.8	72	> 50	02	2	7	0	0	9	7	×	1	
	15	1033.0	W 3	÷22.9	70	> 50	02	2	7	0	0	9	7	×	3	
	18	1033.5	W 3	÷23.8	÷21.4	..	70	> 50	02	2	8	0	0	9	7	×	3	0.0
	21	1033.6	E 3	÷24.6	72	> 50	02	2	8	0	0	9	7	×	1	
11	00	1033.2	E 2	÷24.7	74	> 50	02	2	7	0	0	9	3	×	9	
	03	1032.3	W 2	÷25.0	76	> 50	02	2	8	0	0	9	3	×	9	
	06	1031.7	W 6	÷24.6	..	÷28.0	78	20—50	02	2	8	0	0	9	2	×	8	0.0
	09	1031.1	W 7	÷23.7	75	2—4	71	7	8	8	7	3	×	×	8	
	12	1030.5	W 5	÷22.7	74	10—20	02	2	8	8	5	5	×	×	8	
	15	1030.0	W 5	÷21.9	73	4—10	02	2	8	8	6	3	×	×	8	
	18	1029.7	W 5	÷21.4	÷21.4	..	72	2—4	71	7	8	8	7	3	×	×	8	trace

¹ 0900—2100 Solar halo and 1500 parhelia toc.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	21	1029.7	W 5	÷19.6	74	2—4	71	7	8	8	7	3	×	×	3	
12	00	1029.2	W 6	÷18.2	78	20—50	02	2	8	0	0	9	7	×	9	
	03	1028.1	W 6	÷18.8	78	20—50	02	2	8	0	0	9	7	×	8	
	06	1027.3	WSW 3	÷19.4	..	÷24.7	78	2—4	71	7	8	0	0	9	7	×	8	trace
	09	1025.3	0	÷20.2	78	10—20	70	7	8	0	0	9	3	×	9	
	12	1023.7	W 4	÷20.1	79	10—20	01	2	7	0	0	9	3	×	8	
	15	1022.3	0	÷20.7	78	> 50	01	0	1	0	0	9	4	0	8	
	18	1021.1	0	÷22.4	÷17.4	..	75	> 50	02	0	3	0	0	9	0	1	8	0.3
	21	1019.4	0	÷24.8	75	> 50	02	0	3	0	0	9	0	1	8	
13	00	1017.3	0	÷25.4	75	> 50	02	0	1	0	0	9	0	1	8	
	03	1015.2	0	÷27.5	77	> 50	02	0	1	0	0	9	0	1	8	
	06	1013.3	0	÷28.7	..	÷30.3	78	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1011.1	0	÷28.7	78	> 50	02	0	4	0	0	9	5	2	8	
	12	1008.9	0	÷26.4	77	> 50	03	0	5	0	0	9	5	2	8	
	15	1006.8	0	÷25.6	75	> 50	03 ¹	2	8	0	0	9	0	7	8	
	18	1006.3	W 5	÷24.1	÷19.0	..	75	> 50	02	2	8	0	0	9	0	7	6	0.0
	21	1006.7	W 8	÷21.5	75	> 50	02	2	8	0	0	9	1	×	4	
14	00	1007.6	W 13	÷18.9	74	10—20	02	2	8	0	0	9	2	×	3	
	03	1010.6	W 15	÷19.1	75	4—10	02	2	8	0	0	9	2	×	4	
	06	1012.3	W 13	÷19.1	..	÷29.0	75	4—10	02	2	8	0	0	9	2	×	1	0.0
	09	1013.7	W 12	÷18.8	78	10—20	02	2	8	0	0	9	2	×	3	
	12	1014.0	W 12	÷18.1	72	20—50	02	2	8	0	0	9	2	×	1	
	15	1013.6	W 9	÷17.6	68	10—20	02	2	8	0	0	9	0	7	3	
	18	1013.4	W 8	÷17.4	÷17.2	..	66	10—20	02	2	8	0	0	9	0	7	9	0.0
	21	1012.2	0	÷17.7	72	10—20	02 ²	2	8	4	6	4	0	7	9	
15	00	1010.7	E 3	÷21.8	70	10—20	02	2	8	0	0	9	1	×	8	
	03	1008.2	0	÷23.2	74	> 50	01	0	2	0	0	9	4	1	9	
	06	1006.0	0	÷23.7	..	÷23.8	76	> 50	02	0	2	0	0	9	4	0	8	0.0
	09	1003.2	0	÷23.8	75	> 50	02	0	1	0	0	9	0	4	8	
	12	1001.0	0	÷22.6	75	> 50	00	0	0	0	0	9	0	0	8	
	15	999.0	W 3	÷20.7	74	> 50	00	0	0	0	0	9	0	0	8	
	18	997.4	W 4	÷19.4	÷17.3	..	69	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	997.4	W 6	÷20.1	67	> 50	00	0	0	0	0	9	0	0	3	
16	00	997.9	W 6	÷20.6	66	> 50	00	0	0	0	0	9	0	0	4	
	03	999.0	0	÷23.0	64	> 50	03	0	2	0	0	9	0	5	4	
	06	1000.2	W 10	÷14.9	..	÷23.8	64	> 50	02	0	2	0	0	9	0	1	3	0.0
	09	1002.0	W 12	÷15.6	58	> 50	02	0	2	0	0	9	0	1	3	
	12	1004.4	W 10	÷16.0	52	> 50	02	0	1	0	0	9	0	1	4	
	15	1005.4	W 9	÷15.4	52	> 50	02	0	1	0	0	9	0	1	1	
	18	1005.7	WSW 6	÷14.9	÷13.3	..	50	> 50	02	0	1	0	0	9	0	1	1	0.0
	21	1006.6	SW 2	÷15.7	48	> 50	03	2	7	0	0	9	0	6	4	
17	00	1006.2	S 2	÷19.9	49	> 50	02	2	7	0	0	9	0	6	9	
	03	1006.7	SE'E 4	÷21.7	52	> 50	01	0	1	0	0	9	0	1	4	
	06	1007.2	SE'E 5	÷21.8	..	÷23.2	54	> 50	02	0	1	0	0	9	0	1	3	0.0
	09	1007.9	SE'E 4	÷21.5	58	> 50	02	0	1	0	0	9	0	1	3	
	12	1008.7	W 1	÷21.4	58	> 50	00	0	0	0	0	9	0	0	3	
	15	1008.4	W 4	÷18.2	58	> 50	03	0	4	0	0	9	0	6	9	
	18	1009.1	SE'E 3	÷17.8	÷15.0	..	57	> 50	03	2	6	0	0	9	0	6	4	0.0

¹ 1500—1700 Solar halo.² 1500—2100 Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
18	21	1012.7	E'S 5	÷20.2	56	> 50	02 ¹	2	6	0	0	9	0	6	4	
	00	1013.9	E 4	÷21.8	56	> 50	02	2	8	0	0	9	0	7	1	
	03	1016.5	0	÷22.2	56	> 50	02 ²	2	8	0	0	9	0	7	4	
	06	1017.2	0	÷23.0	..	÷24.0	56	> 50	02	2	8	0	0	9	0	7	1	0.0
	09	1018.9	0	÷22.2	57	> 50	02	2	8	0	0	9	0	7	4	
	12	1019.6	E 3	÷20.5	62	> 50	01	0	2	0	0	9	0	8	2	
	15	1019.7	E 4	÷18.2	56	> 50	02	0	2	0	0	9	0	1	1	
	18	1019.7	E 4	÷18.4	÷17.8	..	55	> 50	02	0	1	0	0	9	0	1	3	0.0
	21	1019.7	E 4	÷21.8	56	> 50	00	0	0	0	0	9	0	0	3	
19	00	1019.5	E 6	÷23.9	60	> 50	00	0	0	0	0	9	0	0	9	
	03	1019.0	WSW 1	÷25.5	60	> 50	00	0	0	0	0	9	0	0	9	
	06	1018.8	0	÷25.9	..	÷28.2	62	> 50	00	0	0	0	0	9	0	0	0	0.0
	09	1018.6	0	÷23.2	62	> 50	00	0	0	0	0	9	0	0	8	
	12	1018.4	0	÷22.2	61	> 50	00	0	0	0	0	9	0	0	8	
	15	1018.2	0	÷21.2	58	> 50	00	0	0	0	0	9	0	0	8	
	18	1018.2	SE'E 5	÷18.8	÷18.3	..	56	> 50	02	0	1	0	0	9	0	2	3	0.0
	21	1019.3	E'S 4	÷22.5	56	> 50	03	0	3	0	0	9	0	5	4	
20	00	1019.0	SE'E 6	÷23.4	56	> 50	03	0	5	0	0	9	0	6	9	
	03	1019.2	0	÷24.5	57	> 50	00	0	0	0	0	9	0	0	4	
	06	1019.0	0	÷24.8	..	÷26.8	58	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1019.5	0	÷25.5	60	> 50	00	0	0	0	0	9	0	0	4	
..	12	1019.1	0	÷22.6	59	> 50	00	0	0	0	0	9	0	0	9	
	15	1018.8	E 1	÷20.7	57	> 50	00	0	0	0	0	9	0	0	8	
	18	1018.7	0	÷18.6	÷18.2	..	55	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	1018.3	0	÷18.9	54	> 50	00	0	0	0	0	9	0	0	7	
21	00	1017.6	0	÷20.2	55	> 50	00	0	0	0	0	9	0	0	9	
	03	1017.1	0	÷25.5	57	> 50	00	0	0	0	0	9	0	0	8	
	06	1016.6	0	÷21.3	..	÷25.7	58	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1014.1	W 5	÷17.2	56	> 50	00	0	0	0	0	9	0	0	9	
	12	1011.3	W 6	÷16.0	52	> 50	00	0	0	0	0	9	0	0	8	
	15	1007.4	W 5	÷15.0	49	> 50	00	0	0	0	0	9	0	0	8	
	18	1003.8	W 6	÷14.3	÷13.2	..	48	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1001.1	WSW 4	÷15.0	46	> 50	00	0	0	0	0	9	0	0	6	
22	00	999.6	W 6	÷17.1	47	> 50	00	0	0	0	0	9	0	0	8	
	03	1000.2	W 16	÷16.0	49	> 50	00	0	0	0	0	9	0	0	4	
	06	1004.4	W 15	÷18.1	..	÷21.5	58	> 50	00	0	0	0	0	9	0	0	4	0.0
	09	1007.7	W 15	÷19.8	58	> 50	02	0	1	0	0	9	4	0	3	
	12	1008.4	W 17	÷18.3	58	10-20	03	0	3	0	0	9	4	1	1	
	15	1009.4	W 15	÷17.7	59	10-20	02	0	3	0	0	9	4	1	3	
	18	1009.5	W 15	÷17.5	÷13.7	..	59	10-20	03	2	5	0	0	9	0	6	1	0.0
	21	1011.4	W 21	÷17.1	60	10-20	01	0	2	0	0	9	4	1	4	
23	00	1012.3	W 18	÷17.9	60	10-20	02	0	3	0	0	9	4	1	2	
	03	1014.4	W 19	÷18.9	61	20-50	02	2	6	0	0	9	0	8	4	
	06	1016.0	W 18	÷18.9	..	÷20.0	60	20-50	02	2	5	0	0	9	4	0	3	0.0
	09	1017.2	W 18	÷18.3	61	10-20	03	2	8	0	0	9	0	7	1	
	12	1017.9	W 18	÷17.4	59	10-20	02	2	8	0	0	9	0	7	3	
	15	1018.1	W 19	÷16.0	58	10-20	02	2	8	0	0	9	0	7	1	
	18	1018.2	W 16	÷15.0	÷13.8	..	54	20-50	02 ³	2	8	0	0	9	0	7	3	0.0

¹ 1800 and 2100 Solar halo.² 0003-0300 Solar halo.³ 0900-1800 Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
24	21	1018.2	W 14	÷14.5	57	> 50	02	2	8	0	0	9	7	7	3	
	00	1018.2	W 11	÷14.2	50	> 50	02	2	8	0	0	9	7	7	3	
	03	1018.0	W 6	÷14.8	48	> 50	01	2	3	0	0	9	4	2	9	
	06	1017.0	SW 4	÷15.4	..	÷19.2	50	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1015.5	WSW 1	÷16.2	50	> 50	02	0	1	0	0	9	0	1	9	
	12	1014.1	E 5	÷14.7	52	> 50	02	0	1	0	0	9	0	1	8	
25	15	1011.6	E 6	÷15.0	58	> 50	02	0	1	0	0	9	0	1	9	
	18	1012.6	E 4	÷15.4	÷14.0	..	62	> 50	03	2	8	0	0	9	2	×	4	0.0
	21	1017.9	W 17	÷14.7	60	20-50	02	2	8	0	0	9	7	×	4	
	00	1023.2	W 16	÷16.3	64	10-20	02	2	8	0	0	9	7	×	3	
	03	1029.0	W 15	÷17.4	65	10-20	02	2	8	0	0	9	7	×	3	
	06	1031.3	W 15	÷18.1	..	÷18.5	65	10-20	02	2	8	0	0	9	7	×	1	0.0
26	09	1034.6	W 18	÷17.5	65	10-20	02	2	8	0	0	9	2	×	4	
	12	1036.5	W 14	÷17.2	66	10-20	02 ¹	2	8	0	0	9	0	7	1	
	15	1037.7	W 15	÷15.8	58	10-20	02 ¹	2	8	0	0	9	4	7	3	
	18	1038.7	W 15	÷15.9	÷14.2	..	55	20-50	02 ¹	2	8	0	0	9	4	7	3	0.0
	21	1039.9	W 10	÷15.5	54	> 50	00	2	0	0	0	9	0	0	3	
	00	1039.9	W 9	÷17.0	54	> 50	02	0	2	0	0	9	4	0	3	
27	03	1040.1	W 8	÷17.3	55	> 50	02	0	2	0	0	9	0	2	4	
	06	1039.6	W 8	÷16.8	..	÷18.5	54	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1039.0	W 11	÷15.8	52	> 50	00	0	0	0	0	9	0	0	8	
	12	1038.5	W 8	÷15.0	50	> 50	00	0	0	0	0	9	0	0	8	
	15	1038.5	W 10	÷13.7	48	> 50	00	0	0	0	0	9	0	0	3	
	18	1038.1	W 14	÷13.5	÷12.8	..	47	> 50	00	0	0	0	0	9	0	0	9	0.0
28	21	1037.9	W 14	÷14.0	46	> 50	03	0	2	0	0	9	4	2	8	
	00	1037.7	W 10	÷15.6	48	> 50	02	0	1	0	0	9	4	0	8	
	03	1037.9	W 11	÷16.1	54	> 50	03	0	3	0	0	9	4	2	4	
	06	1037.3	W 14	÷15.0	..	÷16.6	55	> 50	03 ¹	2	8	0	0	9	4	7	9	0.0
	09	1036.8	W 15	÷14.2	54	> 50	02	2	8	0	0	9	7	×	8	
	12	1036.4	W 14	÷13.9	58	> 50	01	2	3	0	0	9	4	0	8	
29	15	1036.4	W 12	÷12.5	55	> 50	02	0	3	0	0	9	4	0	3	
	18	1035.9	W 15	÷12.8	÷12.1	..	56	> 50	02	0	3	0	0	9	4	0	9	0.0
	21	1036.3	W 9	÷12.8	59	> 50	02	0	3	0	0	9	4	0	4	
	00	1035.5	W 10	÷13.5	60	> 50	03	0	7	0	0	9	4	6	9	
	03	1034.7	W 9	÷13.5	60	> 50	02	2	8	0	0	9	4	7	8	
	06	1034.0	W 7	÷13.4	..	÷15.4	59	> 50	01	0	4	0	0	9	0	1	8	0.0
30	09	1032.5	W 8	÷11.9	57	> 50	01	0	3	0	0	9	0	1	9	
	12	1032.5	W 6	÷11.0	56	> 50	02	0	2	0	0	9	0	1	3	
	15	1030.5	W 7	÷10.2	53	> 50	02	0	2	0	0	9	0	1	9	
	18	1029.5	E 6	÷14.5	÷9.3	..	58	> 50	02	0	2	0	0	9	0	1	6	0.0
	21	1029.0	E 5	÷14.5	62	> 50	00	0	0	0	0	9	0	0	6	
	00	1028.5	E 5	÷15.5	61	> 50	00	0	0	0	0	9	0	0	8	
31	03	1027.5	E 6	÷16.6	61	> 50	00	0	0	0	0	9	0	0	9	
	06	1027.5	E 6	÷15.5	..	÷16.8	62	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1027.6	E 3	÷16.7	60	> 50	00	0	0	0	0	9	0	0	4	
	12	1027.9	0	÷16.0	60	> 50	00	0	0	0	0	9	0	0	3	
	15	1027.6	E 3	÷15.2	61	> 50	00	0	0	0	0	9	0	0	8	
	18	1027.3	E 5	÷15.0	÷13.9	..	62	> 50	00	0	0	0	0	9	0	0	8	0.0

¹ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
30	21	1027.7	E 6	÷15.8	62	> 50	00	0	0	0	0	9	0	0	4	0.0	
	00	1028.8	E 5	÷17.2	63	> 50	00	0	0	0	0	9	0	0	3		
	03	1029.0	E 4	÷18.5	65	> 50	00	0	0	0	0	9	0	0	1		
	06	1029.0	E 4	÷18.2	..	÷19.2	68	> 50	00	0	0	0	0	9	0	0	3		
	09	1029.6	E 3	÷17.6	69	> 50	03 ¹	0	3	0	0	9	0	6	4		
	12	1029.4	E 1	÷16.7	68	> 50	03 ¹	2	8	0	0	9	0	7	9		
	15	1029.0	E 5	÷16.5	66	> 50	02 ¹	2	8	0	0	9	0	7	8		
	18	1029.0	E 4	÷16.7	÷14.9	66	> 50	02 ¹	2	8	0	0	9	0	7		3
	21	1029.0	E 5	÷16.7	68	> 50	02 ¹	2	8	0	0	9	0	7	3		
Mean	1020.4	4.8	÷22.7	÷19.1	÷26.2	66	1.0	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1028.5	E 5	÷17.4	68	> 50	02 ¹	2	8	0	0	9	0	7	9	0.0
	03	1028.5	E 3	÷17.5	69	> 50	02 ¹	2	8	0	0	9	0	7	3	
	06	1028.2	0	÷17.0	..	÷18.5	69	> 50	02 ¹	2	8	0	0	9	0	7	9	
	09	1028.0	0	÷16.2	71	> 50	02 ¹	2	8	0	0	9	0	7	8	
	12	1028.0	0	÷14.8	69	> 50	02 ¹	2	8	0	0	9	0	7	3	
	15	1027.4	0	÷14.0	67	> 50	02 ¹	2	8	0	0	9	0	7	9	
	18	1027.0	0	÷13.2	÷13.0	..	66	> 50	02 ¹	2	8	0	0	9	0	7	8	
	21	1026.5	SE'E 4	÷13.4	68	> 50	02 ¹	2	8	0	0	9	0	7	8	
	2	00	1026.0	0	÷15.0	73	> 50	02 ¹	2	8	0	0	9	0	7	
03		1025.6	E 3	÷16.0	76	> 50	02 ¹	2	8	0	0	9	0	7	8	
06		1024.9	E 1	÷17.0	..	÷18.0	76	> 50	02	0	2	0	0	9	0	2	8	
09		1023.9	0	÷16.2	73	> 50	02	0	1	0	0	9	0	1	8	
12		1022.8	E 1	÷14.3	72	> 50	00	0	0	0	0	9	0	0	8	
15		1021.2	E 3	÷13.2	70	> 50	00	0	0	0	0	9	0	0	9	
18		1020.0	E 5	÷13.6	÷11.1	..	70	> 50	00	0	0	0	0	9	0	0	8	
21		1018.7	E 5	÷15.0	69	> 50	00	0	0	0	0	9	0	0	8	
3		00	1018.3	E 5	÷15.6	70	> 50	00	0	0	0	0	9	0	0	6
	03	1018.3	E 3	÷17.5	72	> 50	00	0	0	0	0	9	0	0	3	
	06	1018.3	E 4	÷16.9	..	÷17.9	72	> 50	02	0	3	0	0	9	0	2	3	
	09	1017.9	E 1	÷16.4	70	> 50	03 ¹	2	8	0	0	9	0	7	9	
	12	1017.9	E 4	÷15.5	70	> 50	02 ¹	2	8	0	0	9	0	7	3	
	15	1017.9	E 5	÷16.0	70	> 50	02 ¹	2	8	0	0	9	0	7	3	
	18	1018.1	E 6	÷16.4	÷13.5	..	70	> 50	77 ¹	7	8	8	7	3	0	7	4	
	21	1018.1	E 7	÷16.6	72	> 50	77 ¹	7	8	8	7	3	0	7	3	
	4	00	1018.1	E 6	÷17.6	72	10—20	77 ¹	7	8	8	7	3	0	7	3
03		1018.1	E 6	÷19.3 ¹	73	> 50	00	2	0	0	0	9	0	0	3	
06		1017.9	E 6	÷19.2	..	÷19.7	73	> 50	02	0	1	0	0	9	4	0	9	
09		1016.9	E 6	÷19.0	74	> 50	02	0	1	0	0	9	4	0	9	
12		1016.3	E 6	÷18.8	73	> 50	03	0	3	0	0	9	5	0	8	
15		1014.5	E 6	÷18.4	74	> 50	02	0	1	1	5	3	4	0	9	
18		1013.8	E 4	÷17.8	÷16.3	..	74	> 50	00	0	0	0	0	9	0	0	6	
21		1014.0	E 1	÷17.8	73	> 50	00	0	0	0	0	9	0	0	4	

¹ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
5	00	1014.0	E 1	÷18.0	73	> 50	00	0	0	0	0	9	0	0	3	0.0
	03	1014.0	0	÷18.7	74	> 50	00	0	0	0	0	9	0	0	3	
	06	1014.2	0	÷17.0	..	÷19.3	71	> 50	00	0	0	0	0	9	0	0	4	
	09	1014.6	0	÷16.0	70	> 50	02	0	3	0	0	9	0	2	2	
	12	1015.2	W 5	÷12.4	62	> 50	00	0	0	0	0	9	0	0	3	
6	15	1016.2	W 5	÷10.4	54	> 50	00	0	0	0	0	9	0	0	4	0.0
	18	1018.1	E 4	÷ 9.8	÷ 8.4	..	48	> 50	00	0	0	0	0	9	0	0	4	
	21	1019.3	E 6	÷12.5	52	> 50	00	0	0	0	0	9	0	0	1	
	00	1020.8	E 6	÷14.3	54	> 50	03	0	1	0	0	9	5	0	3	
	03	1020.8	E 6	÷14.3	57	> 50	03 ¹	0	8	0	0	9	0	7	3	
7	06	1020.1	E 7	÷15.4	..	÷17.0	58	> 50	03 ¹	0	5	0	0	9	5	6	9	0.0
	09	1018.9	E 6	÷14.8	59	> 50	00	0	0	0	0	9	0	0	8	
	12	1017.4	E 2	÷15.7	60	> 50	02	0	1	0	0	9	5	0	8	
	15	1014.9	NE'E 1	÷13.3	58	> 50	02	0	3	0	0	9	0	2	9	
	18	1012.6	0	÷11.0	÷11.0	..	57	> 50	02	0	1	0	0	9	0	2	8	
8	21	1011.7	W 2	÷ 7.5	52	> 50	02	0	1	0	0	9	5	0	4	0.0
	00	1011.9	W 7	÷ 7.3	47	> 50	00	0	0	0	0	9	0	0	4	
	03	1013.7	W 7	÷ 9.6	51	> 50	00	0	0	0	0	9	0	0	4	
	06	1015.5	E 5	÷ 9.8	..	÷16.1	52	> 50	00	0	0	0	0	9	0	0	3	
	09	1017.5	E 6	÷11.8	54	> 50	00	0	0	0	0	9	0	0	3	
9	12	1019.8	E 6	÷13.5	56	> 50	00	0	0	0	0	9	0	0	3	0.0
	15	1021.2	E 6	÷13.5	59	> 50	00	0	0	0	0	9	0	0	1	
	18	1022.0	E 6	÷13.2	÷ 5.7	..	61	> 50	00	0	0	0	0	9	0	0	3	
	21	1023.5	E 4	÷13.2	61	> 50	03	0	1	0	0	9	5	0	4	
	00	1023.6	E 3	÷13.0	62	> 50	01	0	1	0	0	9	4	0	1	
10	03	1023.6	0	÷15.0	60	> 50	02	0	2	0	0	9	0	2	3	0.0
	06	1023.6	E 4	÷12.7	..	÷15.5	65	> 50	03 ¹	2	8	0	0	9	0	7	3	
	09	1024.4	E 4	÷13.0	68	> 50	02 ¹	2	8	0	0	9	0	7	4	
	12	1024.4	0	÷12.7	66	> 50	02 ¹	2	8	0	0	9	0	7	3	
	15	1024.4	E 5	÷11.8	63	> 50	02 ¹	2	8	0	0	9	0	7	3	
11	18	1024.4	E 4	÷11.2	÷11.2	..	61	20—50	02 ¹	2	8	0	0	9	0	7	3	0.0
	21	1024.1	E 4	÷11.0	61	20—50	02 ²	2	8	0	0	9	0	7	9	
	00	1024.1	0	÷11.0	64	20—50	02 ¹	2	8	0	0	9	0	7	3	
	03	1023.6	0	÷11.4	66	20—50	02 ¹	2	8	0	0	9	4	7	9	
	06	1023.3	E 5	÷11.4	..	÷13.4	67	20—50	02 ¹	2	8	0	0	9	0	7	8	
12	09	1023.5	E 5	÷11.2	67	> 50	02 ¹	2	8	1	6	3	0	7	4	0.0
	12	1023.5	E 6	÷11.2	69	10—20	71 ¹	7	8	8	6	3	0	7	3	
	15	1022.9	E 5	÷11.2	71	20—50	71 ¹	7	8	8	6	3	0	7	9	
	18	1022.3	E 4	÷11.5	÷10.8	..	72	10—20	71 ¹	7	7	5	6	2	0	5	8	
	21	1022.0	E 5	÷12.8	72	4—10	71 ¹	7	8	8	6	2	×	×	8	
13	00	1022.0	E 4	÷13.4	73	> 50	71 ¹	7	8	5	6	3	0	7	3	trace
	03	1022.0	E 5	÷14.4	73	10—20	71 ¹	7	8	8	6	3	0	7	3	
	06	1022.0	E 4	÷14.8	..	÷14.8	73	10—20	71	7	8	8	6	3	0	7	3	
	09	1022.0	E 4	÷14.5	73	> 50	00	2	0	0	0	9	0	0	3	
	12	1022.0	E 5	÷14.6	72	> 50	03	0	2	1	6	3	5	0	3	
14	15	1021.6	E 5	÷14.9	71	> 50	02	0	1	1	6	3	0	0	9	0.0
	18	1021.1	E 5	÷14.7	÷11.5	..	71	> 50	02	0	1	1	6	3	0	0	8	
	21	1021.3	E 5	÷15.0	71	> 50	00	0	0	0	0	9	0	0	4	

¹ Solar halo.² Solar halo and parhelia.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
11	00	1021.7	E 4	÷15.7	72	> 50	00	0	0	0	0	9	0	0	3	0.0	
	03	1022.4	0	÷16.5	73	> 50	00	0	0	0	0	9	0	0	3		
	06	1023.0	0	÷14.5	..	÷17.5	70	> 50	00	0	0	0	0	9	0	0	3		
	09	1023.7	E 1	÷15.3	70	> 50	00	0	0	0	0	9	0	0	3		
	12	1024.0	E 4	÷14.6	71	> 50	00	0	0	0	0	9	0	0	1		
	15	1024.2	E 4	÷14.2	72	> 50	00	0	0	0	0	9	0	0	3		
12	18	1022.9	E 4	÷13.3	÷13.0	..	71	> 50	00	0	0	0	0	9	0	0	9	0.0	
	21	1022.4	E 4	÷13.9	70	> 50	00	0	0	0	0	9	0	0	6		
	00	1022.4	E 3	÷14.3	70	> 50	03	0	2	0	0	9	0	0	3		
	03	1022.4	E 1	÷16.0	72	> 50	00	0	0	0	0	9	0	0	3		
	06	1022.7	0	÷15.5	..	÷16.4	70	> 50	00	0	0	0	0	9	0	0	4		0.0
	09	1023.9	0	÷12.2	66	> 50	00	0	0	0	0	9	0	0	3		
13	12	1023.0	0	÷ 8.0	56	> 50	00	0	0	0	0	9	0	0	3	0.0	
	15	1023.3	W 6	÷ 3.0	46	> 50	00	0	0	0	0	9	0	0	3		
	18	1023.3	W 10	÷ 1.5	÷ 1.3	..	43	> 50	02	0	1	0	0	9	4	0	3		
	21	1023.0	W 8	÷ 3.8	44	> 50	03	0	8	0	0	9	4	7	9		
	00	1023.0	W 10	÷ 4.8	47	> 50	02	2	8	0	0	9	2	×	3		
	03	1022.4	W 10	÷ 4.3	50	> 50	02 ¹	2	8	0	0	9	4	7	9		
14	06	1022.9	W 10	÷ 3.2	..	÷15.4	51	> 50	02	2	8	0	0	9	2	×	4	0.0	
	09	1023.1	W 9	÷ 2.6	52	10—20	02	2	8	0	0	9	2	×	1		
	12	1023.5	W 11	÷ 2.0	51	10—20	02	2	8	0	0	9	2	×	3		
	15	1022.1	W 9	÷ 0.6	46	20—50	01	2	6	0	0	9	4	6	9		
	18	1020.3	W 11	0.3	0.3	..	39	> 50	02	2	8	0	0	9	4	7	8		0.0
	21	1018.7	W 9	0.0	38	> 50	02	2	8	0	0	9	4	7	8		
15	00	1018.5	W 9	÷ 0.3	38	> 50	02	2	8	0	0	9	2	×	6	0.0	
	03	1019.9	W 10	÷ 3.6	50	> 50	01	2	5	0	0	9	4	0	4		
	06	1019.9	W 15	÷ 4.0	..	÷ 4.0	46	> 50	02	2	8	0	0	9	2	×	3		
	09	1023.7	W 12	÷ 6.5	48	> 50	02	2	5	4	6	3	4	0	4		
	12	1026.1	W 9	÷ 6.0	41	> 50	02	2	5	3	6	3	4	0	1		
	15	1028.9	W 8	÷ 5.0	40	> 50	02	2	3	0	0	9	4	0	3		
16	18	1030.6	W 6	÷ 4.5	0.2	..	39	> 50	02	2	5	0	0	9	4	0	1	0.0	
	21	1031.5	W 8	÷ 4.0	39	> 50	02	2	5	0	0	9	4	5	1		
	00	1032.4	W 9	÷ 5.0	48	> 50	02	2	5	0	0	9	0	6	3		
	03	1033.0	E 8	÷ 8.2	50	> 50	03	2	2	0	0	9	0	5	3		
	06	1033.1	0	÷ 8.3	..	÷ 8.5	54	> 50	01	0	1	0	0	9	0	5	1		0.0
	09	1032.5	W 5	÷ 4.4	52	> 50	00	0	0	0	0	9	0	0	9		
17	12	1032.0	W 1	÷ 3.5	47	> 50	02	0	1	0	0	9	0	2	8	0.0	
	15	1031.3	E 4	÷ 3.3	42	> 50	03	0	7	0	0	9	0	6	8		
	18	1031.3	E 5	÷ 4.0	÷ 3.0	..	45	> 50	02	2	1	0	0	9	0	1	3		
	21	1031.3	E 6	÷ 5.6	48	> 50	02	0	4	0	0	9	0	2	3		
	00	1031.3	E 5	÷ 6.0	50	> 50	03 ²	2	8	0	0	9	0	7	3		
	03	1031.0	E 3	÷ 7.0	53	> 50	02 ¹	2	8	0	0	9	0	7	9		
18	06	1030.2	0	÷ 5.7	..	÷ 7.0	53	> 50	01	2	7	0	0	9	0	8	9	0.0	
	09	1030.1	0	÷ 3.9	52	> 50	01	2	6	0	0	9	0	8	6		
	12	1029.3	W 6	1.1	40	> 50	01	2	4	0	0	9	4	8	9		
	15	1029.1	W 7	1.2	32	> 50	02	2	4	0	0	9	4	0	7		
	18	1026.7	W 14	2.3	2.3	..	34	> 50	02	0	3	0	0	9	4	0	9		0.0
	21	1025.8	W 17	0.5	35	20—50	09	3	8	0	0	9	2	×	7		

¹ Solar halo.² Solar halo and parhelia.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
17	00	1027.0	W 12	÷ 0.3	42	20—50	09	3	7	0	0	9	7	×	4	
	03	1027.6	W 18 ¹	÷ 1.1	44	> 50	09	3	4	0	0	9	4	0	2	
	06	1029.3	W 11	÷ 0.2	..	÷ 5.7	38	> 50	02	0	3	0	0	9	4	0	4	0.0
	09	1030.8	W 10	0.5	39	> 50	01	0	1	0	0	9	4	0	3	
	12	1030.8	W 10	1.2	36	> 50	00	0	0	0	0	9	0	0	3	
	15	1029.8	W 10	2.6	30	> 50	00	0	0	0	0	9	0	0	9	
	18	1029.0	W 8	3.4	3.7	..	30	> 50	02	0	1	0	0	9	4	0	8	0.0
	21	1027.7	E 7	÷ 1.4	40	> 50	02	0	1	0	0	9	4	0	8	
18	00	1026.9	E 4	÷ 2.8	59	> 50	00	0	0	0	0	9	0	0	8	
	03	1025.9	E 6	÷ 3.6	59	> 50	00	0	0	0	0	9	0	0	8	
	06	1025.0	E 5	÷ 3.2	..	÷ 3.7	57	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1023.8	E 3	÷ 3.2	57	> 50	00	0	0	0	0	9	0	0	8	
	12	1022.3	E 3	÷ 3.0	58	> 50	00	0	0	0	0	9	0	0	8	
	15	1020.2	E 4	÷ 2.5	59	> 50	00	0	0	0	0	9	0	0	9	
	18	1017.9	E 6	÷ 2.7	3.5	..	59	> 50	02	0	1	0	0	9	0	1	8	0.0
	21	1017.1	E 4	÷ 3.5	64	> 50	03	2	4	0	0	9	4	6	6	
19	00	1017.0	E 1	÷ 3.4	62	> 50	03	2	7	0	0	9	2	×	6	
	03	1016.5	SW 7	1.8	60	> 50	03	2	8	0	0	9	7	×	9	
	06	1018.0	W 10	3.2	..	÷ 3.5	60	4—10	02	2	8	8	6	3	×	×	4	0.0
	09	1018.8	W 9	3.3	34	> 50	02	2	8	4	6	4	4	7	1	
	12	1018.4	W 6	3.8	35	> 50	02	2	8	0	0	9	4	7	9	
	15	1017.5	W 14	3.6	24	> 50	02	2	5	0	0	9	4	6	9	
	18	1017.3	W 10	3.4	3.9	..	24	> 50	01	0	1	0	0	9	4	0	6	0.0
	21	1017.5	W 8	2.8	24	> 50	00	0	0	0	0	9	0	0	4	
20	00	1017.2	W 8	2.3	29	> 50	02	0	1	0	0	9	0	1	9	
	03	1016.8	W 6	1.0	38	> 50	02	0	1	0	0	9	4	0	8	
	06	1016.4	W 6	0.7	..	0.7	38	> 50	02	0	1	0	0	9	0	1	8	0.0
	09	1016.6	W 7	1.4	39	> 50	02	0	1	0	0	9	0	1	4	
	12	1017.0	W 7	1.5	31	> 50	02	0	1	0	0	9	0	1	3	
	15	1017.2	W 5	2.3	29	> 50	02	0	1	1	1	6	0	0	3	
	18	1017.5	NW 6	2.2	3.0	..	28	> 50	03	0	3	3	1	6	0	0	3	0.0
	21	1018.7	E 5	÷ 0.7	49	> 50	02	0	3	3	1	6	0	0	4	
21	00	1019.7	E 7	÷ 3.2	52	> 50	02	2	6	1	1	3	7	×	3	
	03	1020.1	E 5	÷ 3.7	64	> 50	03	2	8	0	0	9	7	×	1	
	06	1020.3	E 4	÷ 3.5	..	÷ 3.8	65	> 50	02	2	8	0	0	9	7	×	3	0.0
	09	1020.4	E 5	÷ 3.5	64	> 50	02	2	8	0	0	9	7	×	3	
	12	1021.0	E 5	÷ 3.0	64	> 50	02	2	8	0	0	9	7	×	4	
	15	1021.0	E 5	÷ 3.2	60	> 50	02	2	8	0	0	9	7	×	3	
	18	1020.6	E 2	÷ 2.7	2.2	..	66	> 50	02	2	8	0	0	9	7	×	9	0.0
	21	1019.5	E 2	÷ 2.1	67	> 50	01	2	7	0	0	9	4	×	9	
22	00	1019.0	0	÷ 2.2	67	> 50	02	2	7	0	0	9	4	×	8	
	03	1018.0	W 6	0.1	40	> 50	02	2	7	0	0	9	4	×	9	
	06	1018.1	W 6	÷ 0.5	..	÷ 3.5	42	> 50	01	2	6	0	0	9	4	×	4	0.0
	09	1018.2	E 2	÷ 1.1	46	> 50	01	2	5	0	0	9	4	×	3	
	12	1018.4	E 3	÷ 1.7	53	> 50	02	2	6	0	0	9	4	×	3	
	15	1018.1	E 4	÷ 1.5	50	> 50	02	2	6	0	0	9	4	×	9	
	18	1017.4	E 6	÷ 1.3	0.1	..	51	> 50	01	2	4	0	0	9	4	×	9	0.0
	21	1017.7	E 7	÷ 3.3	60	> 50	01	0	1	0	0	9	4	0	4	

¹ 0000—0300 The wind up to 28 m/sec. Sand drift.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
23	00	1018.0	E 5	÷ 4.1	64	> 50	02	0	1	1	1	3	0	0	3	
	03	1018.4	E 6	÷ 5.3	68	> 50	02	0	3	3	1	3	0	0	3	
	06	1018.7	E 6	÷ 5.2	..	÷ 5.3	69	> 50	03	2	7	7	6	3	×	×	3	0.0
	09	1019.0	E 5	÷ 5.3	69	> 50	02	2	7	7	6	3	×	×	3	
	12	1018.8	E 7	÷ 5.2	69	> 50	02	2	8	8	6	3	×	×	9	
	15	1018.3	E 6	÷ 5.0	68	> 50	01	2	6	6	6	3	×	×	9	
	18	1017.8	E 7	÷ 4.8	÷ 1.1	..	67	> 50	01	0	2	2	1	3	×	×	8	0.0
24	21	1017.8	E 6	÷ 4.8	67	> 50	02	0	4	4	6	3	×	×	3	
	00	1017.7	E 5	÷ 5.8	68	> 50	03	2	7	7	6	3	×	×	9	
	03	1017.4	E 3	÷ 6.8	70	> 50	03	2	8	8	6	3	×	×	9	
	06	1017.0	E 3	÷ 7.3	..	÷ 7.8	74	> 50	02	2	8	8	6	3	×	×	9	0.0
	09	1016.8	E 2	÷ 6.8	75	> 50	02	2	8	8	6	3	×	×	8	
	12	1016.5	0	÷ 6.1	75	> 50	02	2	8	8	6	3	×	×	8	
	15	1016.1	0	÷ 3.8	70	> 50	01	0	2	2	1	3	0	0	8	
25	18	1014.7	0	÷ 3.3	÷ 3.5	..	68	> 50	01	0	1	1	1	3	0	0	9	0.0
	21	1014.2	E 3	÷ 2.8	67	> 50	02	0	1	0	0	9	4	0	8	
	00	1014.1	E 4	÷ 3.2	67	> 50	03	0	3	0	0	9	3	0	6	
	03	1013.9	E 3	÷ 3.4	68	> 50	03	2	6	0	0	9	4	×	8	
	06	1013.7	E 3	÷ 3.6	..	÷ 7.3	68	> 50	02	2	6	0	0	9	4	×	8	0.0
	09	1013.5	0	÷ 2.2	68	> 50	01	2	4	0	0	9	4	0	8	
	12	1013.2	E 4	2.0	59	> 50	02	2	4	0	0	9	4	0	8	
26	15	1012.9	0	2.5	55	> 50	03	2	6	0	0	9	7	×	8	
	18	1012.7	W 10	4.0	4.0	..	47	> 50	03	2	8	0	0	9	7	×	8	0.0
	21	1014.0	W 8	2.5	32	> 50	02	2	7	0	0	9	7	×	4	
	00	1014.7	W 9	1.7	34	> 50	02	2	7	0	0	9	7	×	3	
	03	1014.4	W 6	1.2	39	> 50	01	0	1	0	0	9	4	0	9	
	06	1013.6	W 7	1.7	..	÷ 3.5	39	> 50	02	0	2	0	0	9	4	0	9	0.0
	09	1013.1	0	÷ 0.2	44	> 50	01	0	1	0	0	9	4	0	8	
27	12	1012.0	E 8	÷ 2.3	60	> 50	00	0	0	0	0	9	0	0	8	
	15	1011.5	E 5	÷ 3.2	65	> 50	00	0	0	0	0	9	0	0	8	
	18	1009.7	E 5	÷ 4.0	4.2	..	70	10—20	03	0	1	1	1	2	4	0	8	0.0
	21	1009.0	E 4	÷ 4.3	71	10—20	02	0	1	1	1	2	4	0	6	
	00	1008.3	E 2	÷ 4.8	71	0.2—0.5	47	4	9	9	×	0	×	×	8	
	03	1008.0	E 4	÷ 5.2	71	0.2—0.5	49 ¹	4	9	9	×	0	×	×	6	
	06	1008.0	E 6	÷ 4.7	..	÷ 5.2	70	1—2	02	4	8	8	6	1	×	×	3	0.0
28	09	1008.5	E 6	÷ 5.4	69	1—2	02	2	8	8	6	1	×	×	4	
	12	1009.8	E 5	÷ 5.1	67	10—20	02	2	8	8	6	2	×	×	4	
	15	1009.9	E 6	÷ 4.5	63	20—50	01	2	6	2	1	2	4	×	1	
	18	1009.9	E 6	÷ 4.8	÷ 3.5	..	62	20—50	02	2	8	8	6	3	×	×	3	0.0
	21	1010.2	E 7	÷ 4.7	62	> 50	02	2	8	4	6	3	7	×	4	
	00	1010.7	E 6	÷ 5.6	62	> 50	02	2	8	4	6	3	4	×	3	
	03	1010.4	E 5	÷ 5.7	61	> 50	01	2	6	1	1	3	4	0	9	
29	06	1010.9	E 4	÷ 5.6	..	÷ 6.0	61	> 50	01	0	3	1	1	3	4	0	4	0.0
	09	1011.0	0	÷ 4.2	55	> 50	03	2	6	0	0	9	7	0	3	
	12	1011.2	W 9	÷ 0.5	20	> 50	02	2	7	0	0	9	7	×	3	
	15	1011.4	W 12	÷ 1.2	20	> 50	02	2	7	0	0	9	7	×	3	
	18	1011.5	W 7	÷ 3.0	÷ 0.5	..	20	> 50	02	2	7	0	0	9	2	×	3	0.0
	21	1012.9	W 10	÷ 3.0	20	> 50	01	2	4	0	0	9	4	0	4	

¹ Hoar frost.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
29	00	1013.0	W 8	÷ 3.2	20	> 50	02	2	4	0	0	9	4	0	1	
	03	1013.1	W 10	÷ 3.5	21	> 50	03	2	7	0	0	9	4	×	3	
	06	1013.6	W 12	÷ 4.6	..	÷ 5.6	25	> 50	03	2	8	0	0	9	7	×	4	0.0
	09	1013.2	W 12	÷ 3.4	25	> 50	01	2	7	0	0	9	4	×	9	
	12	1012.8	W 13	÷ 2.7	24	> 50	01	2	6	0	0	9	4	×	8	
	15	1011.7	W 12	÷ 3.2	19	> 50	02	2	8	0	0	9	2	×	9	
	18	1011.2	W 14	÷ 2.5	÷ 2.5	..	31	10—20	02	2	8	0	0	9	2	×	8	0.0
	21	1010.9	W 13	÷ 3.8	55	2—4	71	7	8	8	7	4	×	×	8	
30	00	1010.4	W 16	÷ 4.5	60	2—4	71	7	8	8	7	4	×	×	8	
	03	1010.4	W 14	÷ 2.9	34	> 50	02	2	8	0	0	9	7	×	3	
	06	1011.0	W 14	÷ 2.8	..	÷ 5.0	28	20—50	02	2	8	0	0	9	7	×	4	0.0
	09	1012.6	W 15	÷ 3.2	26	20—50	02	2	8	0	0	9	7	×	4	
	12	1013.5	W 14	÷ 3.0	27	20—50	02	2	8	0	0	9	7	×	3	
	15	1014.5	W 11	÷ 2.4	23	> 50	02	2	8	0	0	9	7	×	3	
	18	1015.4	W 11	÷ 1.5	÷ 1.3	..	20	> 50	01	2	5	0	0	9	4	0	3	0.0
	21	1016.5	W 10	÷ 2.5	24	> 50	02	2	7	0	0	9	7	0	3	
31	00	1017.4	W 10	÷ 3.0	26	> 50	02	2	8	0	0	9	7	×	3	
	03	1017.9	W 9	÷ 3.5	26	> 50	02	2	8	0	0	9	4	7	3	
	06	1018.1	W 6	÷ 3.5	..	÷ 4.1	28	> 50	02	2	8	0	0	9	4	×	3	0.0
	09	1018.0	W 10	÷ 3.2	26	> 50	02	2	8	0	0	9	4	×	9	
	12	1017.8	W 8	÷ 2.4	27	> 50	02	2	8	0	0	9	4	7	8	
	15	1017.0	W 7	÷ 2.1	25	> 50	01	2	6	0	0	9	4	0	9	
	18	1015.6	W 11	÷ 1.7	÷ 1.5	..	22	> 50	02	2	6	0	0	9	4	8	9	0.0
	21	1015.1	W 10	÷ 1.3	22	> 50	02	2	4	0	0	9	4	0	6	
Mean		1019.6		5.6	÷ 6.9	÷ 3.7	÷ 9.9	54	0.2

June 1950

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1014.8	W 9	÷ 2.1	48	> 50	02	0	3	0	0	9	4	0	8	
	03	1014.5	W 7	÷ 2.3	50	> 50	02	0	3	0	0	9	4	0	8	
	06	1014.2	E 8	÷ 4.4	..	÷ 4.5	62	> 50	03 ¹	0	8	0	0	9	4	7	8	0.0
	09	1014.2	E 6	÷ 5.2	74	> 50	02 ¹	2	8	0	0	9	4	7	3	
	12	1014.2	E 6	÷ 4.0	77	> 50	02 ¹	2	8	1	6	5	0	7	3	
	15	1013.6	NE 4	÷ 2.4	74	> 50	01	2	6	0	0	9	4	6	9	
	18	1013.1	W 10	1.6	1.7	..	42	> 50	02	2	8	0	0	9	4	7	8	0.0
	21	1013.8	W 11	0.0	51	> 50	02	2	8	0	0	9	7	×	4	
2	00	1014.1	W 8	÷ 0.2	48	> 50	02	2	8	0	0	9	7	×	1	
	03	1014.2	W 10	÷ 0.2	54	> 50	02	2	8	0	0	9	7	×	3	
	06	1014.6	WNW 15	0.0	..	÷ 5.5	54	> 50	01	2	7	0	0	9	4	×	9	0.0
	09	1014.8	W 12	0.5	50	> 50	02	2	7	0	0	9	4	×	4	
	12	1016.0	W 7	1.4	44	> 50	02	2	7	0	0	9	4	×	3	
	15	1018.3	E 8	÷ 4.2	68	> 50	02	2	6	0	0	9	4	×	4	
	18	1018.4	E 7	÷ 4.0	1.5	..	71	> 50	02	2	5	0	0	9	4	×	1	0.0
	21	1018.8	E 6	÷ 4.2	74	> 50	01	0	1	0	0	9	4	0	3	
3	00	1018.7	E 6	÷ 4.1	76	> 50	02	0	1	0	0	9	4	0	9	

¹ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1018.1	E 5	÷ 4.5	78	> 50	00	0	0	0	0	9	0	0	9	
	06	1018.1	E 5	÷ 4.1	..	÷ 5.1	78	> 50	03	0	1	0	0	9	0	5	3	0.0
	09	1016.8	E 3	÷ 2.8	74	> 50	03	0	4	0	0	9	0	6	9	
	12	1016.0	E 6	÷ 2.8	72	> 50	02	0	4	0	0	9	0	6	6	
	15	1013.8	E 5	÷ 2.0	71	> 50	02	0	2	0	0	9	0	2	9	
	18	1011.7	E 5	÷ 1.7	÷ 1.4	..	71	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1011.0	E 5	÷ 1.7	73	> 50	03 ¹	2	7	0	0	9	0	7	6	
4	00	1009.5	E 6	÷ 1.7	73	> 50	01	2	2	0	0	9	0	5	9	
	03	1007.3	E 4	÷ 2.5	80	> 50	02	0	3	0	0	9	0	5	8	
	06	1004.9	NE E 2	÷ 1.6	..	÷ 4.5	78	> 50	01	0	1	0	0	9	0	1	8	0.0
	09	1002.1	E 2	0.4	72	> 50	03	0	4	0	0	9	0	5	8	
	12	1000.2	E 3	1.5	65	> 50	03	2	8	0	0	9	1	×	8	
	15	998.7	E 2	2.7	64	> 50	01	0	4	0	0	9	4	0	8	
	18	998.4	E 2	5.2	5.3	..	57	> 50	01	0	2	0	0	9	4	0	6	0.0
	21	998.1	W 12	8.1	42	20—50	03	2	8	0	0	9	7	×	8	
5	00	998.0	W 6	7.7	46	20—50	02	2	8	0	0	9	7	×	6	
	03	997.1	W 7	7.7	48	> 50	01	0	3	0	0	9	4	0	9	
	06	997.7	W 6	4.2	..	÷ 1.4	60	> 50	02	0	4	0	0	9	4	0	4	0.0
	09	1000.0	W 11	4.3	67	> 50	02	2	5	0	0	9	4	0	3	
	12	1001.8	W 11	6.2	54	> 50	02	2	3	0	0	9	4	0	3	
	15	1002.9	W 7	7.0	46	> 50	02	0	3	0	0	9	4	0	3	
	18	1002.9	W 3	7.7	7.8	..	43	> 50	02	0	3	0	0	9	4	0	3	0.0
	21	1001.8	ENE 2	7.1	48	> 50	00	0	0	0	0	9	0	0	9	
6	00	1002.1	E 5	4.5	68	> 50	00	0	0	0	0	9	0	0	4	
	03	1002.9	ENE 4	2.4	76	> 50	03	0	3	0	0	9	5	0	3	
	06	1003.4	W 6	5.3	..	2.0	72	> 50	03	1	4	0	0	9	5	0	3	0.0
	09	1004.3	W 10	5.6	54	> 50	02	2	4	0	0	9	4	0	3	
	12	1005.4	W 9	5.4	48	> 50	01	0	3	0	0	9	4	0	3	
	15	1004.8	W 5	6.0	38	> 50	02	0	3	0	0	9	4	0	9	
	18	1003.8	W 4	4.5	6.0	..	41	> 50	03	2	4	0	0	9	4	0	8	0.0
	21	1003.5	E 7	1.8	73	> 50	03	2	7	1	1	3	7	×	6	
7	00	1003.6	E 5	1.4	78	> 50	02	2	8	1	1	3	7	×	4	
	03	1004.7	E 6	÷ 0.1	84	> 50	02	2	8	4	5	3	7	×	4	
	06	1006.0	E 4	÷ 0.2	..	÷ 0.2	91	10—20	70	2	8	6	7	3	7	×	3	trace
	09	1006.7	E 1	÷ 0.4	90	10—20	01	2	5	4	5	3	4	0	1	
	12	1006.7	W 5	2.5	36	> 50	02	0	2	0	0	9	4	0	3	
	15	1905.3	E 4	0.3	77	> 50	02	0	4	0	0	9	4	0	9	
	18	1005.9	E 7	0.0	6.5	..	80	> 50	02	0	3	0	0	9	4	0	4	0.0
	21	1006.7	E 5	÷ 0.2	78	> 50	02	0	3	1	6	3	4	0	3	
8	00	1007.7	E 5	÷ 0.9	79	> 50	02	0	3	2	6	3	4	0	3	
	03	1008.8	E 5	÷ 2.0	81	> 50	03	0	3	0	0	9	0	5	3	
	06	1009.8	E 5	÷ 1.9	..	÷ 2.0	80	> 50	01	0	1	0	0	9	0	1	3	0.0
	09	1010.2	E 6	÷ 1.2	79	> 50	02	0	1	0	0	9	0	1	1	
	12	1009.8	E 6	÷ 0.8	78	> 50	02	0	1	0	0	9	0	1	9	
	15	1009.9	E 6	0.2	76	> 50	02	0	1	0	0	9	0	1	4	
	18	1009.2	E 7	0.7	0.9	..	70	> 50	02	0	1	0	0	9	0	1	9	0.0
	21	1009.5	E 8	0.7	67	> 50	00	0	0	0	0	9	0	0	4	
9	00	1007.9	E 7	1.2	63	> 50	02	0	3	0	0	9	0	1	9	

¹ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1006.6	E 5	÷ 0.8	69	> 50	01	0	1	0	0	9	0	1	8	
	06	1005.9	E 5	÷ 0.9	..	÷ 2.0	75	> 50	02	0	1	0	0	9	0	1	8	0.0
	09	1005.2	E 7	÷ 1.0	73	> 50	03	0	4	0	0	9	0	6	8	
	12	1004.7	E 7	÷ 0.4	66	> 50	02	2	3	0	0	9	5	5	8	
	15	1004.4	E 6	÷ 0.6	71	> 50	02	0	3	0	0	9	5	0	8	
	18	1003.9	E 6	1.0	1.3	..	65	> 50	02	0	3	0	0	9	5	0	8	0.0
	21	1003.8	E 3	0.0	76	> 50	03	2	8	0	0	9	7	×	6	
10	00	1004.4	E 1	0.5	69	> 50	02	2	8	3	6	4	7	×	4	
	03	1005.5	W 5	4.5	71	20—50	02	2	8	3	6	4	7	×	3	
	06	1005.9	E 5	2.2	..	÷ 1.0	73	> 50	01	2	6	0	0	9	4	×	1	0.0
	09	1006.6	E 7	1.9	80	> 50	02	2	8	0	0	9	7	×	3	
	12	1006.8	E 6	2.1	72	> 50	02	2	8	0	0	9	7	×	1	
	15	1005.3	E 7	2.7	70	> 50	01	0	1	0	0	9	4	0	9	
	18	1004.0	E 8	2.7	4.7	..	68	> 50	02	0	1	0	0	9	4	0	8	0.0
	21	1003.1	E 10	2.6	66	> 50	02	0	1	0	0	9	0	1	8	
11	00	1002.4	E 8	1.7	68	> 50	02	0	1	0	0	9	0	1	8	
	03	1002.0	E 5	0.1	75	> 50	02	0	1	0	0	9	4	0	6	
	06	1002.0	E 6	0.4	..	0.1	78	> 50	02	0	1	0	0	9	4	5	3	0.0
	09	1002.0	E 5	1.5	73	> 50	02	0	1	0	0	9	4	2	3	
	12	1002.0	E 5	1.0	76	> 50	00	0	0	0	0	9	0	0	3	
	15	1002.7	E 6	0.7	87	> 50	02 ¹	0	1	0	0	9	0	1	4	
	18	1003.6	E 6	1.8	2.7	..	79	> 50	03	0	5	0	0	9	5	0	3	0.0
	21	1005.7	E 6	1.0	80	> 50	40	2	6	0	0	9	5	0	4	
12	00	1008.1	E 7	0.0	86	> 50	02	2	8	3	6	3	5	×	8	
	03	1010.6	E 6	÷ 0.5	90	20—50	02	2	6	4	6	3	4	0	8	
	06	1011.4	E 7	÷ 0.7	..	÷ 0.7	90	> 50	02	2	7	1	1	3	7	×	1	0.0
	09	1012.4	E 6	0.0	77	> 50	02	2	7	2	1	3	4	×	3	
	12	1012.7	E 4	0.6	72	> 50	01	2	6	1	1	3	4	0	1	
	15	1012.7	E 5	0.8	75	> 50	02	2	7	1	1	3	4	×	3	
	18	1011.3	E 8	0.4	1.8	..	81	> 50	01	0	1	1	1	3	0	1	9	0.0
	21	1010.7	E 7	0.7	82	> 50	02	0	1	1	1	3	0	1	8	
13	00	1010.1	E 6	0.6	84	> 50	02	0	2	0	0	9	0	1	8	
	03	1008.7	E 5	÷ 1.1	88	> 50	40	0	1	0	0	9	0	1	9	
	06	1008.0	E 4	÷ 1.2	..	÷ 2.0	90	> 50	02	4	1	0	0	9	0	1	6	0.0
	09	1006.7	E 4	1.0	79	> 50	40	0	3	0	0	9	0	5	9	
	12	1005.8	E 5	1.3	77	> 50	03	0	4	0	0	9	0	6	8	
	15	1004.4	E 6	2.0	79	> 50	03	2	7	0	0	9	0	7	8	
	18	1003.3	E 8	1.5	2.0	..	80	> 50	03	2	8	0	0	9	7	×	8	0.0
	21	1003.3	E 7	2.6	76	> 50	02	2	8	0	0	9	7	×	3	
14	00	1003.3	E 7	2.8	76	> 50	02	2	8	0	0	9	7	×	3	
	03	1003.3	E 7	1.4	74	> 50	02	2	8	0	0	9	7	×	3	
	06	1003.7	E 5	0.7	..	÷ 1.2	77	> 50	02	2	8	0	0	9	7	×	4	0.0
	09	1005.4	0	1.2	78	> 50	02	2	8	0	0	9	7	×	4	
	12	1005.8	W 12	5.3	64	> 50	02	2	8	0	0	9	7	×	1	
	15	1007.0	W 10	5.5	92	20—50	61	6	8	0	0	9	7	×	4	
	18	1006.9	W 7	5.6	5.6	..	98	20—50	61	6	8	4	0	6	7	×	9	trace
	21	1006.6	W 6	8.1	52	> 50	61	6	3	0	0	9	4	0	9	
15	00	1005.8	W 6	7.9	53	> 50	02	0	4	0	0	9	4	8	9	

¹ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1004.9	E 7	2.2	70	> 50	02	0	4	0	0	9	4	1	8	
	06	1004.3	NE 5	0.5	..	0.3	88	> 50	40	2	6	0	0	9	4	6	8	0.0
	09	1004.3	E 6	0.8	86	> 50	40	2	4	0	0	9	0	5	3	
	12	1004.1	E 5	1.8	79	> 50	02	0	1	0	0	9	0	5	9	
	15	1902.8	E 4	3.2	74	> 50	00	0	0	0	0	9	0	0	9	
	18	1901.8	E 5	4.7	8.2	..	63	> 50	03	0	3	0	0	9	0	0	8	0.0
	21	1000.7	E 6	3.4	64	> 50	03	2	7	0	0	9	5	0	8	
16	00	1000.8	0	5.4	60	> 50	02	2	3	0	0	9	7	×	4	
	03	1001.2	W 7	8.1	39	> 50	02	0	1	1	2	5	5	0	3	
	06	1002.4	W 6	6.9	..	0.5	44	> 50	02	0	2	0	0	9	4	0	4	0.0
	09	1004.0	W 7	9.4	42	> 50	02	0	3	0	0	9	4	0	3	
	12	1004.5	W 10	7.5	48	> 50	02	0	2	1	1	5	4	0	1	
	15	1005.4	W 8	9.5	43	> 50	02	0	3	2	1	5	4	0	3	
	18	1905.3	W 6	9.4	9.5	..	42	> 50	02	0	4	0	0	9	7	0	9	0.0
	21	1005.7	W 7	8.4	47	> 50	03	2	8	0	0	9	7	×	4	
17	00	1905.6	W 4	6.1	54	> 50	02	2	8	0	0	9	7	×	9	
	03	1005.9	W 8	4.9	62	> 50	01	2	7	0	0	9	7	×	9	
	06	1006.0	W 8	5.4	..	4.7	63	> 50	02	2	7	0	0	9	7	×	4	0.0
	09	1007.8	W 7	5.6	61	> 50	02	2	8	0	0	9	7	×	4	
	12	1008.3	W 6	7.4	53	> 50	02	2	7	0	0	9	7	×	1	
	15	1008.2	W 5	9.0	44	> 50	02	2	7	0	0	9	4	×	9	
	18	1008.1	E 6	3.7	9.3	..	63	> 50	02	2	7	0	0	9	4	×	8	0.0
	21	1007.7	E 5	3.8	71	> 50	01	0	2	0	0	9	4	0	9	
18	00	1007.3	E 5	3.2	70	> 50	02	0	2	0	0	9	4	0	8	
	03	1007.7	E 3	3.5	72	> 50	01	0	2	0	0	9	4	1	4	
	06	1007.9	E 3	3.7	..	3.2	73	> 50	02	0	2	0	0	9	4	1	3	0.0
	09	1008.6	E 6	4.9	72	> 50	02	0	2	0	0	9	4	1	4	
	12	1009.6	E 9	5.4	65	> 50	01	0	1	0	0	9	4	0	3	
	15	1010.2	SE 7	5.1	68	> 50	00	0	0	0	0	9	0	0	3	
	18	1011.4	E 8	5.3	5.4	..	66	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1013.1	NE'E 5	3.1	70	> 50	02	0	1	0	0	9	3	0	3	
19	00	1014.8	E 4	2.7	74	> 50	02	0	2	0	0	9	4	0	3	
	03	1017.1	E 5	3.8	73	> 50	02	0	2	0	0	9	3	0	4	
	06	1018.0	E 5	2.7	..	2.5	69	> 50	02	0	2	0	0	9	3	0	1	0.0
	09	1019.4	NE 4	2.4	78	> 50	02	0	2	0	0	9	4	0	3	
	12	1019.8	ENE 6	3.7	73	> 50	03	2	8	0	0	9	1	×	1	
	15	1019.2	SE'E 10	4.5	60	> 50	02	2	8	0	0	9	2	×	9	
	18	1018.4	SE'E 12	4.9	5.4	..	55	> 50	02	2	8	0	0	9	7	×	8	0.0
	21	1017.9	SE'E 10	4.4	56	> 50	02	2	8	0	0	9	7	×	8	
20	00	1017.3	SE 9	3.3	60	> 50	02	2	8	0	0	9	7	×	8	
	03	1016.5	SE'E 6	2.4	68	> 50	02	2	8	0	0	9	7	×	8	
	06	1016.9	NE'E 1	1.2	..	1.0	78	4—10	71	7	8	8	7	5	×	×	4	trace
	09	1016.9	NE'E 2	0.6	84	2—4	71	7	8	8	7	3	×	×	3	
	12	1017.3	ESE 1	0.7	60	1—2	73	7	8	8	7	1	×	×	4	
	15	1018.0	SE'E 5	2.6	68	2—4	71	7	8	8	7	4	×	×	4	
	18	1019.6	ENE 3	2.1	5.0	..	78	2—4	71	7	8	8	7	5	×	×	4	4.2
	21	1022.0	ESE 3	2.8	84	> 50	02	7	8	0	0	9	7	×	4	
21	00	1023.3	E 4	1.4	86	> 50	02	2	8	0	0	9	7	×	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	03	1023.6	ENE 5	2.6	86	> 50	02	2	8	0	0	9	7	×	1	
	06	1023.6	ENE 5	3.5	..	0.1	85	> 50	02	2	8	0	0	9	7	×	3	0.2
	09	1023.8	SE 5	3.2	82	> 50	02	2	8	0	0	9	7	×	3	
	12	1024.0	ESE 4	2.8	80	> 50	02	2	8	1	5	3	7	×	3	
	15	1023.8	E 6	2.4	73	> 50	02	2	8	0	0	9	3	×	9	
	18	1024.0	E 7	2.1	3.9	..	69	> 50	01	2	7	0	0	9	3	×	4	0.0
	21	1024.4	SE 7	2.6	70	> 50	01	0	1	0	0	9	4	0	3	
22	00	1024.2	E 7	3.1	70	> 50	01	0	1	0	0	9	4	0	9	
	03	1024.1	E 6	1.8	73	> 50	02	0	1	0	0	9	0	1	8	
	06	1023.9	E 4	1.6	..	1.6	78	> 50	02	0	1	0	0	9	0	1	8	0.0
	09	1024.6	NE 4	2.5	77	> 50	02	0	1	0	0	9	0	1	4	
	12	1025.3	E 4	4.2	73	> 50	02	0	1	0	0	9	0	1	3	
	15	1025.8	NE 5	4.2	74	> 50	02	0	1	0	0	9	0	1	3	
	18	1026.3	E 4	4.5	4.5	..	75	> 50	02	0	1	0	0	9	0	5	3	0.0
	21	1026.8	E 3	5.1	76	> 50	03	2	5	0	0	9	4	6	3	
23	00	1027.1	E 4	4.8	61	> 50	01	0	3	0	0	9	0	2	3	
	03	1027.6	E 3	6.4	64	> 50	01	0	2	0	0	9	0	2	3	
	06	1028.2	0	8.1	..	1.5	69	> 50	02	0	2	0	0	9	0	2	3	0.0
	09	1028.7	NE'E 3	7.4	64	> 50	03	2	5	0	0	9	0	6	3	
	12	1028.9	E 6	8.3	66	> 50	02	0	3	0	0	9	0	8	3	
	15	1029.0	E 5	7.0	58	> 50	02	0	4	0	0	9	0	8	1	
	18	1029.0	SE'E 9	8.0	8.3	..	54	> 50	03	2	5	0	0	9	0	6	3	0.0
	21	1029.4	SE'E 8	8.5	50	> 50	02	0	4	0	0	9	0	6	4	
24	00	1029.4	E 4	6.2	48	> 50	02	0	3	0	0	9	0	8	3	
	03	1029.6	NE'N 3	5.7	59	> 50	00	0	0	0	0	9	0	0	3	
	06	1029.9	NE 6	3.5	..	3.5	50	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1030.7	SE 7	5.8	50	> 50	00	0	0	0	0	9	0	0	4	
	12	1030.2	SE 10	5.0	56	> 50	00	0	0	0	0	9	0	0	9	
	15	1029.4	E 10	4.4	60	> 50	00	0	0	0	0	9	0	0	9	
	18	1028.9	E 8	4.3	8.5	..	68	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1027.8	E 8	3.0	73	> 50	00	0	0	0	0	9	0	0	9	
25	00	1027.4	SE'E 7	2.2	75	> 50	00	0	0	0	0	9	0	0	6	
	03	1026.2	E 8	2.5	75	> 50	02	0	1	0	0	9	0	1	9	
	06	1025.2	E 6	3.0	..	1.6	76	> 50	02	0	1	0	0	9	0	1	8	0.0
	09	1024.5	NE 6	3.4	76	> 50	00	0	0	0	0	9	0	0	8	
	12	1024.0	E 6	3.8	74	> 50	00	0	0	0	0	9	0	0	8	
	15	1022.8	E 5	4.2	72	> 50	02	0	1	0	0	9	0	2	9	
	18	1022.0	E 6	5.9	6.0	..	70	> 50	02	0	1	0	0	9	0	1	8	0.0
	21	1022.0	ENE 6	5.7	65	> 50	02	0	1	0	0	9	0	1	3	
26	00	1022.4	NE 5	5.2	68	> 50	00	0	0	0	0	9	0	0	4	
	03	1022.5	E 6	4.2	70	> 50	00	0	0	0	0	9	0	0	1	
	06	1022.9	E 6	2.6	..	2.0	74	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1023.7	E 6	5.7	56	> 50	03	0	1	0	0	9	5	0	4	
	12	1023.5	E 6	4.0	64	> 50	03	0	3	0	0	9	5	0	9	
	15	1023.5	E 8	4.3	67	> 50	00	0	0	0	0	9	0	0	3	
	18	1023.0	E 8	4.0	6.0	..	72	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1022.6	E 8	3.0	72	> 50	00	0	0	0	0	9	0	0	8	
27	00	1023.0	E 9	0.4	86	2—4	03	0	8	8	6	2	×	×	4	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1016.5	E 6	4.3	..	3.4	79	> 50	03	0	5	0	0	9	5	0	3	0.0
	09	1017.2	E 5	3.2	80	> 50	02	2	6	1	6	3	5	0	4	
	12	1016.6	E 5	4.6	79	> 50	01	2	3	0	0	9	4	2	9	
	15	1016.1	E 8	6.6	77	> 50	02	0	2	0	0	9	4	0	8	
	18	1015.3	E 6	4.8	6.8	..	79	> 50	02	0	1	0	0	9	4	0	8	0.0
	21	1014.5	E 5	6.3	73	> 50	02	0	1	0	0	9	4	0	8	
3	00	1013.9	E 7	7.6	70	> 50	02	0	1	0	0	9	0	2	8	
	03	1013.1	E 7	5.7	71	> 50	02	0	1	0	0	9	0	2	8	
	06	1012.0	E 7	5.8	..	3.0	69	> 50	02	0	1	0	0	9	0	1	8	0.0
	09	1011.4	E 8	7.0	64	> 50	02	0	1	0	0	9	0	1	8	
	12	1010.2	E 5	5.3	65	> 50	02	0	1	0	0	9	4	0	8	
	15	1008.7	E 6	5.7	60	> 50	02	0	1	0	0	9	4	0	8	
	18	1007.8	E 6	9.0	9.0	..	54	> 50	02	0	1	0	0	9	4	0	6	0.0
	21	1007.2	E 5	8.0	54	> 50	02	0	1	0	0	9	4	0	8	
4	00	1006.5	E 7	6.6	58	> 50	02	0	1	0	0	9	4	0	8	
	03	1006.3	NE 6	6.2	62	> 50	02	0	1	0	0	9	4	0	6	
	06	1006.6	E 6	7.2	..	5.2	63	> 50	02	0	1	0	0	9	4	0	4	0.0
	09	1006.6	E 8	4.5	72	> 50	03 ¹	0	4	0	0	9	4	6	3	
	12	1006.8	E 6	6.5	64	> 50	02	2	7	0	0	9	4	6	4	
	15	1007.0	E 8	11.2	47	> 50	02	2	5	0	0	9	4	6	3	
	18	1007.0	E'S 8	11.6	11.6	..	43	> 50	02	0	3	0	0	9	4	5	3	0.0
	21	1007.0	E 6	11.2	43	> 50	02	0	3	0	0	9	4	5	3	
5	00	1007.0	E 5	7.5	62	> 50	02	0	4	0	0	9	4	0	3	
	03	1007.5	E 6	10.1	55	> 50	02	0	1	0	0	9	4	2	4	
	06	1008.2	SE'E 7	9.2	..	2.1	57	> 50	02	0	1	0	0	9	0	1	3	0.0
	09	1008.8	SE 8	9.0	56	> 50	02	0	1	0	0	9	0	1	3	
	12	1008.9	NE'E 6	8.0	58	> 50	02	0	1	0	0	9	0	1	1	
	15	1008.9	E'N 5	6.0	70	> 50	02	0	1	0	0	9	0	1	3	
	18	1008.7	E 6	7.3	11.5	..	68	> 50	00	0	0	0	0	9	0	0	9	0.0
	21	1008.7	E 5	6.3	73	> 50	00	0	0	0	0	9	0	0	3	
6	00	1008.6	NE 5	6.6	74	> 50	03	2	6	0	0	9	4	0	9	
	03	1009.1	SE 5	7.7	66	> 50	02	2	6	0	0	9	3	×	4	
	06	1009.1	E 4	7.5	..	5.2	68	> 50	00	2	0	0	0	9	0	0	3	0.0
	09	1009.1	E 5	7.0	67	> 50	02	0	1	1	2	5	0	0	3	
	12	1009.3	E 8	7.5	61	> 50	02	0	1	1	2	5	0	0	4	
	15	1009.2	E 7	8.0	61	> 50	02	0	1	1	2	5	0	0	3	
	18	1009.3	E 8	3.2	9.0	..	86	> 50	02	0	3	3	2	5	0	0	3	0.0
	21	1009.3	E'S 6	6.0	69	> 50	02	0	2	2	4	5	0	0	3	
7	00	1009.3	E 6	8.0	55	> 50	02	0	1	1	1	5	0	0	3	
	03	1009.3	E 5	5.7	67	> 50	00	0	0	0	0	9	0	0	3	
	06	1009.3	NE 6	5.5	..	3.2	69	> 50	03	0	3	0	0	9	0	6	3	0.0
	09	1009.2	E 8	5.5	75	> 50	02	2	4	0	0	9	0	8	8	
	12	1009.0	ENE 7	5.5	76	> 50	02	2	4	0	0	9	0	8	8	
	15	1009.1	NE 5	4.2	78	> 50	01	0	2	0	0	9	0	8	4	
	18	1009.2	E 5	5.3	8.2	..	78	> 50	02	0	2	0	0	9	4	0	3	0.0
	21	1010.1	E 3	5.7	72	> 50	03	2	4	0	0	9	4	2	4	
8	00	1010.6	W 6	12.1	42	> 50	01	0	1	0	0	9	4	0	3	
	03	1011.7	W 8	11.5	35	> 50	02	0	2	0	0	9	4	0	4	

¹ Solar halo.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1012.2	WSW 9	11.3	..	5.3	33	> 50	02	0	3	0	0	9	4	0	3	0.0
	09	1014.9	W 9	11.6	40	> 50	02	0	1	1	1	5	0	0	4	
	12	1014.9	W 6	12.8	20	> 50	00	0	0	0	0	9	0	0	3	
	15	1014.3	W 5	12.8	22	> 50	00	0	0	0	0	9	0	0	9	
	18	1013.5	0	13.3	13.4	..	22	> 50	03	0	4	0	0	9	0	6	8	0.0
	21	1011.9	E 8	6.6	64	> 50	01	2	2	0	0	9	0	5	9	
9	00	1011.9	E 6	8.2	58	> 50	02	0	2	0	0	9	4	2	3	
	03	1014.1	W 6	11.4	44	> 50	03	0	3	0	0	9	4	5	4	
	06	1014.9	W 8	12.7	..	8.0	33	> 50	02	0	1	0	0	9	4	0	1	0.0
	09	1015.3	W 7	13.5	27	> 50	02	0	1	0	0	9	0	1	3	
	12	1014.9	W 5	13.4	32	> 50	02	0	4	0	0	9	0	8	9	
	15	1014.6	0	14.6	34	> 50	02	2	6	0	0	9	0	8	8	
	18	1015.6	E 4	8.2	15.0	..	61	> 50	01	0	3	0	0	9	0	8	4	0.0
	21	1015.7	E 6	6.6	69	> 50	02	2	4	0	0	9	4	0	1	
10	00	1016.3	E 4	6.7	66	> 50	01	0	1	0	0	9	4	0	4	
	03	1017.1	W 7	11.1	44	> 50	02	0	2	0	0	9	4	1	3	
	06	1017.7	W 6	11.3	..	6.1	47	> 50	02	0	2	0	0	9	4	5	3	0.0
	09	1019.2	E'S 8	8.7	50	> 50	03	2	8	0	0	9	7	×	4	
	12	1020.0	E 6	8.0	53	> 50	02	2	8	0	0	9	2	×	1	
	15	1020.0	E 7	5.0	76	> 50	02	2	8	0	0	9	7	×	3	
	18	1019.3	ESE 7	8.2	14.6	..	70	> 50	02	2	8	0	0	9	7	×	9	0.0
	21	1018.8	ESE 6	8.0	63	> 50	01	2	6	0	0	9	4	0	8	
11	00	1017.7	E'S 8	8.8	53	> 50	02	2	7	0	0	9	7	0	9	
	03	1016.5	E 6	7.5	57	> 50	02	2	7	0	0	9	7	0	8	
	06	1015.7	E 5	6.3	..	4.4	64	> 50	02	2	8	0	0	9	7	0	8	0.0
	09	1014.6	SE 5	6.9	66	> 50	01	2	8	0	0	9	7	×	8	
	12	1013.6	E 5	8.2	65	> 50	01	2	7	0	0	9	7	×	8	
	15	1012.0	NE 2	7.7	69	> 50	01	2	7	0	0	9	3	×	9	
	18	1011.4	E 4	8.9	9.3	..	69	> 50	02	2	7	0	0	9	3	×	6	0.0
	21	1011.6	0	6.7	70	> 50	02	2	7	0	0	9	3	×	4	
12	00	1011.4	W 5	8.8	72	> 50	02	2	7	0	0	9	3	×	9	
	03	1011.2	W 9	9.6	64	> 50	02	2	7	0	0	9	3	×	8	
	06	1010.8	W 9	9.2	..	6.2	64	> 50	02	2	8	0	0	9	7	×	8	0.0
	09	1010.3	W 6	10.6	56	> 50	01	2	6	0	0	9	3	0	8	
	12	1009.3	W 6	11.8	48	> 50	01	0	3	1	1	8	4	0	9	
	15	1008.3	W 6	12.5	43	> 50	02	0	3	1	1	8	4	0	8	
	18	1007.8	E 6	5.6	12.5	..	75	> 50	02	0	1	0	0	9	4	0	6	0.0
	21	1007.1	E 5	6.0	75	> 50	01	0	1	0	0	9	4	0	8	
13	00	1007.1	E 6	5.0	80	> 50	00	0	0	0	0	9	0	0	3	
	03	1007.1	E 4	4.8	85	> 50	00	0	0	0	0	9	0	0	3	
	06	1007.0	E 5	4.8	..	3.9	84	> 50	00	0	0	0	0	9	0	0	8	0.0
	09	1007.2	E 3	5.7	76	> 50	02	0	1	0	0	9	4	0	4	
	12	1006.9	E 2	10.2	57	> 50	02	0	1	0	0	9	4	1	9	
	15	1006.9	E 5	10.6	56	> 50	02	0	1	0	0	9	0	1	3	
	18	1007.6	E 9	6.9	13.2	..	63	> 50	02	0	1	0	0	9	0	1	4	0.0
	21	1008.6	ESE 10	7.2	66	> 50	02	0	1	0	0	9	0	1	4	
14	00	1010.1	ESE 9	5.3	72	> 50	02	0	1	0	0	9	0	1	4	
	03	1011.6	E 5	3.9	81	> 50	02	0	1	0	0	9	0	1	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1012.6	E 7	2.6	..	2.0	87	> 50	02	0	2	0	0	9	0	2	3	0.0
	09	1014.2	E 7	2.9	88	> 50	02	0	1	0	0	9	0	1	3	
	12	1015.0	E 7	2.5	87	> 50	40	0	1	0	0	9	0	1	1	
	15	1016.0	E 6	2.5	87	> 50	00	0	0	0	0	9	0	0	3	
	18	1016.3	E 6	3.9	7.3	..	82	> 50	00	0	0	0	0	9	0	0	1	0.0
	21	1017.4	E 7	3.1	87	> 50	00	0	0	0	0	9	0	0	4	
15	00	1018.9	E 6	2.9	88	> 50	00	0	0	0	0	9	0	0	3	
	03	1019.5	E 7	2.6	87	> 50	00	0	0	0	0	9	0	0	1	
	06	1020.3	E 6	1.9	..	1.6	86	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1021.2	E 4	3.8	81	> 50	00	0	0	0	0	9	0	0	3	
	12	1021.6	E 5	4.2	78	> 50	00	0	0	0	0	9	0	0	1	
	15	1021.8	E 6	4.3	78	> 50	00	0	0	0	0	9	0	0	3	
	18	1021.9	E 6	4.8	4.8	..	75	> 50	00	0	0	0	0	9	0	0	3	0.0
	21	1022.0	E 9	4.0	82	> 50	00	0	0	0	0	9	0	0	3	
16	00	1022.3	E 8	4.3	82	> 50	00	0	0	0	0	9	0	0	3	
	03	1022.3	E 7	3.6	81	> 50	00	0	0	0	0	9	0	0	3	
	06	1022.0	E 8	4.7	..	1.4	80	> 50	00	0	0	0	0	9	0	0	9	0.0
	09	1021.6	E 8	3.7	81	> 50	00	0	0	0	0	9	0	0	8	
	12	1020.8	E 8	5.0	82	> 50	00	0	0	0	0	9	0	0	9	
	15	1020.1	E 7	6.3	78	> 50	02	0	2	0	0	9	0	2	8	
	18	1019.6	E 8	7.0	7.0	..	75	> 50	02	0	3	0	0	9	0	2	8	0.0
	21	1019.8	E 7	7.5	73	> 50	01	0	1	0	0	9	0	1	4	
17	00	1021.1	E 6	7.7	69	> 50	00	0	0	0	0	9	0	0	4	
	03	1022.6	E 6	6.5	72	> 50	00	0	0	0	0	9	0	0	3	
	06	1023.2	E 6	5.7	..	5.7	74	> 50	00	0	0	0	0	9	0	0	1	0.0
	09	1024.2	E 5	5.6	75	> 50	03	0	1	0	0	9	0	5	3	
	12	1024.3	E 5	5.5	77	> 50	02	0	3	0	0	9	0	4	1	
	15	1024.3	E 6	5.3	79	> 50	03	0	6	0	0	9	5	2	3	
	18	1024.3	E 8	5.5	8.0	..	81	> 50	01	0	3	0	0	9	4	0	3	0.0
	21	1025.4	E 8	6.1	75	> 50	01	0	1	0	0	9	4	0	4	
18	00	1026.0	E 8	5.0	83	> 50	00	0	0	0	0	9	0	0	1	
	03	1026.6	E 8	5.6	80	> 50	00	0	0	0	0	9	0	0	3	
	06	1026.4	ENE 6	4.8	..	4.4	80	> 50	02	0	1	0	0	9	0	1	9	0.0
	09	1026.3	E 5	5.3	80	> 50	02	0	2	0	0	9	0	2	8	
	12	1025.8	NE 5	5.7	78	> 50	02	0	2	0	0	9	0	2	9	
	15	1024.4	E 8	4.4	82	> 50	02	0	2	0	0	9	0	8	9	
	18	1023.3	E 8	7.1	7.1	..	78	> 50	02	0	2	0	0	9	0	8	8	0.0
	21	1022.8	NE'E 7	7.0	71	> 50	02	0	1	0	0	9	0	9	6	
19	00	1022.6	SE'E 6	7.9	68	> 50	02	0	2	0	0	9	0	1	8	
	03	1022.5	E 5	5.7	77	> 50	02	0	1	0	0	9	0	1	8	
	06	1022.5	E 8	4.3	..	4.3	81	> 50	02	0	1	0	0	9	0	1	3	0.0
	09	1022.9	E 7	4.0	82	> 50	02	0	3	0	0	9	0	2	4	
	12	1023.3	E 7	4.6	80	> 50	02	0	3	0	0	9	0	2	3	
	15	1023.6	E 9	5.2	80	> 50	00	0	0	0	0	9	0	0	3	
	18	1024.4	E 9	5.8	7.9	..	78	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1025.4	E 7	6.0	80	> 50	00	0	0	0	0	9	0	0	3	
20	00	1026.9	E 6	6.3	72	> 50	02	0	1	0	0	9	0	2	4	
	03	1027.0	E 5	5.8	67	> 50	02	0	1	0	0	9	0	1	3	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	06	1026.7	E 6	5.0	..	4.0	74	> 50	02	0	1	0	0	9	0	1	9	0.0
	09	1027.0	E 7	5.0	74	> 50	02	0	1	0	0	9	0	1	2	
	12	1026.7	E 8	6.4	55	> 50	02	0	1	0	0	9	0	1	7	
	15	1026.4	E 9	5.4	67	> 50	02	0	1	0	0	9	0	1	8	
	18	1026.1	E 12	4.3	6.8	..	70	> 50	02	0	1	0	0	9	0	1	8	0.0
	21	1025.2	E 11	4.2	73	> 50	02	0	1	0	0	9	0	1	9	
21	00	1024.8	E 6	2.2	82	> 50	02	0	1	0	0	9	0	1	6	
	03	1022.8	SE 8	2.2	81	> 50	02	0	1	1	1	3	0	1	9	
	06	1021.9	ENE 7	0.5	..	0.5	90	> 50	02	0	1	1	5	3	0	1	6	0.0
	09	1020.9	E 7	0.9	94	> 50	02	0	1	1	5	2	0	9	8	
	12	1020.2	E 7	2.4	89	> 50	02	0	1	0	0	9	0	1	6	
	15	1019.2	E 7	4.2	80	> 50	00	0	0	0	0	9	0	0	8	
	18	1019.3	E 7	5.0	5.2	..	80	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1019.4	E 8	5.0	78	> 50	00	0	0	0	0	9	0	0	3	
22	00	1019.4	E 7	3.1	82	> 50	02	0	1	1	5	3	0	1	3	
	03	1018.5	E 8	0.6	93	1—2	10	2	8	8	5	1	×	×	9	
	06	1017.9	E 9	0.4	..	0.4	92	2—4	02	2	8	8	6	1	×	×	9	0.0
	09	1016.4	E 6	0.5	90	2—4	02	2	8	8	6	1	×	×	9	
	12	1015.0	E 4	1.0	84	20—50	02	2	8	2	6	1	5	6	8	
	15	1013.3	E 5	1.5	81	> 50	02	2	7	0	0	9	7	0	8	
	18	1011.6	E 5	1.7	5.0	..	82	> 50	02	2	7	0	0	9	7	0	8	0.0
	21	1010.4	E 3	1.9	84	> 50	61	6	8	0	0	9	7	×	6	
23	00	1009.5	0	3.2	80	> 50	02	2	8	0	0	9	7	×	8	
	03	1009.3	0	4.5	78	> 50	02	2	8	0	0	9	7	×	6	
	06	1009.2	SE'E 1	4.3	..	0.0	79	> 50	01	2	8	0	0	9	7	×	8	trace
	09	1009.5	0	6.3	76	> 50	01	2	5	0	0	9	4	×	4	
	12	1009.6	0	8.5	69	> 50	01	0	1	0	0	9	4	0	3	
	15	1010.2	E 8	6.5	71	> 50	02	0	1	0	0	9	4	0	4	
	18	1011.0	SE 5	7.3	10.8	..	68	> 50	02	0	1	0	0	9	4	9	3	0.0
	21	1012.6	E 5	7.3	68	> 50	02	0	1	0	0	9	4	1	4	
24	00	1013.9	E 5	6.8	72	> 50	02	0	3	0	0	9	4	2	3	
	03	1015.4	E 1	7.1	71	> 50	02	0	2	0	0	9	4	2	3	
	06	1015.9	E 5	7.0	..	3.6	70	> 50	02	0	1	0	0	9	0	1	1	0.0
	09	1016.2	E 5	6.6	71	> 50	03	0	6	0	0	9	5	0	3	
	12	1016.2	E 6	7.0	69	> 50	01	0	1	0	0	9	4	0	3	
	15	1015.2	E 8	9.0	60	> 50	00	0	0	0	0	9	0	0	9	
	18	1014.4	E 6	10.2	10.2	..	66	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1014.2	E 7	8.2	68	> 50	00	0	0	0	0	9	0	0	6	
25	00	1014.3	E 5	7.4	71	> 50	02	0	1	0	0	9	0	1	4	
	03	1014.3	0	8.2	70	> 50	00	0	0	0	0	9	0	0	3	
	06	1013.8	0	9.4	..	5.8	66	> 50	02	0	1	0	0	9	0	1	9	0.0
	09	1013.5	SE 3	9.3	62	> 50	03	0	2	0	0	9	0	5	8	
	12	1013.1	NW 2	11.7	48	> 50	03	2	7	0	0	9	5	6	8	
	15	1012.8	E 7	9.7	58	> 50	02	2	7	0	0	9	5	×	8	
	18	1012.7	E 7	7.8	12.0	..	65	> 50	02	2	7	0	0	9	4	4	6	0.0
	21	1013.1	E 5	9.0	56	> 50	01	0	2	0	0	9	4	1	4	
26	00	1013.0	ENE 6	8.3	69	> 50	01	0	1	0	0	9	0	1	9	
	03	1013.3	E 7	6.5	78	> 50	00	0	0	0	0	9	0	0	4	

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	00	1012.0	W 10	5.2	58	> 50	01	2	7	0	0	9	4	×	3	
	03	1012.4	W 11	3.8	70	> 50	02	2	8	0	0	9	7	×	1	
	06	1012.9	W 10	2.4	..	2.4	86	4—10	02	2	8	4	5	3	7	×	3	0.0
	09	1012.9	W 11	3.0	82	20—50	02	6	8	8	5	6	×	×	3	
	12	1012.6	W 10	3.1	81	4—10	02	2	8	2	5	3	3	×	8	
	15	1012.5	W 10	3.2	82	4—10	60	6	8	8	7	3	×	×	8	
	18	1011.8	W 9	3.3	6.0	..	82	4—10	60	6	8	3	5	3	7	×	9	trace
	21	1011.1	W 8	4.0	71	> 50	02	2	8	0	0	9	7	×	8	
2	00	1010.8	W 7	4.2	70	> 50	02	2	8	0	0	9	7	×	6	
	03	1011.1	W 6	4.2	68	> 50	01	2	7	0	0	9	4	×	4	
	06	1011.4	W 6	4.7	..	2.6	66	> 50	01	2	7	0	0	9	4	×	3	0.0
	09	1012.0	SE'E 5	3.6	52	> 50	02	2	7	0	0	9	4	×	4	
	12	1012.7	E 5	4.4	71	> 50	01	2	7	0	0	9	3	×	3	
	15	1013.4	SE 6	5.0	72	> 50	01	2	4	0	0	9	3	×	3	
	18	1013.5	SE'E 6	4.7	5.3	..	69	> 50	02	2	6	0	0	9	3	×	1	0.0
	21	1013.7	SE'E 5	5.2	65	> 50	02	2	6	0	0	9	3	×	3	
3	00	1014.1	SE'E 8	4.4	68	> 50	02	2	8	0	0	9	3	×	3	
	03	1014.9	SE 3	1.9	..	1.4	86	> 50	02	2	6	1	5	4	4	×	4	
	06	1015.0	SE 7	3.0	78	> 50	02	2	7	0	0	9	4	×	1	0.0
	09	1015.0	SE'E 6	4.5	71	> 50	01	2	6	0	0	9	4	×	3	
	12	1015.0	SE'E 5	3.5	72	> 50	01	0	3	0	0	9	4	0	3	
	15	1014.6	NE 6	1.9	84	> 50	03	2	7	0	0	9	7	×	9	
	18	1014.7	E 6	1.3	4.6	..	82	> 50	03	2	8	0	0	9	7	×	4	0.0
	21	1014.6	E 6	1.1	72	> 50	02	2	8	0	0	9	7	×	9	
4	00	1014.7	E 5	1.4	80	> 50	02	2	8	0	0	9	2	×	4	
	03	1014.7	E 6	1.0	84	> 50	01	2	7	0	0	9	7	×	3	
	06	1015.0	E 5	1.2	..	0.4	85	> 50	01	0	3	0	0	9	4	0	4	0.0
	09	1015.1	SE'E 6	1.5	87	> 50	02	0	4	1	5	3	4	2	3	
	12	1015.0	ENE 7	2.2	86	> 50	02	0	4	0	0	9	4	2	2	
	15	1015.0	ENE 6	2.6	83	> 50	03	2	7	0	0	9	3	×	3	
	18	1014.6	NE 3	3.3	3.3	..	80	> 50	02	2	7	0	0	9	3	×	9	0.0
	21	1014.7	NE 5	4.4	70	> 50	01	2	5	0	0	9	3	×	4	
5	00	1014.6	SE'E 8	5.3	64	> 50	01	2	6	0	0	9	3	×	9	
	03	1014.5	E 3	2.8	65	> 50	03	2	8	0	0	9	3	×	8	
	06	1014.3	E 4	3.3	..	2.6	68	> 50	02	2	8	0	0	9	3	×	8	0.0
	09	1014.0	E 5	3.7	68	> 50	02	2	8	0	0	9	3	×	8	
	12	1013.2	E 5	4.3	69	> 50	02	2	8	0	0	9	3	×	9	
	15	1011.5	NE 6	4.3	71	> 50	01	0	3	0	0	9	4	0	9	
	18	1010.1	E 5	4.4	5.4	..	73	> 50	01	0	2	0	0	9	0	1	8	0.0
	21	1008.6	NE 3	4.4	71	> 50	02	0	1	0	0	9	0	2	8	
6	00	1007.4	E 4	5.1	68	> 50	02	2	6	0	0	9	0	2	8	
	03	1007.3	E 2	4.1	69	> 50	03	2	8	0	0	9	0	7	6	
	06	1007.6	S 2	4.6	..	3.2	72	> 50	03	2	8	0	0	9	2	×	4	0.0
	09	1008.7	W 10	6.5	51	> 50	01	0	3	0	0	9	3	0	4	
	12	1009.2	W 8	6.6	47	> 50	01	0	1	0	0	9	0	1	1	
	15	1009.3	W 11	7.2	42	> 50	00	0	0	0	0	9	0	0	1	

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
	18	1011.1	W 9	8.2	8.2	..	33	> 50	00	0	0	0	0	9	0	0	4	0.0
	21	1010.5	W 8	8.5	30	> 50	02	0	1	0	0	9	0	1	9	
7	00	1011.0	NW'W3	7.0	33	> 50	02	0	1	0	0	9	0	1	4	
	03	1011.2	0	5.2	44	> 50	00	0	0	0	0	9	0	0	3	
	06	1011.9	SE'E 2	3.2	..	3.2	69	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1012.6	0	5.9	52	> 50	00	0	0	0	0	9	0	0	3	
	12	1013.1	W 5	7.3	39	> 50	02	0	1	0	0	9	0	1	3	
	15	1014.2	W 6	8.8	31	> 50	00	0	0	0	0	9	0	0	4	
	18	1013.5	W 4	9.2	9.2	..	33	> 50	02	0	1	0	0	9	0	1	9	0.0
	21	1013.8	W 4	10.2	34	> 50	00	0	0	0	0	9	0	0	4	
8	00	1014.1	E 4	4.3	60	> 50	02	0	2	0	0	9	0	1	3	
	03	1014.3	E 3	4.0	65	> 50	02	0	2	0	0	9	0	1	3	
	06	1014.3	NE 4	3.9	..	2.6	74	> 50	02	0	2	0	0	9	0	1	3	0.0
	09	1013.8	E 3	4.7	68	> 50	02	0	1	0	0	9	0	1	9	
	12	1012.9	NE 5	4.5	68	> 50	02	0	1	0	0	9	0	1	9	
	15	1011.3	ENE 5	4.4	69	> 50	00	0	0	0	0	9	0	0	9	
	18	1009.8	E 6	4.7	10.7	..	67	> 50	02	0	1	0	0	9	0	1	8	0.0
	21	1008.4	NE 3	4.6	68	> 50	00	0	0	0	0	9	0	0	8	
9	00	1007.3	E 4	5.0	69	> 50	02	0	1	0	0	9	4	0	8	
	03	1005.8	E 4	3.6	75	> 50	02	0	1	0	0	9	0	1	8	
	06	1005.1	NE 5	4.4	..	2.6	76	> 50	02	0	1	0	0	9	4	0	6	0.0
	09	1004.6	E 5	4.2	75	> 50	02	0	1	0	0	9	4	0	8	
	12	1003.7	SE 3	4.4	73	> 50	02	0	1	0	0	9	4	0	8	
	15	1002.5	0	5.7	70	> 50	02	0	1	0	0	9	4	0	8	
	18	1001.9	W 3	8.5	8.5	..	51	> 50	02	0	1	0	0	9	4	6	6	0.0
	21	1001.9	W 9	9.7	37	> 50	00	0	0	0	0	9	0	0	3	
10	00	1003.2	W 13	8.3	41	> 50	00	0	0	0	0	9	0	0	4	
	03	1004.2	NW'W7	5.5	56	> 50	02	0	1	0	0	9	0	1	3	
	06	1005.6	W 9	6.4	..	4.1	57	> 50	00	0	0	0	0	9	0	0	3	0.0
	09	1006.1	W 7	6.7	56	> 50	00	0	0	0	0	9	0	0	1	
	12	1006.5	W 6	7.7	52	> 50	00	0	0	0	0	9	0	0	3	
	15	1005.6	W 3	8.5	44	> 50	00	0	0	0	0	9	0	0	9	
	18	1004.6	SE'E 6	5.0	10.0	..	69	> 50	00	0	0	0	0	9	0	0	8	0.0
	21	1003.5	NE 6	4.5	71	> 50	00	0	0	0	0	9	0	0	8	
11	00	1002.0	E 5	5.5	66	> 50	00	0	0	0	0	9	0	0	8	
	03	1001.0	SE 3	2.5	70	> 50	02	0	1	0	0	9	4	0	8	
	06	999.6	0	5.2	..	2.5	68	> 50	03	2	6	0	0	9	0	2	8	0.0
	09	998.9	W 2	5.5	65	> 50	01	0	2	0	0	9	0	1	6	
	12	998.3	NE'E 2	5.6	56	> 50	00	0	0	0	0	9	0	0	8	
	15	996.7	W 6	12.1	39	> 50	00	0	0	0	0	9	0	0	8	
	18	995.8	W 8	12.5	13.2	..	46	> 50	00	0	0	0	0	9	0	0	6	0.0
	21	995.8	W 7	11.7	40	> 50	00	0	0	0	0	9	0	0	3	
12	00	995.3	W 8	10.7	42	> 50	00	0	0	0	0	9	0	0	9	
	03	995.3	W 7	9.8	46	> 50	02	0	1	0	0	9	0	2	3	
	06	995.6	E 5	5.3	..	5.3	65	> 50	02	0	1	0	0	9	0	2	4	0.0
	09	996.0	W 7	8.5	57	> 50	02	0	1	0	0	9	0	1	3	
	12	995.9	W 7	9.3	47	> 50	02	0	2	0	0	9	0	1	9	
	15	994.9	W 6	10.2	×	> 50	02	0	3	0	0	9	4	0	9	

Færdig fra trykkeriet den 16. maj 1952.